Project Traffic Analysis Report (PTAR)

Alternatives Evaluation Study Sinclair Road Extension From Tradition Boulevard to Bella Citta Boulevard

Prepared for:



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PROFESSIONAL ENGINEER CERTIFICATION PROJECT TRAFFIC ANALYSIS REPORT (PTAR)

Project: Alternatives Evaluation Study

Sinclair Road Extension

From Tradition Boulevard to Bella Citta Boulevard

This project traffic analysis report contains engineering information that fulfills the purpose and need for the Alternatives Evaluation Study for Sinclair Road Extension from Tradition Boulevard to Bella Citta Boulevard in Osceola County, Florida. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering as applied through professional judgment and experience. I hereby certify that I am a registered professional engineer in the State of Florida practicing with Kimley-Horn and Associates, Inc., and that I have prepared or approved the evaluation, findings, opinions, conclusions, or technical advice for this project.

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1.0 EXECUTIVE SUMMARY

The Project Traffic Analysis Report (PTAR) has been prepared to provide design traffic volumes and traffic analyses in support of the Alternatives Evaluation Study for Sinclair Road Extension from Tradition Boulevard to Goodman Road. The Sinclair Road Extension will consist of a 4-lane roadway with a center median. Bicycle and pedestrian facilities will also be included.

Traffic data were collected and analyzed to document intersection and arterial operational conditions along the future road extension and the study intersections of Sinclair Road and Tradition Boulevard and Goodman Road and Sinclair Road Extension/Bella Citta Boulevard. The study area also included multiple nearby roadways segments. This analysis evaluates Opening Year 2025 and Design Year 2045 Build conditions and determines arterial speed, arterial level of service (LOS), average travel speed, and other intersection measures of effectiveness (MOEs). The study intersections were evaluated to determine the appropriate lane configurations and traffic control types once Sinclair Road Extension is in place.

Future volumes along the study intersections were developed by comparing annual average daily traffic (AADT) obtained from the Central Florida Regional Planning Model (CFRPM v7) and adjusting the model outputs to account for the model's accuracy in replicating historical traffic volumes. The adjusted AADT was then inputted into the TURNS5 tool to generate the design hourly volume (DHV). Study intersections were evaluated based on the Highway Capacity Manual (HCM) 6th Edition methodologies using Synchro (v11) software.

Under the Build conditions, the Sinclair Road Extension is anticipated to operate acceptably. The northern T-intersection at Tradition Boulevard was found to operate acceptably under signalized control with a dedicated permissive/protected southbound left-turn lane and dedicated left- and right-turn lanes for the minor approach. The intersection at Goodman Road was found to operate acceptably under signalized control, with all approaches providing dedicated permissive/protected left-turn lanes.

Additionally, this study also recommends queue lengths for the left-turn lanes at the study intersections for the Design Year 2045, as shown in **Table ES-1** below.

Table ES-1: Recommended Turn Lane Queue Lengths

| Intersection | Turn Lane Queue Length (feet) | | | | | | | |
|-------------------------------------------|-------------------------------|-----|-----|-----|--|--|--|--|
| intersection | EBL | WBL | NBL | SBL | | | | |
| Sinclair Rd & Tradition Bvld | - | 250 | ı | 300 | | | | |
| Sinclair Rd/Bella Citta Blvd & Goodman Rd | 100 | 500 | 175 | 175 | | | | |

2.0 INTRODUCTION

This Project Traffic Analysis Report (PTAR) has been prepared by Kimley-Horn and Associates, Inc. (Kimley-Horn) on behalf of Osceola County. The purpose of this PTAR is to provide design traffic volumes and traffic analyses in support of the Alternatives Evaluation Study for Sinclair Road Extension.

2.1 PROJECT DESCRIPTION

Osceola County is conducting an Alternatives Evaluation Study, which may be followed by the development of design plans for the extension of Sinclair Road from Tradition Boulevard to Bella Citta Boulevard. This project involves the construction of a new 4-lane divided roadway with pedestrian and bicycle facilities from Tradition Boulevard to South Goodman Road at Bella Citta Boulevard. Associated drainage improvements and stormwater ponds, and modifications of the intersections at each end of the project will be evaluated.

Under existing conditions, Sinclair Road, from Tradition Boulevard to SR 429, is a 4-lane local road with a posted speed limit of 35 MPH. From SR 429 to Old Lake Wilson Road, Sinclair Road is an Urban Major Collector with a posted speed limit of 35 MPH. Bella Citta Boulevard, west of Goodman Road, is a 2-lane Urban Major Collector with a posted speed limit of 40 MPH. The project is located in Osceola County, Florida and is displayed on **Exhibit 1**.

2.2 EXISTING TRANSIT SERVICE

There is no transit service in the study area.

2.3 OBJECTIVE

The objective of this report is to provide Osceola County with the annual average daily traffic (AADT), peak hour volumes (PHV), intersection and roadway volume-to-capacity (V/C) ratios, and level of service (LOS) for the Existing Year 2021, and traffic forecasts for Opening Year 2025 and the Design Year 2045 Build condition. A No-Build condition is not addressed in this report. This report includes the development of the design traffic characteristics, including standard K-factor, design hour directional demand (D), and percentage of trucks for both the design hour and daily demand (Tf, T24) for use in the operational analysis of future conditions. Intersection turning movement queue lengths are also documented.

Exhibit 1: Project Location Map



3.0 METHODOLOGY

The methodology for this analysis, dated February 2, 2022 (provided in **Appendix A**), describes the project assumptions, analysis years, measures of effectiveness (MOE), safety analysis, and future traffic development. The MOEs are as follows:

Table 1: Measures of Effectiveness (MOE) Summary

| Intersection | Arterial | Safety |
|---------------------------|---------------------------|----------------------|
| Queue Lengths | Travel Speed | Crash Frequency |
| Volume-to-Capacity Ratios | Arterial Level-of-Service | Crash Rate |
| Delay | | Number of Fatalities |
| Level of Service | | Crash Severity Level |

While the County does not have LOS standards for transportation, they do consider V/C ratios as one of many factors (which are related to the County's mobility indicators) in establishing priorities for roadway improvements. It should be noted that while V/C ratios below 1.0 are desirable, they are not required by Osceola County.

4.0 EXISTING CONDITIONS

An analysis of existing year (2021) operating conditions was conducted for the study area segments and intersections. Data collection was conducted to establish intersection turning movement counts and segment counts. The results of this data collection are presented in the subsequent tables and exhibits.

4.1 TRAFFIC COUNT INFORMATION

Traffic volume counts were collected from existing sources and supplemented with additional counts obtained for this study. Existing sources are summarized in **Table 2**.

Table 2: Existing Traffic Counts

| Source | Station | Location | Туре | Date |
|--------------------|---------|--------------------------------------------|-----------------|-----------|
| FDOT | 921086 | Goodman Rd, north of Bella Citta Blvd | Historic, Daily | 7/8/2020 |
| Florida Traffic | 921087 | Historic, Daily | 7/7/2020 | |
| Online | 927084 | Bella Citta Blvd, west of Goodman Rd | Historic, Daily | 7/7/2020 |
| | 126 | Goodman Rd, north of Bella Citta Blvd | Daily | 4/1/2021 |
| | 121 | Masters Blvd, south of Bella Citta Blvd | Daily | 10/7/2021 |
| Osceola | 184 | Bella Citta Blvd, west of Goodman Rd | Daily | 3/24/2021 |
| County | 122 | Champion Gate Blvd, east of Masters Blvd | Daily | 9/16/2021 |
| | 105 | S Old Lake Wilson Rd, north of Sinclair Rd | Daily | 3/23/2021 |
| | 103 | S Old Lake Wilson Rd, south of Sinclair Rd | Daily | 3/23/2021 |

Since Sinclair Road Extension is a planned road, traffic data collection of existing conditions was minimal, focused on the roadways on each end of the extension, as shown in **Table 3**.

Table 3: Study Traffic Count Locations

| Count Type | Count Location |
|--------------------------------------|----------------------------------------------|
| | Sinclair Road, north of Tradition Boulevard |
| | Bella Citta Boulevard, west of Goodman Road |
| 72-hour Bi-directional Volume Counts | Goodman Road, north of Bella Citta Boulevard |
| | Goodman Road, south of Bella Citta Boulevard |
| | Happy Trail, west of Sinclair Road |
| 8-hour Turning Movement Counts | Bella Citta Boulevard at Goodman Road |

No vehicle classification counts were taken as the future conditions are expected to be different than existing traffic. Future truck percentages were estimated based on similar functioning roadways within Osceola County.

4.2 EXISTING GEOMETRY

The existing geometry in the study area was obtained through a review of aerial imagery and confirmed through field observations. The existing typical cross-section for Sinclair Road, from SR 429 to Tradition Boulevard, is four 12-foot lanes with an 18-foot median and 4-foot sidewalk on the east side of the road. Approaching Tradition Boulevard, the southbound approach on Sinclair Road narrows down to one lane. The existing typical cross-section for Tradition Boulevard is two 12-foot, undivided lanes with a 9-foot sidewalk on one side of the road. Tradition Boulevard has a gate entrance for Reunion, which is located approximately 1,200 feet from Sinclair Road.

Two intersections are included in the study area: 1) Sinclair Road and Tradition Boulevard, and 2) Goodman Road and Bella Citta Boulevard. The intersection of Sinclair Road & Tradition Boulevard currently operates as a free-flow intersection with no conflicting movements with the exception of Uturning movements. The intersection of Goodman Road and Bella Citta Boulevard operates as an unsignalized T-intersection with Bella Citta Boulevard as a stop-controlled approach. Bella Citta Boulevard is a two-lane undivided roadway with a 12-foot westbound lane, an 11-foot eastbound lane, a 4-foot bicycle lane in the westbound direction, and a 5-foot sidewalk on the north side of the road. Goodman Road is a two-lane undivided roadway with 12-foot lanes south of Bella Citta Boulevard and 10-foot lanes north of Bella Citta Boulevard.

Exhibit 2 illustrates existing geometry at each of the study intersections.

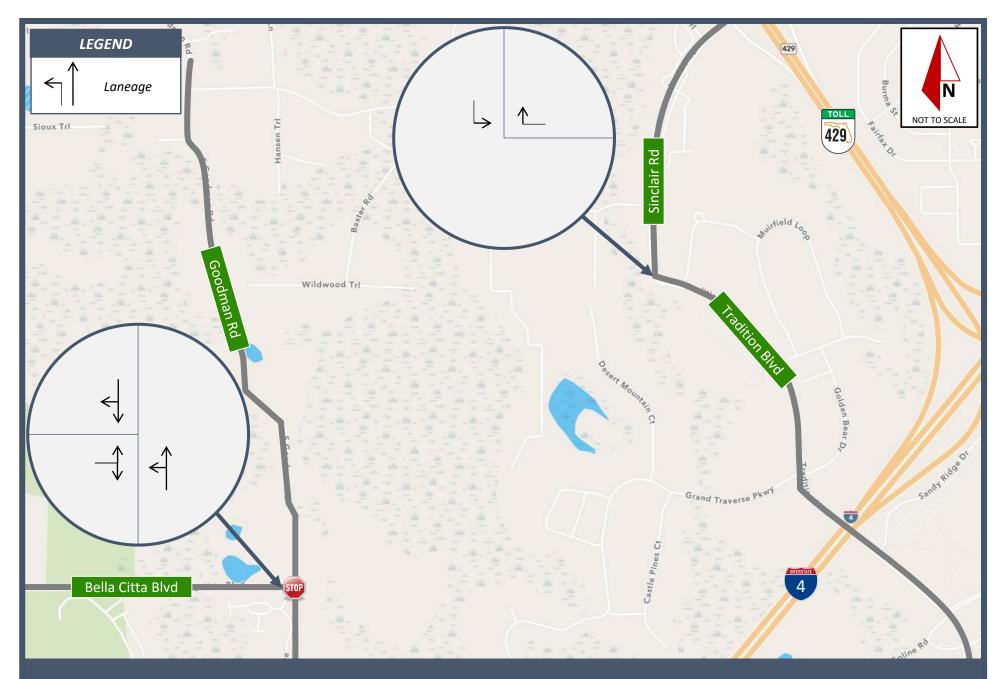


Exhibit 2: Existing (2021) Intersection GeometrySinclair Road Extension | Project Traffic Analysis Report (PTAR)

4.3 EXISTING TRAFFIC VOLUMES

Existing traffic data was obtained from Osceola County's Traffic report and by conducting 72-hour bidirectional traffic counts collected from Tuesday, November 16, 2021, to Thursday, November 18, 2021, at the locations listed in **Table 3**. **Table 4** provides a summary of the existing volumes, Annual Average Daily Traffic (AADT) volumes, along with other roadway characteristics. The D-factors were calculated based on the hourly volume count data. Standard K-factors were used based on the area type. **Appendix B** provides the raw volume counts data. Data referenced from the Florida Department of Transportation (FDOT) Florida Traffic Online (FTO) database is included in **Appendix C**. **Exhibit 3** illustrates the existing AADT on the study roadways.

Table 4: Existing (2021) Roadway Characteristics

| Roadway Segment | Ave | erage Daily | Traffic (Al | DT) ¹ | Seasonal Adj. Factor ² | Existing | Two Way | Peak Hour | Peak Hour | Measured | |
|-----------------------------------|--------|-------------|-------------|------------------|-----------------------------------------|-------------------|----------------------------------|-----------|-----------|-----------------------|----------|
| | Day 1 | Day 2 | Day 3 | Average | | AADT ³ | Peak Hour Vol. ^{1,4} | NB/EB | SB/WB | D-Factor ⁵ | K-Factor |
| Happy Trails | | | | | | | | | | | |
| west of Sinclair Road | 820 | 794 | 869 | 828 | | 800 | 70 | 47 | 23 | 67% | |
| Traditions Boulevard | | | | | | | | | | | |
| east of Sinclair Road | 3,480 | 3,484 | 4,062 | 3,675 | | 3,500 | 345 | 132 | 213 | 62% | |
| Sinclair Road | | | | | | | | | | | |
| east of Goodman Road | - | - | - | - | | - | - | - | - | - | |
| north of Tradition Boulevard | 3,480 | 3,484 | 4,062 | 3,675 | | 3,500 | 345 | 132 | 213 | 62% | |
| east of SR 429 | - | - | - | - | | 11,500 | 956 | 462 | 494 | 52% | |
| Bella Citta Boulevard | | | | | | | | | | | |
| west of S Goodman Road | 9,129 | 9,005 | 10,077 | 9,404 | 0.96 | 9,000 | 740 | 410 | 330 | 55% | 9% |
| S Goodman Road | | | | | 0.96 | | | | | | 9% |
| north of Bella Citta Boulevard | 4,524 | 4,308 | 4,849 | 4,560 | | 4,400 | 446 | 124 | 322 | 72% | |
| south of Bella Citta Boulevard | 11,115 | 11,091 | 12,071 | 11,426 | | 11,000 | 987 | 351 | 636 | 64% | |
| Master Boulevard | | | | | | | | | | | |
| north of Champions Gate Boulevard | - | - | - | - | | 12,000 | 987 | 351 | 636 | 64% | |
| Champions Gate Boulevard | | | | | | | | | | | |
| east of Masters Boulevard | - | - | - | - | | 31,500 | 1,793 | 853 | 940 | 52% | |
| S Old Lake Wilson Road | | | | | | | | | | | |
| north of Sinclair Road | - | - | - | - | | 20,000 | 1,669 | 741 | 928 | 56% | |
| south of Sinclair Road | - | - | - | - | | 18,000 | 1,766 | 713 | 1053 | 60% | |

Notes:

4.4 YEAR 2021 TURNING MOVEMENT COUNTS

Intersection turning movement counts were conducted for each of the study intersections for 8-hour periods on Tuesday, November 16, 2021. Traffic count data were adjusted using the latest seasonal factor (SF) published in the FTO database for the week turning movement counts were collected. Intersection volume development worksheets are provided in **Appendix D**. **Exhibit 4** illustrates the adjusted existing 2021 turning movement volumes.

^{1.} From traffic data collection.

^{2.} Per FDOT's Florida Traffic Online (FTO) database for Osceola County.

^{3.} Annual Average Daily Traffic (AADT) obtained from Osceola County Roadway Network Capacity Report and traffic counts.

^{4.} Volumes obtained from Osceola County 2021 Roadway Network Capacity Report.

^{5.} D-Factor calculated for the highest peak hour (PM period).

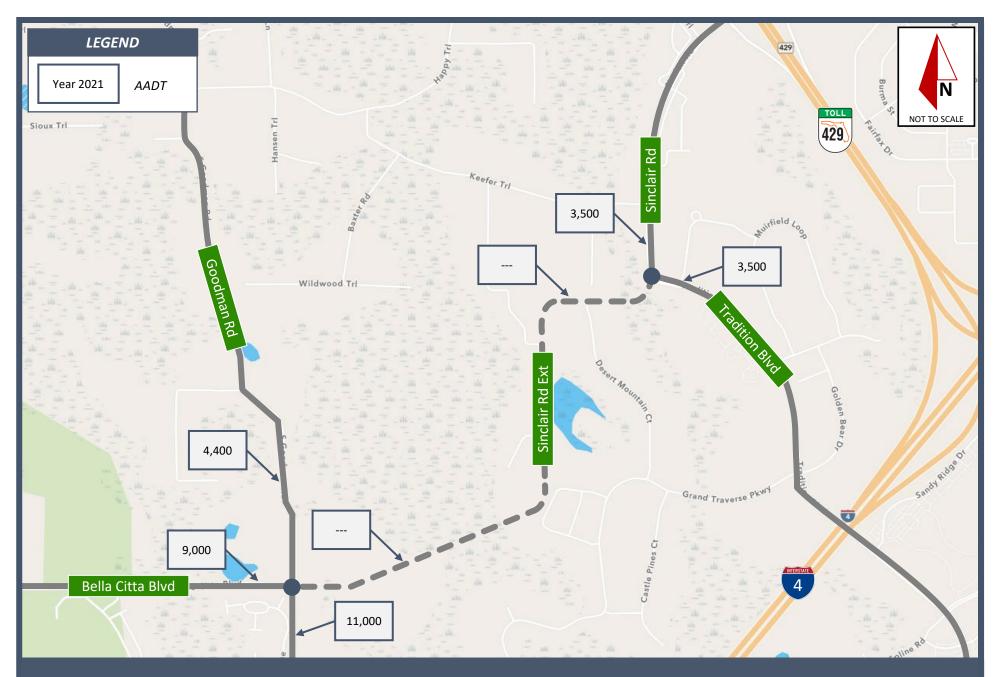


Exhibit 3: Existing (2021) Annual Average Daily Traffic (AADT) Sinclair Road Extension | Project Traffic Analysis Report (PTAR)

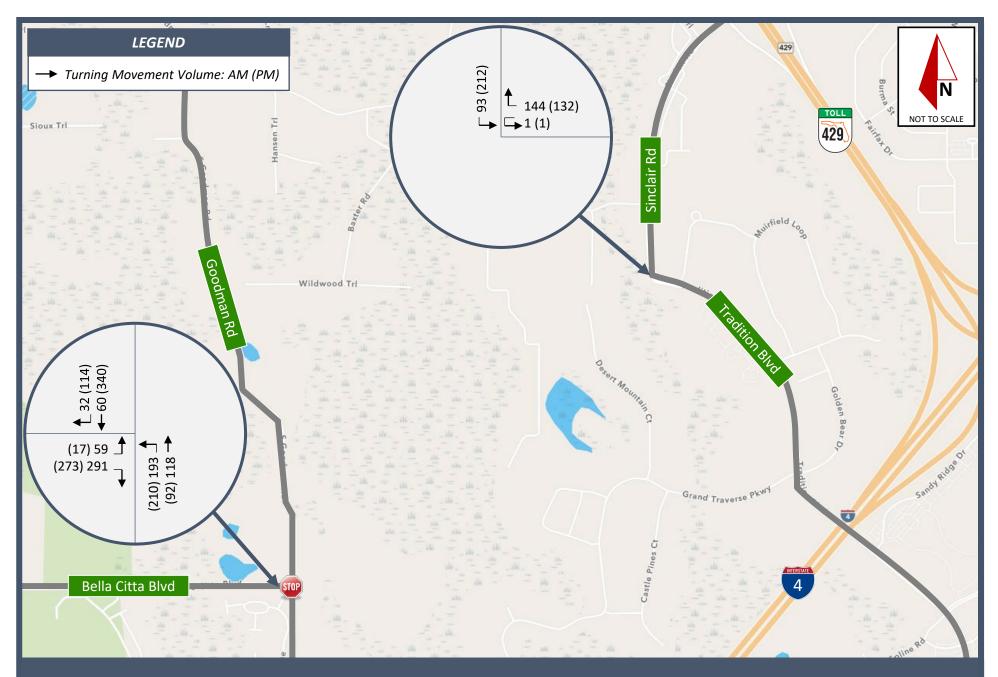


Exhibit 4: Existing (2021) Intersection Turning Movement Volumes
Sinclair Road Extension | Project Traffic Analysis Report (PTAR)

4.5 YEAR 2021 LEVEL OF SERVICE ANALYSIS

Existing intersection capacity analysis was conducted for each of the study area intersections. Roadway segment arterial performance was not calculated for the proposed Sinclair Road Extension since it does not exist at this time.

4.5.1 YEAR 2021 ROADWAY LEVEL OF SERVICE ANALYSIS

Existing traffic volume, operating conditions, LOS, and V/C ratios were identified from Osceola County's 2021 Roadway Network Capacity Report, included in **Appendix E**. Existing traffic volumes were also supplemented with traffic counts conducted for this study. LOS capacities were reviewed to be consistent with FDOT 2020 generalized service volume Quality/Level of Service (QLOS) tables. **Table 5** shows the peak hour peak direction (PHPD) volume, LOS, and V/C ratios for the study roadways.

Table 5: Existing (2021) Roadway Segment Performance Summary

| Dood.vov.Commont | Laura | Target LOS | LOS | Existing year 2021 | | | | |
|-----------------------------------|-------|------------|----------|--------------------|------|-----|--|--|
| Roadway Segment | Lanes | Standard | Capacity | PHPD | V/C | LOS | | |
| Happy Trail | | | | | | | | |
| west of Sinclair Road | 2 | Е | 570 | 47 | 0.08 | С | | |
| Traditions Boulevard | | | | | | | | |
| east of Sinclair Road | 2 | Е | 570 | 213 | 0.37 | С | | |
| Sinclair Road | | | | | | | | |
| east of Goodman Road | - | - | - | - | - | F | | |
| north of Tradition Boulevard | 4 | Е | 1,680 | 213 | 0.13 | С | | |
| east of SR 429 | 4 | Е | 1,680 | 494 | 0.29 | С | | |
| Bella Citta Boulevard | | | | | | | | |
| west of S Goodman Road | 2 | Е | 570 | 410 | 0.72 | D | | |
| S Goodman Road | | | | | | | | |
| north of Bella Citta Boulevard | 2 | D | 790 | 322 | 0.41 | С | | |
| south of Bella Citta Boulevard | 2 | D | 790 | 636 | 0.81 | С | | |
| Master Boulevard | | | | | | | | |
| north of Champions Gate Boulevard | 2 | D | 830 | 636 | 0.77 | С | | |
| Champions Gate Boulevard | | | | | | | | |
| east of Masters Boulevard | 4 | D | 1,530 | 940 | 0.61 | С | | |
| S Old Lake Wilson Road | | | | | | | | |
| north of Sinclair Road | 4 | D | 1,760 | 928 | 0.53 | С | | |
| south of Sinclair Road | 2 | D | 790 | 1,053 | 1.33 | F | | |

4.5.2 YEAR 2021 INTERSECTION OPERATIONAL ANALYSIS

Intersection operational analyses were conducted for the existing 2021 AM and PM peak hours conditions using procedures outlined in the Highway Capacity Manual 6th Edition with Synchro (v11) software. Synchro outputs are included in **Appendix F**.

As shown in **Tables 6 and 7** below, both intersections are shown to operate acceptably during the AM and PM peak hour conditions.

Table 6: Existing (2021) Intersection Performance – AM Peak Hour

| Intersection | MOE | E | astbour | nd | W | estbou | nd | No | orthbou | nd | So | uthbou | nd | Overall |
|-------------------------------|----------------|------|---------|-------|------|--------|-------|------|---------|-------|------|--------|-------|---------|
| intersection | IVIOE | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| Cinalaia Baad @ | Delay | | | | | | 0.0 | - | | | 0.0 | | | 0.0 |
| Sinclair Road @ Tradition | LOS | | | | | | Α | | | | Α | | | |
| Boulevard | V/C | | | | | | 0.0 | | | | 0.0 | | | |
| (Unsignalized) | Queue (veh) | 1 | | | 1 | | 0 | 1 | | | 0 | | | |
| Delle Citte | Delay | 16.7 | | 16.7 | | | - | 7.9 | 0.0 | - | - | 0.0 | 0.0 | 9.8 |
| Bella Citta Boulevard @ | LOS | С | | С | | | | Α | Α | | | Α | Α | |
| Goodman Road (Unsignalized | V/C | 0.59 | | 0.59 | | | | 0.16 | 0.0 | | | 0.0 | 0.0 | |
| | Queue (veh) | 4 | | 4 | | | | 1 | 0 | | | 0 | 0 | |

Table 7: Existing (2021) Intersection Performance – PM Peak Hour

| Intersection | MOE | E | Eastbound | | | Westbound | | | Northbound | | | Southbound | | |
|--------------------------------|----------------|------|-----------|-------|------|-----------|-------|------|------------|-------|------|------------|-------|---------|
| intersection | IVIOE | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| Civilate Based C | Delay | | | | | | 0.0 | | | | 0.0 | | | 0.0 |
| Sinclair Road @ Tradition | LOS | | | | | | Α | | | | Α | | | |
| Boulevard | V/C | | | | | | 0.0 | | | | 0.0 | | | |
| (Unsignalized) | Queue (veh) | | | | | | 0 | | | | 0 | | | |
| Dalla Citta | Delay | 20.3 | | 20.3 | | | | 9.3 | 0.0 | | | 0.0 | 0.0 | 7.5 |
| Bella Citta Boulevard @ | LOS | С | | С | | | | Α | Α | | | Α | Α | |
| Goodman Road (Unsignalized) | V/C | 0.59 | | 0.59 | | | | 0.22 | 0.0 | | | 0.0 | 0.0 | |
| | Queue (veh) | 4 | | 4 | | | | 1 | 0 | | | 0 | 0 | |

5.0 SAFETY ANALYSIS

Historical crash data were obtained at the study intersections for a five-year period from January 1, 2016, to December 31, 2020. The crash data was obtained from the University of Florida's Signal Four Analytics online crash database, which compiles statewide crash data from the Florida Highway Patrol (FHP) and local law enforcement agencies. The data was analyzed to identify specific crash patterns and locations that may indicate a potential safety problem within the study area. The proposed roadway extension was also reviewed to identify any potential safety implications to the corridor. The study area includes the intersections of Sinclair Road and Tradition Boulevard, and Goodman Road and Bella Citta Boulevard. All identified crashes were reviewed; summary crash data tables are included in **Appendix G**.

5.1 EXISTING CRASH DATA STATISTICS

A total of nine (9) crashes were reported for the five-year period, of which only one involved an injury. Five crashes occurred at night, and four occurred during the day, all under clear and dry weather conditions. All of the crashes that occurred at the intersection of Sinclair Road and Tradition Boulevard involved one vehicle impacting roadway infrastructure (e.g., utility pole, guardrail, traffic sign, etc.). Crashes located at the intersection of Goodman Road and Bella Citta Boulevard involved two vehicles. **Table 8** summarizes the total number of crashes that occurred within the study area.

| Year | | ımber of shes | | ber of Crashes | | of Dark shes | | Number of Off- Road Crashes | | |
|------------------|-----|------------------|-----|-------------------|------|-----------------|------|--------------------------------|--|--|
| | #1 | #2 | #1 | #2 | #1 | #2 | #1 | #2 | | |
| 2016 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | | |
| 2017 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | | |
| 2018 | 2 | 0 | 1 | 0 | 2 | 0 | 2 | 0 | | |
| 2019 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| 2020 | 2 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | | |
| Total | 4 | 5 | 1 | 0 | 4 | 1 | 4 | 1 | | |
| Average per year | 0.8 | 1 | 0.2 | 0 | 0.8 | 0.2 | 0.8 | 0.2 | | |
| Perc | ent | | 25% | 0% | 100% | 20% | 100% | 20% | | |

Table 8: Summary of Crashes

Note:

#1 Sinclair Road & Tradition Boulevard intersection

#2 Bella Citta Boulevard & Goodman Road intersection

5.2 EXISTING CRASH DATA BY CRASH TYPE

The crash data was organized to determine any significant trend in the circumstances involved in the crashes. The crash data was organized by crash type throughout the five-year study period. As shown in **Table 9**, approximately 55.6% of crashes were off-road (run-off-the-road) crashes.

Table 9: Summary of Crashes by Type

| Crash | 2016 | | 2017 | | 2018 | | 2019 | | 2020 | | Total | | Percent | |
|-----------|------|----|------|----|------|----|------|----|------|----|-------|----|---------|-----|
| Type | #1 | #2 | #1 | #2 | #1 | #2 | #1 | #2 | #1 | #2 | #1 | #2 | #1 | #2 |
| Left Turn | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0% | 40% |
| Off-Road | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 4 | 1 | 100% | 20% |
| Rear End | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0% | 20% |
| Sideswipe | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0% | 20% |

Note:

5.3 EXISTING CRASH DATA BY INTERSECTIONS

Four (4) crashes were reported at the intersection of Sinclair Road and Tradition Boulevard within the five-year period. All crashes reported at this intersection were off-road crashes. The off-road crashes occurred by vehicles approaching the curve where Sinclair Road meets Tradition Boulevard and losing control. These types of crashes were shown to occur early in the day (between 3:00 AM and 8:00 AM) and late at night after 10:00 PM. These crashes occurred during clear weather and dry surface conditions. Potential contributing factors to the occurrence of crashes at this intersection are listed below:

- Intersection lighting may not be adequate,
- Retroreflective signage may not be adequate,
- Lack of appropriate warning signage, and steep slope

Five (5) crashes were reported at the intersection of Goodman Road and Bella Citta Boulevard within the five-year period. Two (2) left turn crashes were reported to be caused by vehicles performing a left turn movement from Goodman Road onto Bella Citta Boulevard and colliding with a vehicle on the conflicting movement. One of the crashes involved a minor street movement, and the other crash involved a major street movement. Potential contributing factors to the occurrence of crashes at this intersection are listed below:

- Unprotected movements for all approaches,
- Gaps along the major approach may be difficult to find or judge during peak times, and
- Narrow north leg at Goodman Road with minimal clearance

The other three (3) crashes were off-road, sideswipe, and rear-end. All of these crashes occurred during clear and dry conditions, except for the sideswipe which occurred during cloudy weather.

5.4 EXISTING CRASH DATA BY SEGMENTS

Crashes along the Sinclair Road Extension were predicted based on the Highway Safety Manual (HSM) methodology, as shown in the subsequent section.

5.5 OVERVIEW OF FATAL CRASHES

No fatal crashes were reported within the study area intersections.

^{#1} Sinclair Road & Tradition Boulevard intersection

^{#2} Bella Citta Boulevard & Goodman Road intersection

5.6 CRASH FREQUENCY AND CRASH RATE DEVELOPMENT

The crash rates and crash frequencies (crashes per year) at the study area intersections were developed based on the five-year crash data. The crash rates are expressed in the number of crashes per million vehicles entered (million entering vehicles [MEV]), based on the following equations:

$$MEV = \frac{Total\ Entering\ Volume\ imes 365 imes Number\ of\ Years}{1,000,000}$$

$$Crash\ Rate = \frac{Number\ of\ Crashes\ per\ n\ Years}{MEV}$$

The total entering volumes (TEV) were developed by averaging the total entering volume for the three-day period that data was collected and adjusting it by the seasonal factor as provided by FDOT's FTO database. As shown in **Table 10**, the intersection of Goodman Road and Bella Citta Boulevard has a slightly higher crash frequency and a lower crash rate than the intersection of Sinclair Road and Tradition Boulevard. Statewide average crash rates were obtained from FDOT's Crash Analysis Reporting (CAR) System database. As shown in **Table 10**, the intersection of Goodman Road and Bella Citta Boulevard has a slightly lower crash rate than the statewide average for a similar area and facility type; however, the crash rate for the intersection of Sinclair Road and Tradition Boulevard is significantly higher than the statewide average. See Section 5.3 regarding potential contributing factors.

Table 10: Crash Frequency and Crash Rate Summary

| | Intersection TEV | | Number of Crashes | Crash Frequency (Crashes per Year) | Crash Rate | Statewide Average Crash Rate | |
|---|-------------------------------------------|--------|----------------------|---------------------------------------------|------------|------------------------------------|--|
| 1 | Sinclair Road and Tradition Boulevard | 3,528 | 4 | 0.8 | 0.62 | 0.29 | |
| 2 | Goodman Road and Bella Citta Boulevard | 12,187 | 5 | 1.0 | 0.22 | 0.29 | |

6.0 DEVELOPMENT OF DESIGN TRAFFIC CHARACTERISTICS

Design traffic characteristics were developed in accordance with the Project Traffic Forecasting (PTF) Handbook, January 2019. The primary design characteristics are the Peak Hour Factor (PHF), the standard K-factor, the D-factor, and the percentage of trucks for both the design hour and daily conditions (T_f , T_{24}). These characteristics were used in developing future traffic volumes and conducting future operational analyses.

6.1 STANDARD K-FACTOR

The K-factor defines the proportion between the design hour volume (DHV) and daily volume. As explained in the PTF Handbook, the K-factor "defines the volume of traffic for which the road is designed to handle." FDOT has adopted a standard K-factor to use in analyses based on area and facility type. For arterials and highways within an urbanized area, the standard K-factor is 9.0%. Therefore, a K-factor of 9.0% was used.

6.2 D-FACTOR

The D-factor is used to determine the directional split of traffic during the design hour. The D-factors were calculated for all approaches of the study intersections, which were obtained from the traffic counts and are shown in the intersection volume development worksheet in **Appendix D**. FDOT's PTF Handbook recommends a range of D-factors based on the facility type.

The calculated D-factors for the existing portion of Sinclair Road and Bella Citta Boulevard, previously shown in **Table 4**, which will be part of the main corridor, fall within the FDOT recommended D values. The calculated D-factors were used in the analysis, with a D-factor of 61.0% used for Sinclair Road Extension. A D-factor of 53% was used for the westbound approach during the PM peak hour at the intersection of Sinclair Road/Bella Citta Boulevard & Goodman Road. During the AM peak hour, the peak direction along Sinclair Road is the northbound approach and the during the PM peak hour the peak direction is the southbound approach. Similar distribution can be observed along Goodman Road during the peak periods. Bella Citta Boulevard's peak direction during the AM and PM peak hours are the westbound and eastbound approaches, respectively.

6.3 T FACTORS

Truck percentages were calculated for both daily (T_{24}) and peak hour (T_f) conditions at the study intersections. The T_f is estimated to be at least half of T_{24} . Based on the collected traffic counts, the truck percentage during the peak hour at the intersection of Sinclair Road and Tradition Boulevard was 5%. Therefore, it can be assumed the daily truck percentage is 10% at this intersection. During the peak hour at the intersection of Goodman Road and Bella Citta Boulevard, the truck percentage was 2.6%. Therefore, it can be assumed the daily truck percentage is 5.2% at this intersection. The truck percentages for all intersection movements were calculated and are shown in the intersection volume development worksheet. A minimum truck percentage of 2% was utilized for the operational analysis. The truck factor for the Sinclair Road Extension was assumed as the average of both intersections, which results in a peak hour truck percentage (T_f) of 3.5% and a daily truck percentage (T_{24}) of 7.0%. This is consistent with the recommendation from the PTF Handbook that the T_f value should be at least half of the T_{24} .

6.4 RECOMMENDED DESIGN TRAFFIC CHARACTERISTICS

The recommended design traffic characteristics for Sinclair Road Extension are identified in **Table 11**. These are based on a review of FDOT recommended values and measured design traffic characteristics.

Table 11: Recommended Design traffic Characteristics

| Roadway Segment | K-Factor | D-Factor | T ₂₄ Factor | T _f Factor |
|-------------------------|----------|----------|------------------------|-----------------------|
| Sinclair Road Extension | 9.0% | 61.0% | 7.0% | 3.5% |

7.0 SUB-AREA MODEL VALIDATION

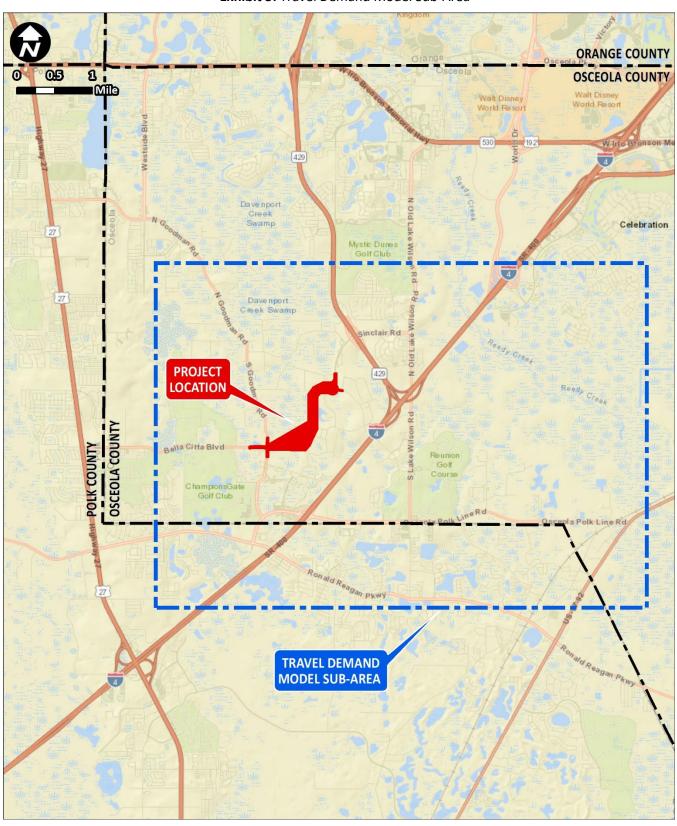
7.1 INTRODUCTION

A sub-area model validation analysis was performed to determine the accuracy of the travel demand within and adjacent to the study area. Base Year 2015 model volumes were compared to historical 2015 AADT. Model outputs were analyzed and considered when developing Design Year 2045 volumes. The travel demand model sub-area is shown on **Exhibit 5**.

7.2 BASE YEAR 2015 MODEL VALIDATION

Model validation was performed to ensure that the model is accurate enough to forecast reasonable roadway daily volumes. The accuracy of the model was assessed by calculating validation criteria, such as V/C ratio and root mean square error (RMSE).

Exhibit 5: Travel Demand Model Sub-Area



7.2.1 BASE YEAR 2015 MODEL ADJUSTMENTS

Raw Base Year 2015 model volumes were extracted and adjusted by applying a Model Output Conversion Factor (MOCF) of 0.91 for Osceola County as provided in FDOT's FTO database, resulting in the 2015 Model Volume. The model underrepresented the volumes along Goodman Road south of Bella Citta Boulevard and along Bella Citta Boulevard west of Goodman Road with a volume-to-count (VoC) ratio of 0.50. The model also underrepresented the volume along Masters Boulevard with a VoC ratio of 0.50, and overrepresented the volume along Goodman Road north of Bella Citta Boulevard with a VoC ratio of 4.14, as shown in **Table 12**. These observations were considered when developing future year 2045 volumes, as described in the subsequent section. No adjustments were made in the model to roadway segment attributes (speed, area type, facility type, etc.).

7.2.2 BASE YEAR 2015 MODEL VALIDATION RESULTS

As shown in **Table 12**, the 2015 model shows higher volumes along most of the roadway segments. The overall percent deviation of the travel demand model sub-area is 12%, with an overall volume-to-count of 1.12.

Table 12: Comparison of Model Volumes to Actual Traffic Count Data

| Roadway Segment | Raw 2015 2015 Model Model Vol. Vol. | | Historical 2015 AADT | 2015 Volume Diff. (Hist. AADT - Model Vol.) | 2015 Model Vol./ 2015 Count | Percent Deviation |
|-----------------------------------|----------------------------------------|--------|-------------------------|------------------------------------------------------|-----------------------------------|----------------------|
| Happy Trail | | | | | | |
| west of Sinclair Rd | 2,983 | 2,700 | - | - | - | - |
| Tradition Boulevard | | | | | | |
| east of Sinclair Road | 2,272 | 2,100 | - | - | - | - |
| Sinclair Road | | | | | | |
| east of Goodman Road | - | - | - | - | - | - |
| north of Tradition Boulevard | 2,272 | 2,100 | - | - | - | - |
| east of SR 429 | 8,255 | 7,500 | 4,200 | -3,300 | 1.79 | 79% |
| Bella Citta Boulevard | | | | | | |
| west of Goodman Road | 2,637 | 2,400 | 4,800 | 2,400 | 0.50 | -50% |
| Goodman Rd | | | | | | |
| north of Bella Citta Blvd | 3,216 | 2,900 | 700 | -2,200 | 4.14 | 314% |
| south of Bella Citta Blvd | 2,788 | 2,500 | 8,000 | 5,500 | 0.31 | -69% |
| Masters Boulevard | | | | | | |
| north of Champions Gate Boulevard | 4,353 | 4,000 | 8,000 | 4,000 | 0.50 | -50% |
| Champions Gate Boulevard | | | | | | |
| east of Masters Boulevard | 25,236 | 23,000 | 17,500 | -5,500 | 1.31 | 31% |
| S Old Lake Wilson Road | | | | | | |
| north of Sinclair Road | 16,270 | 15,000 | 12,000 | -3,000 | 1.25 | 25% |
| south of Sinclair Road | 20,858 | 19,000 | 13,000 | -6,000 | 1.46 | 46% |
| Overall | 83,613 | 76,300 | 68,200 | | 1.12 | 12% |

Exhibit 6 shows a comparison of the base year 2015 model volumes and historical 2015 volumes at the study area intersections' approaches. **Appendix H** includes base year (2015) model volumes.

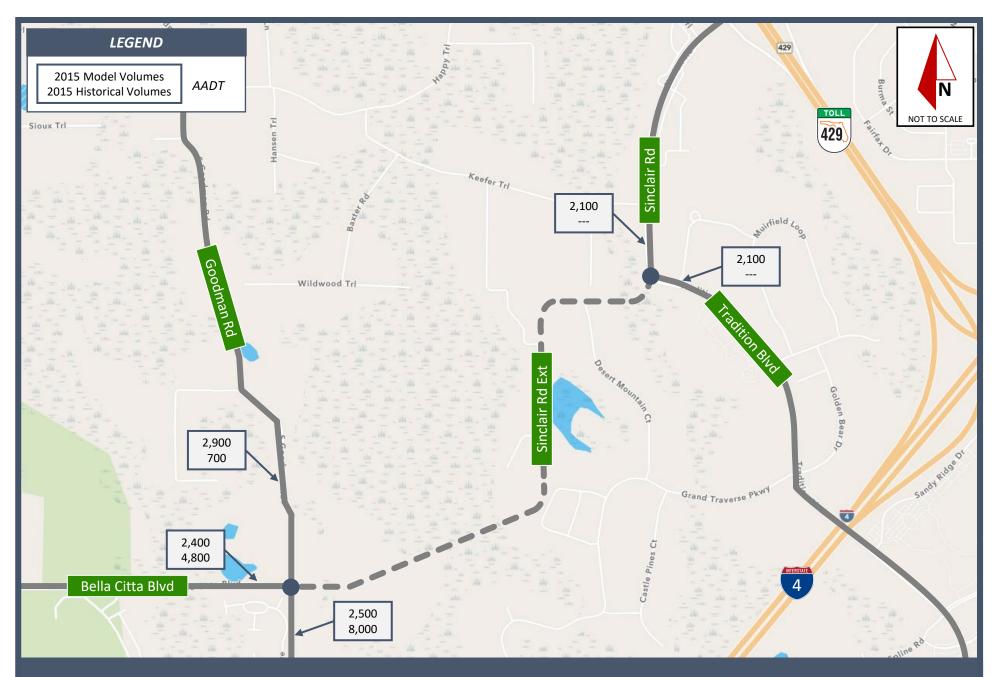


Exhibit 6: Year 2015 Volume Comparison
Sinclair Road Extension | Project Traffic Analysis Report (PTAR)

7.2.3 ROOT MEAN SQUARE ERROR

The percent RMSE quantifies the difference between the model volumes and traffic counts. The RMSE is a measure of dispersion, and it tends to normalize model error better than volume-to-count ratios that allow for high ratios to offset low ratios. 2015 model volumes (prior to any adjustments beyond applying the MOCF) were used to develop the areawide RMSE. As shown in **Table 13**, the areawide RMSE is 22% higher than the acceptable standard. Preferred and acceptable RMSE standards were obtained from Table 3-2 of the FDOT Project Traffic Forecasting Handbook (2019). This deviation in the model was considered when generating 2045 model volumes.

| Volume Croun | Count | Model | RMSE | Sta | andard | Sample |
|-----------------|--------|--------|--------|-----------|------------|--------|
| Volume Group | AADT | AADT | RIVISE | Preferred | Acceptable | Size |
| Less than 5,000 | 16,500 | 19,500 | 65% | 45% | 100% | 6 |
| 5,000 - 9,999 | 20,000 | 14,000 | 65% | 35% | 45% | 3 |
| 10,000 - 14,999 | 25,000 | 19,000 | 76% | 27% | 35% | 2 |
| 15,000 - 19,999 | 30,500 | 42,000 | 38% | 25% | 30% | 2 |
| 20,000 - 29,999 | 17,500 | 23,000 | 31% | 15% | 37% | 1 |
| 30,000 - 49,999 | 0 | 0 | n/a | 15% | 25% | 0 |
| 50,000 - 59,999 | 0 | 0 | n/a | 10% | 20% | 0 |
| Over 60,000 | 0 | 0 | n/a | 10% | 19% | 0 |
| RMSE Areawide | 93,000 | 98,000 | 67% | 35% | 45% | |

Table 13: Percent Root Mean Square Error by Volume Group

7.3 BASE YEAR 2015 MODEL VALIDATION CONCLUSION

The Base 2015 model for CRFPMv7 was reviewed and compared against historic counts within the study area to model volumes. Most of the regional roadways within the study area (i.e., I-4, SR 429, CR 532/Champions Gate Boulevard, and CR 545/Old Lake Wilson Road) were shown to have reasonable 2015 volume-to-count ratios so the model was not recalibrated. The model did show low volumes along Goodman Road south of Bella Citta Boulevard, and Bella Citta Boulevard west of Goodman Road, when compared to limited 2015 count data. Recalibration of these roads would have negatively impacted well-calibrated regional roads; therefore, no modifications were performed to the Base 2015 model network. There were also no modifications made to TAZs within the study area to avoid affecting the model's calibration. Instead, the 2045 Cost Feasible model results were adjusted to address model underrepresentation on Goodman Road and Bella Citta Boulevard (See Section 8.4).

The overall percent deviation for the travel demand sub-area is 12%, with an overall volume-to-count ratio of 1.12. As stated in the FDOT Project Traffic Forecasting (PTF) Handbook, the acceptable volume-to-count ratio for arterial roadways is ±15%. For collector roads, a larger difference of ±25% is acceptable. The areawide RMSE for the travel demand sub-area is 67%, 20% higher than the acceptable standard. These observations were considered when developing year 2045 volumes, as described in the subsequent section. No modifications were performed to the base year 2015 model. 2045 Build volumes were carefully adjusted to consider the results from the Base Year 2015 model as described in Section 8.4.

8.0 FUTURE TRAFFIC FORECASTS

8.1 STUDY ALTERNATIVES

Two Cost Feasible (CF) 2045 models were run to determine the impacts of the Sinclair Road extension: a No-Build Scenario (without Sinclair Road Extension) and a Build scenario (with the Sinclair Road extension). This study evaluates a Build alternative for the Opening (2025) and Design (2045) years. Both the No-Build and Build model runs included all modifications made to the CF 2045 model as described in the subsequent sections. The Build alternative consisted of Sinclair Road as a 4-lane road extending from Tradition Boulevard to the intersection of Goodman Road and Bella Citta Boulevard.

8.2 TRAVEL DEMAND MODEL

The latest adopted Central Florida Regional Planning Model (CFRPM) version 7 was used to forecast unadjusted Design Year 2045 daily traffic volumes at the future intersection approaches. Adjustments to the model outputs were performed based on a review of the Base Year 2015 model, which was shown to underrepresent the volumes along some of the adjacent roadways. Adjusted volumes are shown on **Exhibit 6**. Model outputs for the No-Build and Build scenario are included in **Appendix H**.

8.2.1 NEARBY DEVELOPMENTS

The following nearby planned developments were identified within the study area:

- Reunion
- Goodman Road Charter School (850 students) in the northeast corner of the intersection of Goodman Road and Bella Citta Boulevard
- Elevation/Dewan Property (444 Multifamily Dwelling Units) located on the south side of the Sinclair Road Extension, east of Goodman Road
- Sinclair Road Property (446 Multifamily Dwelling Units, 3,500 square foot restaurant, and a 10-vehicle fueling positions gas station with convenience market) located in the southwest quadrant of the Sinclair Road interchange with SR 429
- Illuminate Church (42,000 square feet) located north of Sinclair Road, east of SR 429

8.2.2 SOCIOECONOMIC DATA

The Cost Feasible (CF) 2045 socioeconomic data (dwelling units, employment, etc.) in the 2045 model are approved by the metropolitan planning organizations (MPOs) and local governments. The socioeconomic data forecasts utilize the population forecasts developed by the Bureau of Economic and Business Research (BEBR) at the county level. These forecasts are spread across each County's TAZs based on assumptions by the local governments. With Osceola County's historic and projected high level of growth, some areas within the County are anticipated to have higher intensity and density of development in the future than what currently exists today. While it is recognized that not all the actual 2045 development will be located in the specific TAZs assumed, these forecasts are as accurate as possible given the available information at the time they are developed.

However, the Cost Feasible (CF) 2045 socioeconomic data (ZDATA) was reviewed to determine if all known existing and future developments were accounted for in the model. Upon review, the 2045 ZDATA sufficiently accounted for all planned developments in the area except for the Goodman Road Charter School. A separate TAZ (5525) was coded into the network with a connection to Goodman Road north of Sinclair Road to represent the school's access. The TAZ located south of Sinclair Road and north

of I-4 (5468) was divided into three separate TAZs (5468, 5526, and 5527) to better represent future developments' access points along Sinclair Road. The original model did not have any connections within the Reunion Development, which did not allow for internal circulation. The Reunion Development is a gated community and does not allow for background/cut-thru traffic between Tradition Boulevard and S Old Lake Wilson and Osceola Polk Line Road (CR 532). Tradition Boulevard currently provides access between the northern and southern portions of Reunion via an overpass on I-4 and allows for vehicles on either side of I-4 to access Sinclair Road, S Old Lake Wilson Road, and CR 532. The TAZ connectors for the Reunion Development (5468 and 5449) were modeled to represent the access points better and the internal circulation between the Reunion West and Reunion East while restricting cut-thru/background traffic through Reunion.

The TAZ and ZDATA edits are summarized in **Table 14** and the location of the modified TAZs is illustrated on **Exhibit 7**. Additionally, a technical memorandum, included in **Appendix I**, was performed further describing the socioeconomic adjustments to the model and illustrating how Reunion correlates to the model.

Employees Students **Dwelling Units** TAZ Hotel/Motel Commercial K-12 Single-Family Multifamily Service Industrial Revised Initial Revised Initial Revised Initial Initial Revised Initial Revised Initial Revised Initial Revised 5484 ¹ 5525 ² 5527 ³

Table 14: CF 2045 TAZ and ZDATA Revisions

8.2.3 PLANNED AND PROGRAMMED IMPROVEMENTS

Prior to conducting the CF 2045 No-Build and Build model runs, the roadway network was revised to determine if planned and programmed improvements were accounted for within the study area. The following revisions were made to the CF 2045 roadway network:

- The 2045 CF roadway network did not include the Poinciana Parkway Extension north of CR 532 (Osceola Polk Line Road) to the Interstate 4 (I-4)/SR 429 interchange; therefore, the connection from CR 532 and Interstate 4 (I-4)/SR 429 was coded into the network. The connection at the I-4/SR 429 interchange was assumed to be full access.
- Sinclair Road Extension was coded into the model as a 4-lane road with similar attributes to the existing portion of Sinclair Road north of Tradition Boulevard.
- A segment of Tradition Boulevard was added to the model to represent the existing/future T-intersection at Sinclair Road.

Notes:

^{1.} Planned Illuminate Church is accounted for within the initial 2045 ZDATA.

^{2.} New TAZ, split from 5483 for the planned Goodman Road Charter School (850 students) (includes a factor of 3.0 to align with ITE trip generation)

^{3.} New TAZ, split from 5468 for Dewan/Elevation (444 Multifamily DU) and Sinclair Road Property (446 Multifamily DU, 3.5 KSF restaurant, and 10 pump gas station) (includes a factor of 1.2 for TAZ 5526 and

 $^{{\}it 3.1 for TAZ\,5527\,to\,better\,reflect\,ITE\,estimated\,daily\,trips)}.$

^{*}Reunion TAZs are highlighted in blue.

• Westside Boulevard is planned to be fully connected to the north and south by the year 2045, and it was coded in the model as a 4-lane road connecting from and to Bella Citta Boulevard and Sand Mine Road. The modified roadway network is illustrated on **Exhibit 7**.

EQ. Sand Hill Rd Sinclair Rd Bella Citta Blvd

Exhibit 7: CF 2045 Modified TAZs and Roadway Network

8.2.4 MODEL-BASED GROWTH RATES

Table 15 shows a summary of the model-based growth rates derived using Base Year 2015 and Design Year 2045 volumes for the Build condition. As shown in the table below, the Sinclair Road Extension is shown to reduce traffic along some segments, such as Happy Trail, Goodman Road, Masters Boulevard, and Champions Gate Boulevard. Traffic along S. Old Lake Wilson Road is not shown to change much as a result of the Sinclair Road Extension.

Table 15: Model-Based Growth Rate Summary

| | | Year 2045 | 5 No Build | Year 20 | 45 Build | |
|-----------------------------------|----------------------|----------------|--------------------------|----------------------|--------------------------|----------------------|
| Roadway Segment | Vol. Adj. Model Grov | | Annual Growth Rate | Adj. Model Volume | Annual Growth Rate | Vol. % Difference |
| Happy Trail | | | | | | |
| west of Sinclair Rd | 2,700 | 11,500 | 4.9% | 10,500 | 4.6% | -9.5% |
| Tradition Boulevard | | | | | | |
| east of Sinclair Road | 2,100 | 10,500 | 5.5% | 12,000 | 6.0% | 12.5% |
| Sinclair Road | | | | | | |
| east of Goodman Road | - | - | - | 15,500 | - | - |
| north of Tradition Boulevard | 2,100 | 10,500 | 5.5% | 20,500 | 7.9% | 48.8% |
| east of SR 429 | 7,500 | 23,000 | 3.8% | 23,500 | 3.9% | 2.1% |
| Bella Citta Boulevard | | | | | | |
| west of Goodman Road | 2,400 | 5 <i>,</i> 700 | 2.9% | 12,500 | 5.7% | 54.4% |
| Goodman Rd | | | | | | |
| north of Bella Citta Blvd | 2,900 | 6,000 | 2.5% | 5,000 | 1.8% | -20.0% |
| south of Bella Citta Blvd | 2,500 | 9,300 | 4.5% | 8,800 | 4.3% | -5.7% |
| Masters Boulevard | | | | | | |
| north of Champions Gate Boulevard | 4,000 | 13,000 | 4.0% | 10,000 | 3.1% | -30.0% |
| Champions Gate Boulevard | | | | | | |
| east of Masters Boulevard | 23,000 | 36,500 | 1.6% | 35,000 | 1.4% | -4.3% |
| S Old Lake Wilson Road | | | | | | |
| north of Sinclair Road | 15,000 | 42,000 | 3.5% | 42,000 | 3.5% | 0.0% |
| south of Sinclair Road | 19,000 | 40,000 | 2.5% | 40,000 | 2.5% | 0.0% |

8.2.5 BEBR GROWTH RATES

The University of Florida's Bureau of Economics and Business Research (BEBR) projections were obtained for Osceola County to develop the annual growth rates for the Design year 2045. BEBR low, medium, and high population projections were considered in the development of the design year 2045 Build volumes. **Table 16** shows the BEBR population growth rates. An excerpt of the BEBR population projection data referenced (Volume 54, Bulletin 198, April 2021) is included as **Appendix J**. The growth rate was calculated using the Compound Annual Growth Rate (CAGR) equation.

Table 16: BEBR Population Growth Rates

| County | BEBR Pop Estimate | BEBR Po | Growth Rate (CAGR) | | | |
|---------|----------------------|---------|-----------------------|-------|--|--|
| | April 1, 2020 | Range | 2045 | 2045 | | |
| | | Low | 518,300 | 1.17% | | |
| Osceola | 387,055 | Medium | 643,100 | 2.05% | | |
| | | High | 798,500 | 2.94% | | |

Source: BEBR Volume 54, Bulletin 198, April 2021 (page 8).

8.3 HISTORICAL TRAFFIC TRENDS

Historical AADT was obtained from Osceola County's traffic count database and FDOT's FTO database. Historical AADT was obtained for five years, from 2015 to 2019, as available. 2020 AADT was not considered due to the impact on travel patterns caused by the COVID-19 pandemic. Historical growth trends were determined based on a linear trend. **Table 17** shows a summary of the annual growth trend to Design Year 2045 for the roadway segments within the study area. **Appendix K** shows the trend analysis spreadsheet.

Table 17: Trend-Based Growth Rates

| Roadway Segment | Count Sta. | 2015 | 2016 | 2017 | 2018 | 2019 | R ² | Annual Growth Rate |
|-----------------------------------|---------------|--------|--------|--------|--------|--------|----------------|--------------------------|
| Happy Trail | | | | | | | | |
| west of Sinclair Rd | - | - | - | - | - | - | - | - |
| Tradition Boulevard | | | | | | | | |
| east of Sinclair Road | - | - | - | - | - | - | - | - |
| Sinclair Road | | | | | | | | |
| east of Goodman Road | - | - | - | - | - | - | - | - |
| north of Tradition Boulevard | - | - | - | - | - | - | - | - |
| east of SR 429 | 106 | 4,171 | 5,852 | 6,138 | 6,636 | 8,728 | 90.0% | 11.9% |
| Bella Citta Boulevard | | | | | | | | |
| west of Goodman Road | 927084 | 4,800 | 6,000 | 5,400 | 5,600 | 5,800 | 30.2% | 2.8% |
| Goodman Rd | | | | | | | | |
| north of Bella Citta Blvd | 126 | 698 | 1,836 | 2,537 | 2,886 | 3,207 | 93.3% | 18.0% |
| south of Bella Citta Blvd | 921087 | 5,200 | 5,400 | 6,700 | 6,900 | 7,100 | 88.6% | 7.3% |
| Masters Boulevard | | | | | | | | |
| north of Champions Gate Boulevard | 121 | 8,039 | 7,746 | 8,995 | 9,942 | 9,586 | 78.1% | 5.5% |
| Champions Gate Boulevard | | | | | | | | |
| east of Masters Boulevard | 928034 | 17,300 | 17,900 | 18,600 | 21,500 | 22,500 | 92.5% | 6.3% |
| S Old Lake Wilson Road | | | | | | | | |
| north of Sinclair Road | 105 | 12,084 | 12,152 | 14,419 | 15,596 | 18,901 | 91.7% | 9.4% |
| south of Sinclair Road | 103 | 13,016 | 14,200 | 15,726 | 17,644 | 20,093 | 97.9% | 9.0% |

8.4 RECOMMENDED TRAFFIC FORECASTS

Model output data from the two CF 2045 model runs were extracted and analyzed to determine the impacts of the proposed Sinclair Road Extension. Model volumes were adjusted using the Osceola County MOCF. The MOCF is identified in the FDOT FTO seasonal factor sheet (included in **Appendix C**). The Sinclair Road Extension is shown to serve as an attractive connection between Polk County to the west of Reunion and the major freeway interchange of Interstate 4 (I-4) and SR 429. The proposed Sinclair Road Extension is shown to reduce traffic along most parallel routes from/to I-4/SR429 and Bella Citta Boulevard and US 27.

No-Build and Build 2045 volumes were adjusted to account for the base year 2015 model underrepresentation of volumes along portions of Goodman Road and Bella Citta Boulevard. Two sets of adjustments were performed:

Adjustment #1: Historical 2015 AADTs were compared to the adjusted 2015 daily model volume. The model showed to underrepresent the volumes along Goodman Road south of Bella Citta Boulevard and Bella Citta Boulevard west of Goodman Road. The difference in volume (historical 2015 AADT – 2015 model volume) was added to the Build 2045 model daily volume and the volumes were rounded.

Adjustment #2:

- For the Build 2045 scenario, the major corridor volumes (Sinclair Road west of SR 429, and Bella Citta Boulevard west of Goodman Road) were increased by ±10% of the highest volume along the segment (2,000 daily trips) to reflect the growth in underrepresented traffic volumes. Volumes were rounded where applicable.
- For the No-Build 2045 scenario, the major corridor volumes (Goodman Road south of Bella Citta Boulevard, and Bella Citta Boulevard west of Goodman Road) were increased by 2,000 daily trips to reflect the growth in underrepresented traffic volumes. Volumes were rounded where applicable.

Growth rates were calculated using a Compound Annual Growth Rate (exponential growth) equation.

Table 18 shows a summary of the No-Build and Build 2045 volume development. **Exhibit 8** illustrates the future Year 2045 AADT.

 Table 18: Future (2045) Roadway Volume Development

| | | | | 2015 | Existing | Actual | 2045 | AADT Model V | olume | 20 | No-l 45 AADT Volun | | ion | 20 | Bu 45 AADT Volun | | ion |
|-----------------------------------|------------------------|--------------------|-------------------------|--------|--------------|----------------------------------|------------------------|---------------------|---------------------|--------------------------------|-----------------------------------------|-----------------------------------------|----------------------------------|--------------------------|-------------------------------------|-------------------------------------|----------------------------------|
| Roadway Segment | Raw 2015 Model Vol. | 2015 Model Vol. | Historical 2015 AADT | | 2021 AADT | Growth Rate (2015 to 2021) | No-Build Model Vol. | Build Model Vol. | Model Vol. Diff. | No-Build 2045 Model AADT | Adj. #1 No- Build 2045 Model AADT | Adj. #2 No- Build 2045 Model AADT | Growth Rate (2021 to 2045) | Build 2045 Model AADT | Adj. #1 Build 2045 Model AADT | Adj. #2 Build 2045 Model AADT | Growth Rate (2021 to 2045) |
| Happy Trail | | | | | | | | | | | | | | | | | |
| west of Sinclair Rd | 2,983 | 2,700 | - | - | 800 | - | 11,500 | 10,500 | -1,000 | 11,500 | 11,500 | 11,500 | 11.75% | 10,500 | 10,500 | 10,500 | 11.32% |
| Tradition Boulevard | | | | | | | | | | | | | | | | | |
| east of Sinclair Road | 2,272 | 2,100 | - | - | 3,500 | - | 10,500 | 12,000 | 1,500 | 10,500 | 10,500 | 10,500 | 4.68% | 12,000 | 12,000 | 12,000 | 5.27% |
| Sinclair Road | | | | | | | | | | | | | | | | | |
| east of Goodman Road | - | - | - | - | - | - | - | 15,500 | 15,500 | - | - | - | - | 15,500 | 15,500 | 17,500 | - |
| north of Tradition Boulevard | 2,272 | 2,100 | - | - | 3,500 | - | 10,500 | 20,500 | 10,000 | 10,500 | 10,500 | 10,500 | 4.68% | 20,500 | 20,500 | 22,500 | 8.06% |
| east of SR 429 | 8,255 | 7,500 | 4,171 | -3,329 | 11,500 | 18.4% | 23,000 | 23,500 | 500 | 23,000 | 23,000 | 23,000 | 2.93% | 23,500 | 23,500 | 23,500 | 3.02% |
| Bella Citta Boulevard | | | | | | | | | | | | | | | | | |
| west of Goodman Road | 2,637 | 2,400 | 4,800 | 2,400 | 9,000 | 11.0% | 5,700 | 12,500 | 6,800 | 5,700 | 8,100 | 10,000 | 0.44% | 12,500 | 14,900 | 17,000 | 2.69% |
| Goodman Rd | | | | | | | | | | | | | | | | | |
| north of Bella Citta Blvd | 3,216 | 2,900 | 698 | -2,202 | 4,400 | 35.9% | 6,000 | 5,000 | -1,000 | 6,000 | 6,000 | 6,000 | 1.30% | 5,000 | 5,000 | 5,000 | 0.53% |
| south of Bella Citta Blvd | 2,788 | 2,500 | 8,039 | 5,539 | 11,000 | 5.4% | 9,300 | 8,800 | -500 | 9,300 | 14,800 | 17,000 | 1.83% | 8,800 | 14,300 | 14,500 | 1.16% |
| Masters Boulevard | | | | | | | | | | | | | | | | | |
| north of Champions Gate Boulevard | 4,353 | 4,000 | 8,039 | 4,039 | 12,000 | 6.9% | 13,000 | 10,000 | -3000 | 13,000 | 17,000 | 17,000 | 1.46% | 10,000 | 14,000 | 14,000 | 0.64% |
| Champions Gate Boulevard | | | | | | | | | | | | | | | | | |
| east of Masters Boulevard | 25,236 | 23,000 | 17,300 | -5,700 | 31,500 | 10.5% | 36,500 | 35,000 | -1500 | 36,500 | 36,500 | 36,500 | 0.62% | 35,000 | 35,000 | 35,000 | 0.44% |
| S Old Lake Wilson Road | | | | | | | | | | | | | | | | | |
| north of Sinclair Road | 16,270 | 14,800 | 12,084 | -2,716 | 20,000 | 8.8% | 42,000 | 42,000 | 0 | 42,000 | 42,000 | 42,000 | 3.14% | 42,000 | 42,000 | 42,000 | 3.14% |
| south of Sinclair Road | 20,858 | 19,000 | 13,016 | -5,984 | 18,000 | 5.6% | 40,000 | 40,000 | 0 | 40,000 | 40,000 | 40,000 | 3.38% | 40,000 | 40,000 | 40,000 | 3.38% |



Exhibit 8: Future (2045) No-Build and Build Annual Average Daily Traffic (AADT) Volumes Sinclair Road Extension | Project Traffic Analysis Report (PTAR)

8.5 INTERSECTION DESIGN HOUR VOLUMES

Future Design Hourly Volume (DHV) for Opening Year 2025 and Design Year 2045 were developed using TURNS5. Adjusted Build 2045 model volumes, shown in **Table 18** above, and recommended traffic characteristics were inputted in TURNS5 to generate future DHV for the AM and PM peak hours. TURNS5 output sheets are included in **Appendix L**. DHVs were reviewed to determine if any necessary adjustments were needed. Overall, the DHV for both the study intersections reflected reasonable distribution and anticipated growth. No adjustments were performed to the future intersection turning movement volumes.

Exhibits 9 and 10 show the Opening Year 2025 and Design Year 2045 Build intersection volumes.



Exhibit 9: Opening Year (2025) Build Intersection Turning Movement Volumes
Sinclair Road Extension | Project Traffic Analysis Report (PTAR)



Exhibit 10: Design Year (2045) Build Intersection Turning Movement Volumes
Sinclair Road Extension | Project Traffic Analysis Report (PTAR)

9.0 FUTURE CONDITION ANALYSIS

Future conditions were analyzed for the Build condition for the Opening Year 2025 and Design Year 2045. The Build Condition consists of the extension of Sinclair Road as a four-lane road from Tradition Boulevard to the intersection of Goodman Road and Bella Citta Boulevard. Operating conditions for the arterial and for intersections were calculated using Synchro (v11) software. A roadway LOS analysis was performed for the roadway segments within the study area. This analysis is consistent with the Sinclair Road Preliminary Traffic Analysis technical memorandum, included in **Appendix M**.

9.1 BUILD ALTERNATIVE OPERATIONAL ANALYSIS

9.1.1 ROADWAY LEVEL OF SERVICE ANALYSIS - BUILD

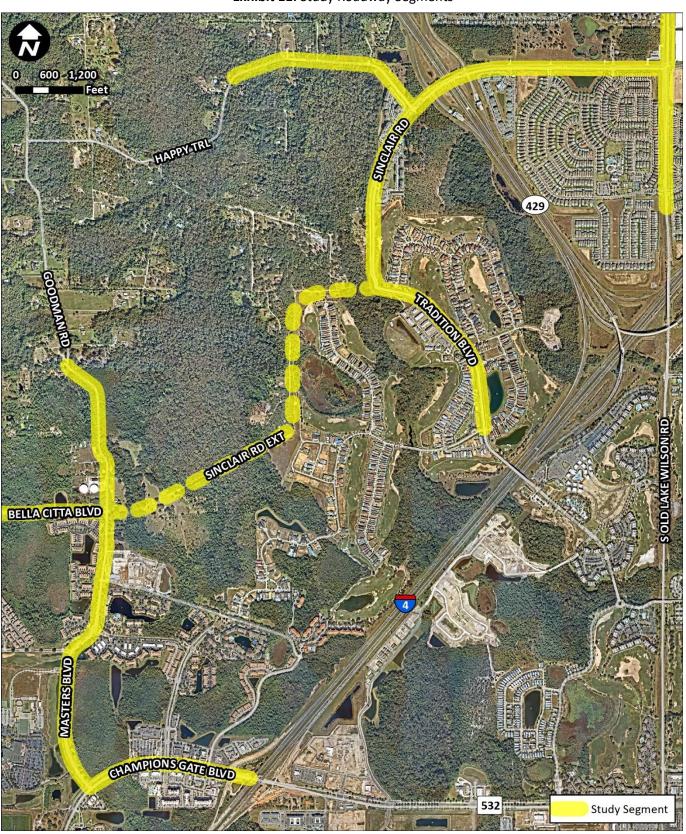
A roadway LOS analysis was performed for the roadway segments within the study area, as shown on **Exhibit 11**. Future Peak Hour Peak Direction (PHPD) volumes were developed by forecasting existing peak hour volumes using the calculated exponential growth rates from **Table 18**. Roadway segment characteristics and LOS capacities were obtained from Osceola County's 2020 Roadway Network Capacity Report and FDOT's Generalized Service Volume Tables.

Table 19 shows the analysis of the roadway LOS analysis.

Table 19: Future (2025 and 2045) Roadway Segment Performance Summary

| | | Target LOS | LOS | Oper | ing Year | 2025 | | Target LOS | LOS | Desi | gn Year 2 | 2045 |
|-----------------------------------|-------|------------|----------|-------|----------|------|-------|------------|----------|-------|-----------|------|
| Roadway Segment | Lanes | Standard | Capacity | PHPD | V/C | LOS | Lanes | Standard | Capacity | PHPD | V/C | LOS |
| Happy Trail | | | | | | | | | | | | |
| west of Sinclair Road | 2 | E | 570 | 72 | 0.13 | С | 2 | Е | 570 | 617 | 1.08 | F |
| Traditions Boulevard | | | | | | | | | | | | |
| east of Sinclair Road | 2 | E | 570 | 262 | 0.46 | С | 2 | Е | 570 | 730 | 1.28 | F |
| Sinclair Road | | | | | | | | | | | | |
| east of Goodman Road | - | - | - | - | - | - | 4 | Е | 1,680 | 949 | 0.56 | D |
| north of Tradition Boulevard | 4 | E | 1,680 | 290 | 0.17 | С | 4 | E | 1,680 | 1,369 | 0.82 | D |
| east of SR 429 | 4 | E | 1,680 | 556 | 0.33 | D | 4 | Е | 1,680 | 1,009 | 0.60 | D |
| Bella Citta Boulevard | | | | | | | | | | | | |
| west of S Goodman Road | 2 | E | 570 | 456 | 0.80 | D | 4 | E | 1,280 | 774 | 0.61 | D |
| S Goodman Road | | | | | | | | | | | | |
| north of Bella Citta Boulevard | 2 | D | 790 | 329 | 0.42 | С | 2 | D | 790 | 366 | 0.46 | С |
| south of Bella Citta Boulevard | 2 | D | 790 | 666 | 0.84 | С | 2 | D | 790 | 838 | 1.06 | F |
| Master Boulevard | | | | | | | | | | | | |
| north of Champions Gate Boulevard | 2 | D | 830 | 653 | 0.79 | С | 2 | D | 830 | 742 | 0.89 | С |
| Champions Gate Boulevard | | | | | | | | | | | | |
| east of Masters Boulevard | 4 | D | 1,530 | 957 | 0.63 | С | 4 | D | 1,530 | 1,044 | 0.68 | С |
| S Old Lake Wilson Road | | | | | | | | | | | | |
| north of Sinclair Road | 4 | D | 1,760 | 1,050 | 0.60 | С | 4 | D | 1,760 | 1,949 | 1.11 | F |
| south of Sinclair Road | 2 | D | 790 | 1,203 | 1.52 | F | 4 | D | 1,760 | 2,340 | 1.33 | F |

Exhibit 11: Study Roadway Segments



9.1.2 FUTURE ARTERIAL PERFORMANCE MEASURES – BUILD

An arterial performance analysis was performed for the extension of Sinclair Road under the Build conditions for the Opening Year 2025 and Design Year 2045 conditions. The arterial analysis was performed using Synchro (v11) software. Arterial performance measures such as speed and LOS, are shown in **Table 20**. As shown below, the Sinclair Road Extension is anticipated to operate below the targeted LOS E.

Build Year / Time Speed (mph) LOS **Period** NB/EB WB/SB NB/EB WB/SB M Peak Hour 2025 29 28 В В 2045 26 27 В В **M** Peak Hour 2025 29 27 В В 2045 27 26 В В

Table 20: Arterial Performance Measures Summary

9.1.3 INTERSECTION LEVEL OF SERVICE ANALYSIS - BUILD

Intersection operational analyses were conducted for AM and PM peak hour conditions for both analysis years, 2025 and 2045. Volumes from TURNS5 were used in the operational analysis for the study intersections. The study intersections were evaluated with multiple control types (unsignalized and signalized) and lane configurations to determine the appropriate intersection configuration needed during the horizon year (2045). The signalized intersection control was selected to evaluate both intersections. The same intersection control was assumed for the Opening Year 2025.

As shown in **Tables 21 through 24**, all study intersection movements are shown to operate with acceptable LOS and V/C ratio less than one (1.0) during the peak hours with the following lane configuration:

Sinclair Road (N/S) and Tradition Boulevard (E/W)

- Northbound: 1 through lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 2 through lanes
- Westbound: 1 left-turn lane and 1 right-turn lane

Sinclair Road/Bella Citta Boulevard and S Goodman Road

- Northbound: 1 left-turn lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 1 shared through/right lane
- Westbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane
- Eastbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane

Table 21: Opening Year (2025) Intersection Performance – AM Peak Hour

| Intersection | MOE | E | astbour | nd | W | estbou | nd | No | orthbou | nd | So | uthbou | nd | Overall |
|------------------------------|----------------|------|---------|-------|------|--------|-------|------|---------|-------|------|--------|-------|---------|
| intersection | IVIOL | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| C'arlair Barri O | Delay | | | | 25.8 | | 36.8 | | 9.7 | 9.8 | 6.8 | 4.8 | | 19.0 |
| Sinclair Road @ Tradition | LOS | | | | С | | D | | Α | Α | Α | Α | | В |
| Boulevard | V/C | | | | 0.08 | | 0.85 | | 0.10 | 0.10 | 0.21 | 0.04 | | |
| (Signalized) | Queue (veh) | | | | 1 | | 9 | | 1 | 1 | 2 | 0 | | |
| Dalla Citta | Delay | 14.7 | 17.5 | 32.2 | 18.6 | 16.7 | 16.7 | 62.5 | 0.0 | 25.6 | 27.1 | 0.0 | 37.3 | 35.6 |
| Bella Citta Boulevard @ | LOS | В | В | С | В | В | В | Ε | Α | С | С | Α | D | D |
| Goodman Road | V/C | 0.16 | 0.13 | 0.87 | 0.28 | 0.04 | 0.04 | 0.96 | 0.00 | 0.53 | 0.08 | 0.00 | 0.79 | |
| (Signalized) | Queue (veh) | 2 | 2 | 15 | 1 | 1 | 1 | 15 | 0 | 7 | 1 | 0 | 8 | |

Table 22: Opening Year (2025) Intersection Performance – PM Peak Hour

| Intersection | MOE | E | astbour | nd | W | estbou | nd | No | orthbou | nd | So | uthbou | nd | Overall |
|------------------------------|----------------|------|---------|-------|------|--------|-------|------|---------|-------|------|--------|-------|---------|
| intersection | IVIOE | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| Cinalain Baad O | Delay | | | | 33.6 | | 39.9 | | 8.6 | 8.6 | 5.6 | 3.8 | | 14.7 |
| Sinclair Road @ Tradition | LOS | | | | С | | D | | Α | Α | Α | Α | | В |
| Boulevard | V/C | | | | 0.10 | | 0.66 | | 0.05 | 0.06 | 0.27 | 0.06 | | |
| (Signalized) | Queue (veh) | | | | 1 | | 7 | | 1 | 1 | 3 | 1 | | |
| Dalla Citta | Delay | 16.9 | 19.1 | 28.4 | 18.8 | 17.8 | 17.8 | 23.1 | 0.0 | 18.4 | 22.3 | 0.0 | 32.2 | 25.5 |
| Bella Citta Boulevard @ | LOS | В | В | С | В | В | В | С | Α | В | С | Α | С | С |
| Goodman Road | V/C | 0.09 | 0.09 | 0.83 | 0.30 | 0.06 | 0.06 | 0.67 | 0.00 | 0.16 | 0.05 | 0.00 | 0.80 | |
| (Signalized) | Queue (veh) | 1 | 1 | 11 | 2 | 1 | 1 | 6 | 0 | 2 | 1 | 0 | 9 | |

Table 23: Design Year (2045) Intersection Performance – AM Peak Hour

| Intersection | MOE | E | astbour | nd | W | estbou | nd | No | orthbou | nd | So | uthbou | nd | Overall |
|------------------------------|----------------|------|---------|-------|------|--------|-------|------|---------|-------|------|--------|-------|---------|
| intersection | WOL | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| C'arlair Barri O | Delay | | | | 22.6 | | 59.5 | | 58.4 | 58.6 | 62.6 | 13.8 | | 47.7 |
| Sinclair Road @ Tradition | LOS | | | | С | | Ε | | Ε | Е | Е | В | | D |
| Boulevard | V/C | | | | 0.27 | | 0.96 | | 0.94 | 0.94 | 0.95 | 0.30 | | |
| (Signalized) | Queue (veh) | | | | 5 | | 24 | | 23 | 23 | 12 | 6 | | |
| Dalla Citta | Delay | 28.5 | 73.1 | 74.7 | 71.8 | 26.3 | 26.4 | 38.5 | 0.0 | 76.7 | 60.0 | 0.0 | 39.0 | 59.6 |
| Bella Citta Boulevard @ | LOS | С | Ε | Е | E | С | С | D | Α | Е | Е | Α | D | Е |
| Goodman Road | V/C | 0.24 | 0.96 | 0.96 | 0.93 | 0.29 | 0.30 | 0.65 | 0.00 | 0.97 | 0.78 | 0.00 | 0.34 | |
| (Signalized) | Queue (veh) | 4 | 29 | 27 | 20 | 8 | 8 | 6 | 0 | 28 | 7 | 0 | 8 | |

Table 24: Design Year (2045) Intersection Performance – PM Peak Hour

| Intersection | MOE | E | astbour | nd | W | estbou | nd | No | orthbou | nd | So | uthbou | nd | Overall |
|------------------------------|----------------|------|---------|-------|------|--------|-------|------|---------|-------|------|--------|-------|---------|
| intersection | IVIOE | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Overall |
| Cinalaia Band © | Delay | | | | 36.6 | | 61.5 | | 18.7 | 18.8 | 14.0 | 6.7 | | 19.7 |
| Sinclair Road @ Tradition | LOS | | | | D | | Е | | В | В | В | Α | | В |
| Boulevard | V/C | | | | 0.54 | | 0.89 | | 0.41 | 0.42 | 0.78 | 0.36 | | |
| (Signalized) | Queue (veh) | | | | 8 | | 13 | | 9 | 8 | 9 | 6 | | |
| Dalla Citta | Delay | 21.1 | 31.0 | 33.0 | 44.5 | 17.0 | 17.0 | 31.5 | 0.0 | 35.7 | 29.6 | 0.0 | 42.2 | 32.1 |
| Bella Citta Boulevard @ | LOS | С | С | С | D | В | В | С | Α | D | С | Α | D | С |
| Goodman Road | V/C | 0.12 | 0.73 | 0.80 | 0.93 | 0.32 | 0.32 | 0.64 | 0.0 | 0.68 | 0.39 | 0.0 | 0.81 | |
| (Signalized) | Queue (veh) | 1 | 12 | 12 | 14 | 6 | 6 | 7 | 0 | 8 | 4 | 0 | 9 | |

9.1.4 QUEUE LENGTH ANAYSIS

The 95th-percentile queues at the left-turning movements at the study intersections were obtained from Synchro outputs. The higher of the AM and PM peak hour was used determine the recommended queue storage lengths for Design Year (2045) conditions. An average vehicle length of 25 feet was assumed. The calculations of the recommended turn lane queue lengths are shown in **Table 25**.

Sinclair Rd Sinclair Rd/Bella Citta Blvd & Tradition Bvld & Goodman Rd **Turn Lane Turn Lane** 95th % Vehicle 95th % Vehicle Queue Queue Movement Queue Length Queue Length Length Length (vehicles)1 (vehicles)1 (feet) (feet) (feet) (feet) 25 4 **EBL** 0 25 100 10 25 250 20 25 **WBL** 500 0 25 7 25 175 **NBL** 25 7 12 300 25 175 **SBL**

Table 25: Turn Lane Queue Length Determination

Note:

1. 95th-percentile queue as reported in the Synchro outputs (Appendix F).

9.2 PREDICTIVE CRASH ANALYSIS

A Highway Safety Manual (HSM) analysis was conducted for the 2045 Build alternative using predictive crash methods in order to quantify future crashes along the Sinclair Road Extension and the study intersections. The predictive crash analysis was performed using the HSM Chapter 12 methodology for urban/suburban arterial and intersections. The HSM includes Safety Performance Functions (SPFs) as bases for crash predictions; SPFs are equations used to estimate the average crash frequency per year as a function of traffic volume and roadway characteristics. The HSM methodology allows for the result of the standard SPF predictive models (predicted crashes) to be adjusted by incorporating historical crash data using Empirical-Bayes to obtain a more site-specific composite crash frequency (expected crashes). Historic crash data was not incorporated in this analysis. The results reflect predicted crashes only. **Appendix N** includes the HSM analysis spreadsheet outputs.

Sinclair Road Extension was assumed as a 35 MPH 4-lane divided roadway. The future roadway extends approximately 1.5 miles. The proposed roadway was assumed with lighting present, no on-street parking, and two residential driveways. These driveways represent the Dewan/Elevation residential development located on the south side of Sinclair. The two signalized intersections located at the extremity of the future Sinclair Road Extension were assumed to have the lane configurations listed in the previous section.

Based on the assumptions stated herein and the HSM methodology, Sinclair Road is predicted to have an average crash frequency of 4.6 crashes per year. The two study intersections are predicted to increase their crash frequency by year 2045 as a result of the increased traffic. A summary of the predicted crashes is shown in **Table 26**.

Table 26: Crash Prediction Summary

| | Crash | es per Year - Build | 2045 |
|----------------------------------------|----------------------------|---------------------|-------|
| Facility | Property Damage Only (PDO) | Fatal and Injury | КАВСО |
| Segment | | | |
| Sinclair Rd Extension | 3.3 | 1.3 | 4.6 |
| Intersections | | | |
| Sinclair Rd & Tradition Blvd | 1.7 | 0.9 | 2.6 |
| Sinclair Rd & Goodman/Bella Citta Blvd | 2.1 | 1.1 | 3.2 |

10.0 RECOMMENDATIONS

Based on the analysis performed for the Design Year 2045 Build traffic conditions, it is recommended that both study intersections be signalized and provide the following lane configuration:

Sinclair Road (N/S) and Tradition Boulevard (E/W)

- Northbound: 1 through lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 2 through lanes
- Westbound: 1 left-turn lane and 1 right-turn lane

Sinclair Road/Bella Citta Boulevard and S Goodman Road

- Northbound: 1 left-turn lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 1 shared through/right lane
- Westbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane
- Eastbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane

Both intersections should operate with permissive/protected left turning movements. Recommended left-turn lane queue lengths are shown in **Table 27**.

Table 27: Recommended Turn Lane Queue Lengths

| Intersection | Turr | n Lane Queu | e Length (f | eet) |
|-------------------------------------------|------|-------------|-------------|------|
| intersection | EBL | WBL | NBL | SBL |
| Sinclair Rd & Tradition Bvld | - | 250 | - | 300 |
| Sinclair Rd/Bella Citta Blvd & Goodman Rd | 100 | 500 | 175 | 175 |

APPENDIX A

Traffic Analysis Methodology

Traffic Analysis Methodology for Project Traffic Analysis Report (PTAR)

Alternatives Evaluation Study Sinclair Road Extension From Tradition Boulevard to Bella Citta Boulevard

Prepared for:



Osceola County, Florida
Department of Transportation and Transit
1 Courthouse Square, Suite 3100
Kissimmee, FL 34741

FEBRUARY 2022

Prepared by:

Kimley-Horn and Associates, Inc.

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1.0 PROJECT DESCRIPTION

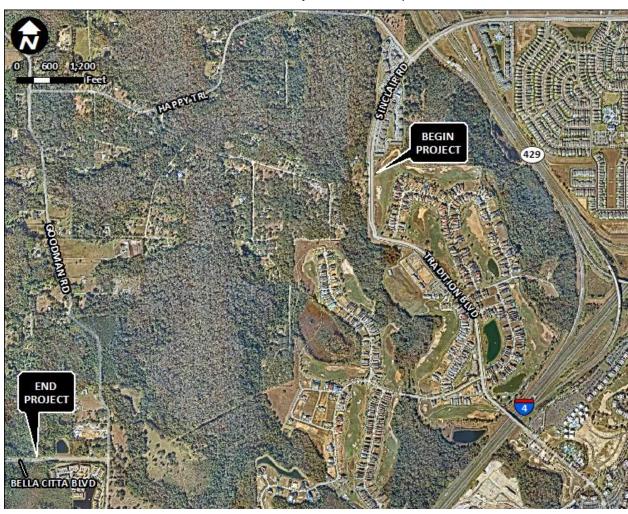
1.1 PROJECT BACKGROUND

Osceola County is conducting an Alternatives Evaluation Study, which will be followed by a development of design plans for the extension of Sinclair Road from Tradition Boulevard to Bella Citta Boulevard. This project involves the construction of a new roadway from Tradition Boulevard to S Goodman Road, initially as a two-lane facility, with the option to widen to four lanes at some time in the future. This traffic analysis will evaluate when the roadway will warrant expansion to 4-lanes. Multimodal accommodations, associated drainage improvements and stormwater ponds, and modification of the intersections at each end of the project will be evaluated.

In the existing conditions, Sinclair Road, from Tradition Boulevard to SR 429, is a 4-lane local road with a posted speed limit of 35 MPH. From SR 429 to Old Lake Wilson Road, Sinclair Road is an Urban Major Collector with a posted speed limit of 35 MPH. Bella Citta Road, west of Goodman Road is a 2-lane Urban Major Collector with a posted speed limit of 40 MPH. The project is located in Osceola County, and is displayed on **Exhibit 1**.

This document provides details of the technical approach for Project Traffic Analysis for the Sinclair Road Extension. The traffic analysis will be conducted based on methods and procedures described in the 2020 Florida Department of Transportation (FDOT) Project Development & Environment (PD&E) Manual, the 2021 FDOT Traffic Analysis Handbook, and the 2019 FDOT Project Traffic Forecasting Handbook. This traffic analysis will be documented in the Project Traffic Analysis Report (PTAR).

Exhibit 1: Project Location Map



2.0 DATA COLLECTION

Data will be collected within the project area. There are two adjacent studies underway, and the study team will coordinate with these studies and obtain available data for consideration during Part A. These studies include:

- The Poinciana Parkway Extension Project Development and Environment (PD&E) study (by Florida's Turnpike) will be evaluating the Sinclair Road interchange with SR 429.
- The S. Old Lake Wilson Road PD&E study (by Osceola County) will be evaluating the Sinclair Road intersection with S. Old Lake Wilson Road.

2.1 TRAFFIC COUNT SOURCES

Traffic volume counts will be collected from existing sources and supplemented with additional counts obtained for this study. Existing sources are summarized in **Table 1**.

Source **Station** Location Type **Date FDOT** 921086 Goodman Road, north of Bella Citta Boulevard Historic, Daily 7/8/2020 Florida 921087 Goodman Road, south of Bella Citta Boulevard Historic, Daily 7/7/2020 Traffic 927084 Bella Citta Boulevard, west of Goodman Road Historic, Daily 7/7/2020 Online 126 Goodman Road, north of Bella Citta Boulevard 10/7/2020 Daily 10/7/2020 Osceola 121 Goodman Road, south of Bella Citta Boulevard Daily County 184 Bella Citta Boulevard, west of Goodman Road Daily 3/10/2020

Table 1: Existing Traffic Counts

Since Sinclair Road Extension is a planned road, traffic data collection of existing conditions will be minimal, focused on the roadways on each end of the extension, as shown in **Table 2**.

Count Type

Sinclair Road, north of Tradition Boulevard

Bella Citta Boulevard, west of Goodman Road

Goodman Road, north of Bella Citta Boulevard

Goodman Road, south of Bella Citta Boulevard

Happy Trail, west of Sinclair Road

8-hour Turning Movement Counts

Bella Citta Boulevard at Goodman Road

Table 2: Study Traffic Count Locations

No vehicle classification counts will be taken as the future conditions with the extension are expected to be different than existing traffic. Future truck percentages will be estimated based on similar functioning roadways within Osceola County.

2.2 PEDESTRIAN, BICYCLE & OTHER MULTIMODAL DATA

Pedestrian and bicycle data will be extracted from the turning movement counts as shown in **Table 2**. Pedestrian and bicycle data for the intersection of Sinclair Road at Tradition Boulevard will be collected in the field in September 2021 (or later) when the Osceola County schools reopen after the summer break. Currently, there are no transit stops (or routes) within project limits. Based on the latest Osceola County Comprehensive Plan - 2040 Transit System plans, transit-related improvements are not planned within the project limits.

2.3 EXISTING TRAFFIC DEVELOPMENT

2.3.1 ANNUAL AVERAGE DAILY TRAFFIC (AADT)

The traffic counts collected in 2021 will be used to develop AADTs for existing conditions. Segments will include:

- Sinclair Road, north of Tradition Boulevard
- Bella Citta Road, west of Goodman Road
- Tradition Boulevard, east of Sinclair Road
- Goodman Road, north of Bella Citta Boulevard
- Goodman Road, south of Bella Citta Boulevard

In addition, as requested by the County, AADTs for existing conditions outside the project area will be identified for informational purposes:

- Sinclair Road, from SR 429 to S. Old Lake Wilson Road (County Station #106)
- S. Old Lake Wilson Road, north of Sinclair Road (County Station #105)
- S. Old Lake Wilson Road, south of Sinclair Road (County Station #103)
- Masters Boulevard, north of Champions Gate Boulevard (County Station #121)
- Champions Gate Boulevard, from Masters Boulevard to I-4 (County Station #122)

2.3.2 INTERSECTION PEAK HOUR VOLUMES (FROM TMC)

Eight-hour turning movement counts (TMCs) will be collected for the intersection of Bella Citta Boulevard and Goodman Road. The peak eight hours will be identified from the 72-hour traffic volume counts on the intersection legs. Since the "intersection" of Sinclair Road and Tradition Boulevard only has two legs, the 72-hour traffic volume count at this location will be used to develop the "turning movements" at this intersection. The TMCs will be adjusted to represent design traffic for AM and PM peak hours.

3.0 PROJECT ASSUMPTIONS

3.1 ANALYSIS YEARS

The corridor will be analyzed for the following years:

- Existing Year 2021
- Opening Year 2025
- Design Year 2045

In addition, the year the corridor warrants providing a 4-lane facility will be identified.

3.2 PROJECT ALTERNATIVES

The study will evaluate the following alternative:

Build Alternative: The Build alternative will represent the construction of Sinclair Road
extension as a two-lane facility within the study limits along with committed and planned
improvements near the project area.

A No-Build Alternative will not be addressed.

3.3 TRAVEL DEMAND MODEL

The latest version of the Central Florida Regional Planning Model (CFRPM) [version 7.0], FDOT's adopted regional planning model, with the base year 2015 and the horizon year 2045 will be used in developing the future traffic projections within the project area.

3.4 TARGET LEVEL OF SERVICE (LOS)

LOS targets per the Osceola County Comprehensive Plan are summarized below:

• Sinclair Road Extension and Study Intersections: LOS E

3.5 ANALYSIS TOOL(S)

Synchro/SimTraffic 11 will be used to perform the LOS operational analyses for the study intersections and arterial. Highway Capacity Manual (HCM), 6th Edition-based analysis results (if available) will be provided for both the signalized and unsignalized intersections. Roadway segment LOS will be computed using Synchro/SimTraffic reported average speed and criteria from Exhibit 18-1 of the HCM, 6th Edition.

3.6 DESIGN HOUR TRAFFIC FACTORS FOR FUTURE ANALYSIS

- Peak Hour Factor (PHF)
 - Will be determined in the PTAR and compared against acceptable ranges found in the Project Traffic Forecasting Handbook
- K Factor (proportion of the AADT that occurs during the design hour):
 - Will be determined in the PTAR and compared against acceptable ranges found in the Project Traffic Forecasting Handbook
- D Factor (percentage of the total, two-way design hour traffic traveling in the peak direction)
 - Will be determined in the PTAR and compared against acceptable ranges found in the Project Traffic Forecasting Handbook

- T Factor (percentage of the AADT volume generated by trucks or commercial vehicles)
 - Will be determined in the PTAR and compared against acceptable ranges found in the Project Traffic Forecasting Handbook

3.7 STUDY MEASURES OF EFFECTIVENESS (MOES)

The analysis results will include the following performance measures:

- Study Intersection:
 - Overall LOS and Lane Group LOS,
 - Overall Volume-to-Capacity (V/C) ratio and Lane Group V/C,
 - Overall Delay (seconds per vehicle) and Lane Group delay, and
 - 95th percentile queues for turn lanes (for future storage length requirements)
- Arterial:
 - Speed, and
 - LOS

3.8 SAFETY ANALYSIS

Historical Crash Data from 2016 to 2020 will be evaluated for the intersections of:

- Sinclair Road at Tradition Boulevard
- Goodman Road at Bella Citta Boulevard

Source:

- From Osceola County
- Signal Four Analytics

4.0 FUTURE TRAFFIC DEVELOPMENT

The traffic forecasting methodology will be consistent with the procedures outlined in the 2019 FDOT Project Traffic Forecasting Handbook. This section discusses the detailed methodology for the future year traffic forecast development process for the Build conditions.

4.1 SUB-AREA MODEL VALIDATION

CFRPM version 7.0 with the base year 2015, and the horizon year 2045 will be used in developing the future traffic projections within the project area. The proposed sub-area, shown on **Exhibit 2**, in the CFRPM model will be calibrated and validated for the existing year 2021 conditions. The Socio-Economic (SE) data for the year 2020 will be used. As part of the sub-area validation, land use and roadway network data, roadway speeds, capacities, travel patterns, pathfinding algorithms will be examined, and necessary model updates will be made to better validate model results within the project area. The model validation and calibration of the CFRPM model will follow the guidance provided in the "FSUTMS-Cube Framework Phase II Model Calibration and Validation Standards".

ORANGE COUNTY 2 OSCEOLA COUNTY Walt Disney World Resort Walt Disney World Resort 429 4 Davenport Greek Swamp Celebration Mystic Dunes Golf Club Dave nport Creek Swamp inclair Rd **PROJECT** LOCATION OSCEOLA COUNTY Bella Citta Blvd ChampionsGate Golf Club **PROPOSED TRAVEL DEMAND** MODEL SUB-AREA

Exhibit 2: Proposed Travel Demand Model Sub-Area

4.2 FUTURE YEAR MODEL DEVELOPMENT

After the subarea base year validation, the same model updates will be applied to the 2025 and 2045 future year models. For future conditions, a build alternative will be modeled for the years 2025 and 2045.

4.2.1 STAKEHOLDER COORDINATION

Before conducting the year 2025 and 2045 model runs, the socio-economic data and the roadway network (Cost Feasible 2045 CFRPM) will be updated to account for any new developments and network connectivity identified by the County. The future year travel demand model will consider programmed and planned improvements in the vicinity of the project area that are consistent with regional transportation plans, including the following:

- FDOT Five Year Work Program and MetroPlan Orlando Transportation Improvement Program
- FDOT Strategic Intermodal System (SIS) plans
- Committed improvements from local and private sources
- Adopted LRTPs and Comprehensive Plans
- Central Florida Expressway Authority (CFX) Masterplan

Specifically, the project team will coordinate with the County, CFX, and Florida's Turnpike Enterprise (FTE) on the following important planned improvements, including their expected opening date:

- Poinciana Parkway Extension, from CR 532 to SR 429 at I-4 (by FTE)
- Southport Connector Expressway (by CFX)

4.3 FUTURE TRAFFIC FORECASTS

Since the Sinclair Road Extension will be a new roadway connection, the opening year 2025 and design year 2045 traffic volumes will be estimated using the model forecasted volumes (using the approved 2025 and 2045 datasets for CFRPM 7.0), with consideration of historical growth rates on surrounding roadways and Bureau of Economics & Business Research (BEBR) low, medium, and high population projections.

Should there be future traffic estimates that are not consistent with the historical trends or reasonable expectations for growth in the study corridor, these issues will be reviewed with the County, and an acceptable solution will be reached on any revisions necessary.

In addition, as requested by the County, AADTs for 2025 and 2045 conditions for roadways outside the project area, for build and no-build conditions, will be identified for informational purposes:

- Sinclair Road, from SR 429 to S. Old Lake Wilson Road
- S. Old Lake Wilson Road, north of Sinclair Road
- S. Old Lake Wilson Road, south of Sinclair Road
- Masters Boulevard, north of Champions Gate Boulevard
- Champions Gate Boulevard, from Ronald Reagan Parkway to Masters Boulevard
- Champions Gate Boulevard, from Masters Boulevard to I-4

4.4 DESIGN TRAFFIC CHARACTERISTICS

The recommended standard "K" factor of 9.0% will be used for all the study roadway segments. The "D" and "T" factors will be developed using historical data reported by FDOT Florida Traffic Online (FTO), previous counts, and the recommended ranges identified in the 2019 Project Traffic Forecasting Handbook.

4.5 DESIGN HOUR VOLUMES

The recommended design traffic characteristics, existing intersection turning movement volumes and the future traffic projections will be used as inputs to the TURNS5 spreadsheet to develop the intersection design hour volumes. The output of the TURNS5 will be adjusted to account for reasonability and balancing purposes.

5.0 OPERATIONAL ANALYSIS

5.1 TRAFFIC OPERATIONAL ANALYSIS

Detailed operational analyses will be performed for all analysis years for both AM and PM peak hours using Synchro. Based on input from the County, SimTraffic simulation may be conducted for the intersections of Bella Citta Boulevard and Goodman Road, and Sinclair Road and Tradition Boulevard. Analyses will be performed for the following scenarios:

- Existing Year 2021
- Opening Year 2025 Build Conditions
- Design Year 2045 Build Conditions

The need for future signalization at the stop-controlled intersections will be based on the volume-based Manual on Uniform Traffic Control Devices (MUTCD) signal warrants (1-3).

5.2 ALTERNATIVE ANALYSIS

The study intersection alternatives will be developed and assessed under the Build condition based on traffic demand. Turn lane and storage length requirements will be based on the operational analyses of the future Build alternative.

6.0 SAFETY ANALYSIS

6.1 CRASH DATA ANALYSIS

Detailed crash data within the project area will be analyzed and documented. The safety analysis will summarize location of crashes, crash types, contributing causes of these crashes, most common types of crashes, crash rates, and safety ratios.

6.2 SAFETY ANALYSIS

The safety analysis will be performed following Part 2, Chapter 2 of the PD&E Manual. Based on the information obtained from the crash data, the project safety needs associated with the existing and future conditions will be identified. Furthermore, a Build Highway Safety Manual (HSM) safety analysis will be conducted utilizing Crash Modification Factors (CMFs), if available, and predictive crash methods to estimate potential future crashes.

7.0 DOCUMENTATION

A PTAR will be prepared to document the data collection task, results of the existing conditions analysis, results of the CFRPM model validation, the year 2025 and 2045 travel demand modeling efforts, development of future AADTs, and design hour volumes, safety analysis, Build alternative analysis results, and final recommendations.

APPENDIX B

Raw Traffic Count

Prepared by NDS/ATD

VOLUME

Sinclair Rd N/O Tradition Blvd

Day: Tuesday Date: 11/16/2021

City: Kissimmee Project #: FL21_130268_001

| | DAI | II Y T | ОТА | d S | | NB | SE | | EB | | WB | | | | | | | Tot | |
|---------------------------------|----------|--------------|------------|--------------|-------|-------|----------|--------------|---------------------------------|---------------|--------------|----------|--------------|----|---|------------|---|---------------|--------------|
| | | | 017 | (LO | | 1,549 | 1,9 | 31 | 0 | | 0 | | | | | | | 3,48 | 30 |
| AM Period | NB | | SB | | EB | WB | | OTAL | PM Period | NB | | SB | | EB | V | V B | | TOT | AL |
| 00:00 00:15 | 2 4 | | 2 3 | | | | 7 | | 12:00 12:15 | 33 22 | | 16 23 | | | | | | 9 5 | |
| 00:30 00:45 | 4 | 11 | 0 | 7 | | | 4 | 18 | 12:30 12:45 | 15 30 | 100 | 27 20 | 86 | | | | | 2 | 186 |
| 01:00 | 0 | 11 | 2 | 1 | | | 2 | 10 | 13:00 | 29 | 100 | 25 | 00 | | | | | 4 | 100 |
| 01:15 01:30 | 2 | | 1 | | | | 3 | | 13:15 13:30 | 18 18 | | 19 28 | | | | | | 7 6 | |
| 01:45 | 0 | 3 | 1 | 5 | | | 1 | 8 | 13:45 | 21 | 86 | 20 14 | 86 | | | | | | 172 |
| 02:00 02:15 | 0 | | 2 | | | | 2 | | 14:00 14:15 | 29 35 | | 17 32 | | | | | 6 | 6 7 | |
| 02:30 | 1 | | 0 | | | | 1 | | 14:30 | 33 | | 25 | | | | | 5 | 8 | |
| 02:45 03:00 | 0 | 2 | 0 | 5 | | | 2 | 7 | 14:45 15:00 | 33 29 | 130 | 33 43 | 107 | | | | | <u>6</u> 2 | 237 |
| 03:15 | 0 | | 1 | | | | 1 | | 15:15 | 21 | | 31 | | | | | 5 | 2 | |
| 03:30 03:45 | 2 3 | 6 | 1 0 | 3 | | | 3 | 9 | 15:30 15:45 | 21 23 | 94 | 38 34 | 146 | | | | | 9 7 | 240 |
| 04:00 | 0 | | 0 | | | | 0 | , | 16:00 | 19 | , 1 | 52 | 1 10 | | | | 7 | 1 | 2 10 |
| 04:15 04:30 | 1 5 | | 1 1 | | | | 2 | | 16:15 16:30 | 36 30 | | 51 49 | | | | | 8 | 7 9 | |
| 04:45 | 4 | 10 | <u>i</u> | 3 | | | 5 | 13 | 16:45 | 35 | 120 | 64 | 216 | | | | 9 | 9 | 336 |
| 05:00 05:15 | 4 3 | | 1 0 | | | | 5 | | 17:00 17:15 | 49 27 | | 41 51 | | | | | | 0 8 | |
| 05:30 | 1 | 4.0 | 2 | 0 | | | 3 | 40 | 17:30 | 31 | 400 | 66 | 407 | | | | 9 | 7 | 001 |
| 05:45 06:00 | 6 | 10 | <u>5</u> 2 | 8 | | | 8 | 18 | 17:45 18:00 | 32 14 | 139 | 39 49 | 197 | | | | | 1 3 | 336 |
| 06:15 | 9 | | 2 | | | | 11 | | 18:15 | 25 | | 44 | | | | | 6 | 9 | |
| 06:30 06:45 | 6 18 | 39 | 9 20 | 33 | | | 15 38 | | 18:30 18:45 | 11 13 | 63 | 54 56 | 203 | | | | 6 | 5 9 | 266 |
| 07:00 | 21 | | 25 | | | | 46 | | 19:00 | 14 | | 59 | | | | | 7 | 3 | |
| 07:15 07:30 | 18 21 | | 23 28 | | | | 41 49 | | 19:15 19:30 | 19 14 | | 46 21 | | | | | 3 | 5 5 | |
| 07:45 08:00 | 27 32 | 87 | 27 28 | 103 | | | 54 60 | | 19:45 20:00 | 14 9 | 61 | 22 20 | 148 | | | | 2 | | 209 |
| 08:15 | 44 | | 20 | | | | 64 | | 20:15 | 5 | | 20 17 | | | | | 2 | 2 | |
| 08:30 08:45 | 32 34 | 142 | 20 34 | 102 | | | 52 68 | | 20:30 20:45 | 4 8 | 26 | 21 12 | 70 | | | | | 5 0 | 96 |
| 09:00 | 44 | 142 | 24 | 102 | | | 68 | | 21:00 | 2 | | 22 | 70 | | | | 2 | 4 | 70 |
| 09:15 09:30 | 25 32 | | 30 27 | | | | 55 59 | | 21:15 21:30 | 12 9 | | 17 10 | | | | | | 9 9 | |
| 09:45 | 30 | 131 | 21 | 102 | | | 51 | 233 | 21:45 | 6 | 29 | 10 | 59 | | | | 1 | 6 | 88 |
| 10:00 10:15 | 31 31 | | 22 24 | | | | 53 55 | | 22:00 22:15 | 6 5 | | 13 7 | | | | | | 9 2 | |
| 10:30 | 38 | 405 | 25 | 0.5 | | | 63 | | 22:30 | 8 | ~ - | 9 | | | | | 1 | 7 | |
| 10:45 11:00 | 21 28 | 121 | 20 24 | 91 | | | 41 52 | | 22:45 23:00 | <u>4</u> 6 | 23 | 12 3 | 41 | | | | | <u>6</u> | 64 |
| 11:15 | 27 | | 23 | | | | 50 | | 23:15 | 3 | | 4 | | | | | | 7 | |
| 11:30 11:45 | 28 23 | 106 | 20 31 | 98 | | | 48 54 | | 23:30 23:45 | 0 | 10 | 3 | 12 | | | | | 3 | 22 |
| TOTALS | | 668 | | 560 | | | | 1228 | TOTALS | | 881 | | 1371 | | | | | | 2252 |
| SPLIT % | 5 | 54.4% | | 45.6% | | | | 35.3% | SPLIT % | | 39.1% | | 60.9% | | | | | (| 64.7% |
| | DΑ | IJΥIJ | OTA | 15 | | NB | SE | 3 | EB | | WB | | | | | | | Tot | _ |
| | | | | NE3- | | 1,549 | 1,9 | 31 | 0 | | 0 | | | | | | | 3,48 | 80 |
| AM Peak Hour | | 08:15 | | 08:45 | | | | 08:15 | PM Peak Hour | | 16:15 | | 16:45 | | | | | | 16:45 |
| AM Pk Volume Pk Hr Factor | | 154 0.875 | | 115 0.846 | | | | 252 0.926 | PM Pk Volume Pk Hr Factor | | 150 0.765 | | 222 0.841 | | | | | | 364 0.919 |
| 7 - 9 Volume | | 229 | | 205 | 0 | 0 |) | 434 | 4 - 6 Volume | | 259 | | 413 | | 0 | C |) | | 672 |
| 7 - 9 Peak Hour | | 08:00 | | 07:15 | | | | | 4 - 6 Peak Hour | | 16:15 | | 16:45 | | | | | | 16:45 |
| 7 - 9 Pk Volume Pk Hr Factor | | 142 0.807 | | 106 0.946 | | | | 244 0.897 | 4 - 6 Pk Volume Pk Hr Factor | | 150 0.765 | | 222 0.841 | | | | | | 364 0.919 |
| TRITI TUOTOI | | 5.551 | | 3.710 | 0,000 | 0.0 | | 0.077 | The Fuotor | | 5.700 | | 0.011 | 0. | | 0.0 | | | 31717 |

Prepared by NDS/ATD VOLUME

Sinclair Rd N/O Tradition Blvd

Day: Wednesday Date: 11/17/2021 City: Kissimmee Project #: FL21_130268_001

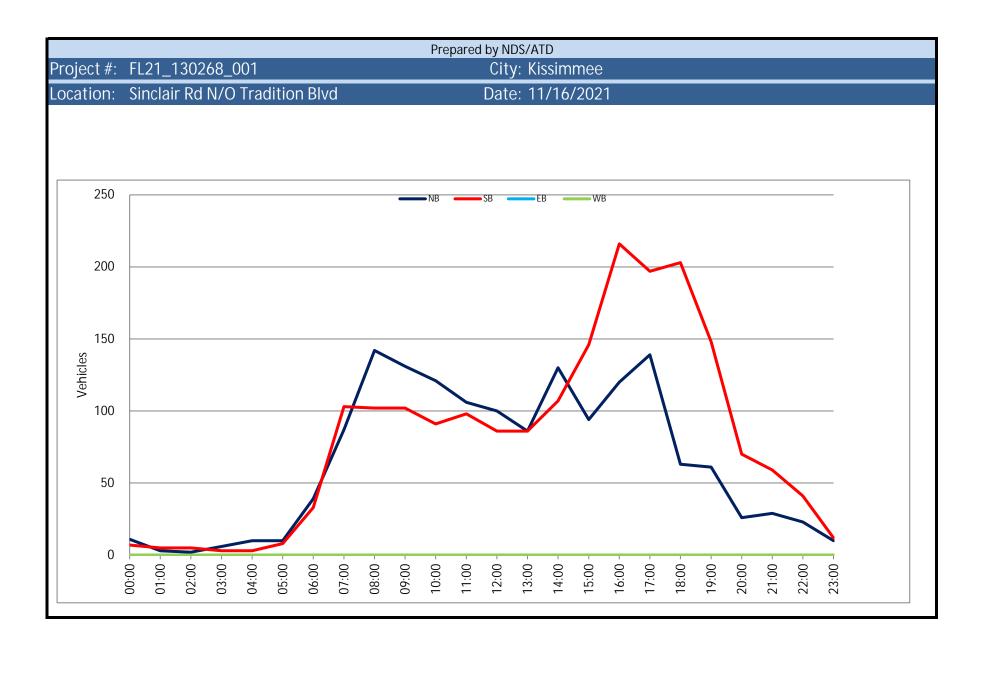
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|---------------------------|----------|--------------|---------------|--------------|------|-------|-------|----------|--------------|---------------------------------|----------|--------------|----------|--------------|----|-------|----|-------|----------|--------------|
| | | | 017 | | | 1,554 | | 1,930 | | 0 | | 0 | | | | | | | 3,4 | 184 |
| AM Period | NB | | SB | | EB | WB | | | TAL | PM Period | NB | | SB | | EB | | WB | | | TAL |
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| 00:30 | 3 | 10 | 4 | 7 | | | | 7 | 17 | 12:30 | 18 | 00 | 20 | 00 | | | | | 38 | 101 |
| 00:45 01:00 | 1 1 | 10 | <u>0</u> 1 | / | | | | 2 | 17 | 12:45 13:00 | 32 33 | 99 | 18 23 | 82 | | | | | 50 56 | 181 |
| 01:15 | 3 | | 1 | | | | | 4 | | 13:15 | 24 | | 26 | | | | | | 50 | |
| 01:30 01:45 | 0 2 | 6 | 1 0 | 3 | | | | 1 2 | 9 | 13:30 13:45 | 19 32 | 108 | 27 31 | 107 | | | | | 46 63 | 215 |
| 02:00 | 0 | | 0 | | | | | 0 | , | 14:00 | 23 | 100 | 24 | 107 | | | | | 47 | 210 |
| 02:15 02:30 | 0 0 | | 1 1 | | | | | 1 1 | | 14:15 14:30 | 31 36 | | 22 21 | | | | | | 53 57 | |
| 02:45 | 1 | 1 | 1 | 3 | | | | 2 | 4 | 14:45 | 23 | 113 | 25 | 92 | | | | | 48 | 205 |
| 03:00 03:15 | 0 1 | | 0 | | | | | 0 | | 15:00 15:15 | 24 15 | | 36 32 | | | | | | 60 47 | |
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| 05:30 05:45 | 2 2 | 6 | 1 3 | 5 | | | | 3 5 | 11 | 17:30 17:45 | 23 30 | 101 | 48 65 | 219 | | | | | 71 95 | 320 |
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| 06:45 | 14 | 38 | 12 | 23 | | | | 26 | 61 | 18:45 | 18 | 83 | 46 | 188 | | | | | 64 | 271 |
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| 07:45 08:00 | 27 26 | 90 | 29 25 | 100 | | | | 56 51 | 190 | 19:45 20:00 | 16 8 | 57 | 19 21 | 90 | | | | | 35 29 | 147 |
| 08:15 | 36 | | 29 | | | | | 65 | | 20:15 | 15 | | 19 | | | | | | 34 | |
| 08:30 08:45 | 33 30 | 125 | 25 31 | 110 | | | | 58 61 | 235 | 20:30 20:45 | 6 9 | 38 | 19 20 | 79 | | | | | 25 29 | 117 |
| 09:00 | 28 | 123 | 35 | 110 | | | | 63 | 200 | 21:00 | 9 | | 16 | 17 | | | | | 25 | 117 |
| 09:15 09:30 | 21 29 | | 33 27 | | | | | 54 56 | | 21:15 21:30 | 13 11 | | 13 18 | | | | | | 26 29 | |
| 09:45 | 31 | 109 | 30 | 125 | | | | 61 | 234 | 21:45 | 6 | 39 | 10 | 57 | | | | | 16 | 96 |
| 10:00 10:15 | 36 29 | | 17 18 | | | | | 53 47 | | 22:00 22:15 | 3 5 | | 8 9 | | | | | | 11 14 | |
| 10:30 | 43 | | 27 | | | | | 70 | | 22:30 | 4 | | 12 | | | | | | 16 | |
| 10:45 | 17 32 | 125 | 29 25 | 91 | | | | 46 57 | 216 | 22:45 23:00 | 4 | 16 | 8 | 37 | | | | | 12 | 53 |
| 11:00 11:15 | 36 | | 24 | | | | | 60 | | 23:15 | 2 5 | | 7 | | | | | | 6 12 | |
| 11:30 | 27 | 100 | 18 | 07 | | | | 45 | 220 | 23:30 | 5 | 1 / | 9 | 21 | | | | | 14 3 | 25 |
| 11:45 TOTALS | | 123 642 | 30 | 97 570 | | | | 58 | 220 1212 | 23:45 TOTALS | 2 | 912 | ı | 21 1360 | | | | | 3 | 35 2272 |
| SPLIT % | | 53.0% | | 47.0% | | | | | 34.8% | | | | | 59.9% | | | | | | 65.2% |
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| | | | | | | 1,554 | | 1,930 | | 0 | | 0 | | | | | | | 3,4 | 184 |
| AM Peak Hour | | 09:45 | | 08:45 | | | | | 08:15 | PM Peak Hour | | 16:00 | | 16:30 | | | | | | 16:00 |
| AM Pk Volume Pk Hr Factor | | 139 0.808 | | 126 0.900 | | | | | 247 0.950 | PM Pk Volume Pk Hr Factor | | 145 0.884 | | 239 0.842 | | | | | | 380 0.896 |
| 7 - 9 Volume | | 215 | | 210 | 0 | | 0 | | 425 | 4 - 6 Volume | | 246 | | 454 | | 0 | | 0 | | 700 |
| 7 - 9 Peak Hour | | 08:00 | | 08:00 | | | | | 08:00 | 4 - 6 Peak Hour | | 16:00 | | 16:30 | | | | | | 16:00 |
| 7 - 9 Pk Volume | | 125 | | 110 0.997 | | | | | | 4 - 6 Pk Volume Pk Hr Factor | | 145 | | 239 | | | | | | 380 |
| Pk Hr Factor | | 0.868 | | 0.887 | 0.00 | U | 0.000 | | 0.904 | FK TIL FACTOI | | 0.884 | | 0.842 | | 0.000 | | 0.000 | | 0.896 |

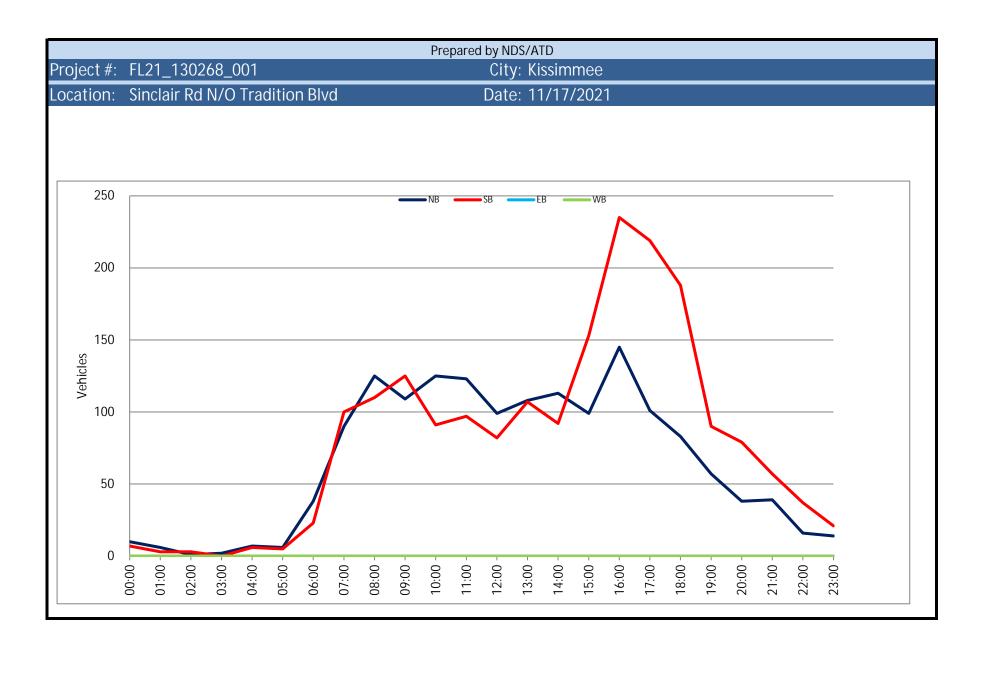
Prepared by NDS/ATD VOLUME

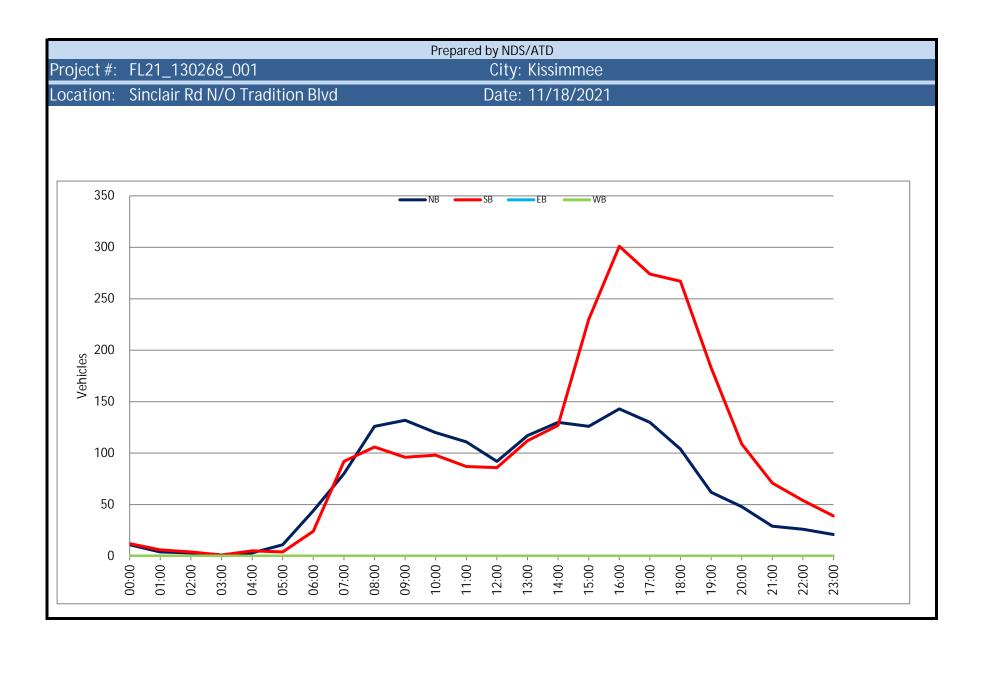
Sinclair Rd N/O Tradition Blvd

Day: Thursday Date: 11/18/2021 City: Kissimmee Project #: FL21_130268_001

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| | DΡ | VIL I | O1F | 1LJ | | 1,674 | | 2,388 | | 0 | | 0 | | | | | | | 4,0 | 062 |
| AM Period | NB | | SB | | EB | WB | | TO | TAL | PM Period | NB | | SB | | EB | V | VB | | TO | TAL |
| 00:00 | 4 | | 3 | | | | | 7 | | 12:00 | 26 | | 17 | | | | | | 43 | |
| 00:15 | 4 | | 4 | | | | | 8 | | 12:15 | 25 | | 22 | | | | | | 47 | |
| 00:30 00:45 | 3 0 | 11 | 3 | 12 | | | | 6 | 23 | 12:30 12:45 | 15 26 | 92 | 22 25 | 86 | | | | | 37 51 | 178 |
| 01:00 | 1 | 11 | 2 | 12 | | | | 3 | 23 | 13:00 | 30 | 72 | 28 | 00 | | | | | 58 | 170 |
| 01:15 | 1 | | 3 | | | | | 4 | | 13:15 | 18 | | 20 | | | | | | 38 | |
| 01:30 | 1 | | 1 | , | | | | 2 | 4.0 | 13:30 | 31 | 447 | 31 | 440 | | | | | 62 | 000 |
| 01:45 02:00 | 0 | 4 | <u>0</u> 2 | 6 | | | | 2 | 10 | 13:45 14:00 | 38 43 | 117 | 33 28 | 112 | | | | | 71 71 | 229 |
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| 02:30 | 1 | | 2 | | | | | 3 | | 14:30 | 22 | | 33 | | | | | | 55 | |
| 02:45 | 1 | 3 | 0 | 4 | | | | 1 | 7 | 14:45 | 43 | 130 | 37 | 127 | | | | | 80 | 257 |
| 03:00 03:15 | 0 | | 0 | | | | | 1 | | 15:00 15:15 | 31 40 | | 58 51 | | | | | | 89 91 | |
| 03:13 | 0 | | 0 | | | | | 0 | | 15:30 | 32 | | 64 | | | | | | 96 | |
| 03:45 | 0 | 1 | 0 | 1 | | | | 0 | 2 | 15:45 | 23 | 126 | 57 | 230 | | | | | 80 | 356 |
| 04:00 | 0 | | 0 | | | | | 0 | | 16:00 | 36 | | 71 | | | | | | 107 | |
| 04:15 04:30 | 0 2 | | 0 1 | | | | | 0 3 | | 16:15 16:30 | 40 33 | | 78 67 | | | | | | 118 100 | |
| 04:45 | 1 | 3 | 4 | 5 | | | | 5 | 8 | 16:45 | 34 | 143 | 85 | 301 | | | | | 119 | 444 |
| 05:00 | 4 | | 1 | | | | | 5 | | 17:00 | 19 | | 75 | | | | | | 94 | |
| 05:15 | 3 | | 0 | | | | | 3 | | 17:15 | 45 | | 81 | | | | | | 126 | |
| 05:30 05:45 | 3 | 11 | 2 1 | 4 | | | | 3 1 | 15 | 17:30 17:45 | 30 36 | 130 | 57 61 | 274 | | | | | 87 97 | 404 |
| 06:00 | 4 | 11 | 2 | _ | | | | 6 | 13 | 18:00 | 31 | 130 | 67 | 217 | | | | | 98 | 707 |
| 06:15 | 10 | | 5 | | | | | 15 | | 18:15 | 23 | | 62 | | | | | | 85 | |
| 06:30 | 16 | 4.4 | 6 | 2.4 | | | | 22 | 40 | 18:30 | 25 | 104 | 60 | 2/7 | | | | | 85 | 271 |
| 06:45 07:00 | 14 17 | 44 | 11 23 | 24 | | | | 25 40 | 68 | 18:45 19:00 | 25 19 | 104 | 78 52 | 267 | | | | | 103 71 | 371 |
| 07:15 | 19 | | 26 | | | | | 45 | | 19:15 | 20 | | 59 | | | | | | 79 | |
| 07:30 | 16 | | 14 | | | | | 30 | | 19:30 | 14 | | 52 | | | | | | 66 | |
| 07:45 | 28 26 | 80 | 29 32 | 92 | | | | 57 58 | 172 | 19:45 20:00 | 9 11 | 62 | 20 35 | 183 | | | | | 29 46 | 245 |
| 08:00 08:15 | 43 | | 32 18 | | | | | 61 | | 20:15 | 12 | | 35 19 | | | | | | 31 | |
| 08:30 | 29 | | 25 | | | | | 54 | | 20:30 | 10 | | 28 | | | | | | 38 | |
| 08:45 | 28 | 126 | 31 | 106 | | | | 59 | 232 | 20:45 | 15 | 48 | 27 | 109 | | | | | 42 | 157 |
| 09:00 09:15 | 26 30 | | 21 25 | | | | | 47 55 | | 21:00 21:15 | 8 12 | | 27 17 | | | | | | 35 29 | |
| 09:13 | 37 | | 30 | | | | | 67 | | 21:30 | 0 | | 15 | | | | | | 15 | |
| 09:45 | 39 | 132 | 20 | 96 | | | | 59 | 228 | 21:45 | 9 | 29 | 12 | 71 | | | | | 21 | 100 |
| 10:00 | 26 | | 26 | | | | | 52 | | 22:00 | 7 | | 11 | | | | | | 18 | |
| 10:15 10:30 | 28 34 | | 26 19 | | | | | 54 53 | | 22:15 22:30 | 9 | | 9 18 | | | | | | 16 27 | |
| 10:35 | 32 | 120 | 27 | 98 | | | | 59 | 218 | 22:45 | 3 | 26 | 16 | 54 | | | | | 19 | 80 |
| 11:00 | 26 | | 20 | | | | | 46 | | 23:00 | 5 | | 12 | | | | | | 17 | |
| 11:15 | 38 | | 18 | | | | | 56 50 | | 23:15 | 9 | | 8 | | | | | | 17 | |
| 11:30 11:45 | 27 20 | 111 | 23 26 | 87 | | | | 50 46 | 198 | 23:30 23:45 | 6 1 | 21 | 13 6 | 39 | | | | | 19 7 | 60 |
| TOTALS | 20 | 646 | 20 | 535 | | | | 70 | 1181 | TOTALS | ı | 1028 | J | 1853 | | | | | , | 2881 |
| | | | | | | | | | | | | | | | | | | | | |
| SPLIT % | | 54.7% | | 45.3% | | | | | 29.1% | SPLIT % | | 35.7% | | 64.3% | | | | | | 70.9% |
| | D_4 | AILY T | | \ C | | NB | | SB | | EB | | WB | | | | | | | To | otal |
| | - DP | KILY I | OIF | 1LJ | | 1,674 | | 2,388 | | 0 | | 0 | | | | | | | 4,0 | 062 |
| AM Peak Hour | | 09:00 | | 08:45 | | | | | 09:15 | PM Peak Hour | | 14:45 | | 16:30 | | | | | | 16:00 |
| AM Pk Volume | | 132 | | 107 | | | | | 233 | PM Pk Volume | | 146 | | 308 | | | | | | 444 |
| Pk Hr Factor | | 0.846 | | 0.863 | | | | | 0.869 | Pk Hr Factor | | 0.849 | | 0.906 | | | | | | 0.933 |
| 7 - 9 Volume | | 206 | | 198 | 0 | | 0 | | 404 | 4 - 6 Volume | | 273 | | 575 | | 0 | | 0 | | 848 |
| 7 - 9 Peak Hour | | 07:45 | | 08:00 | | | | | | 4 - 6 Peak Hour | | 16:00 | | 16:30 | | | | | | 16:00 |
| 7 - 9 Pk Volume | | 126 | | 106 | | | | | 232 | 4 - 6 Pk Volume | | 143 | | 308 | | | | | | 444 |
| Pk Hr Factor | | 0.733 | | 0.828 | 0.00 | J | 0.000 | | 0.951 | Pk Hr Factor | | 0.894 | | 0.906 | 0 | 0.000 | U. | 000 | | 0.933 |







VOLUME Happy Trail W/O Sinclair Rd

Day: Tuesday Date: 11/16/2021 City: Davenport Project #: FL21_130268_002

| | DAILY TOTALS | | _ | NB | SB | | EB | | WB_ | | | | | | | otal |
|---------------------------------|--------------|---------------|-------------|-------------|----------|-------------|---------------------------------|----|-------|------|---------------|-------------|----------------|-------------|----------|---------------|
| | | | | 0 | 0 | | 492 | | 328 | _ | | | | | | 20 |
| AM Period 00:00 | NB SB | EB | | WB 3 | _ | TAL | PM Period 12:00 | NB | S | SB | EB 8 | | WB | | TO 14 | TAL |
| 00:00 | | 0 | | 0 | 4 0 | | 12:00 | | | | 6 | | 6 4 | | 10 | |
| 00:30 | | 1 | • | 1 | 2 | 0 | 12:30 | | | | 4 | 0.0 | 4 | 10 | 8 | 0.0 |
| 00:45 01:00 | | <u>1</u> 1 | 3 | 1 5 0 | 2 | 8 | 12:45 13:00 | | | | <u>2</u> 4 | 20 | <u>4</u> 2 | 18 | 6 | 38 |
| 01:15 | | Ö | | 0 | Ö | | 13:15 | | | | 9 | | 4 | | 13 | |
| 01:30 01:45 | | 2 | 3 | 0 | 2 | 3 | 13:30 13:45 | | | | 6 5 | 24 | 4 | 1./ | 10 9 | 38 |
| 02:00 | | 2 | ა | 1 | 3 | <u> </u> | 14:00 | | | | 8 | 24 | 4 5 | 14 | 13 | 30 |
| 02:15 | | 1 | | 1 | 2 | | 14:15 | | | | 7 | | 5 | | 12 | |
| 02:30 02:45 | | 1 0 | 4 | 0 2 | 0 | 6 | 14:30 14:45 | | | | 13 9 | 37 | 8 5 | 23 | 21 14 | 60 |
| 03:00 | | 0 | · · | 0 | 0 | | 15:00 | | | | 17 | <u> </u> | 10 | | 27 | 30 |
| 03:15 03:30 | | 0 | | 2 | 2 | | 15:15 15:30 | | | | 11 12 | | 3 1 | | 14 16 | |
| 03:45 | | 1 | 1 | 0 2 | 1 | 3 | 15:45 | | | | 2 | 42 | 4 | 21 | 6 | 63 |
| 04:00 | | 0 | | 0 | 0 | | 16:00 | | | | 6 | | 13 | | 19 | |
| 04:15 04:30 | | 1 1 | | 0 1 | 2 | | 16:15 16:30 | | | | 8 8 | | 10 9 | | 18 17 | |
| 04:45 | | 1 | 3 | 0 1 | 1 | 4 | 16:45 | | | | 9 | 31 | 10 | 42 | 19 | 73 |
| 05:00 05:15 | | 3 1 | | 2 | 5 1 | | 17:00 17:15 | | | | 5 5 | | 8 8 | | 13 13 | |
| 05:30 | | 4 | | 0 | 4 | | 17:13 | | | | 8 | | 8 | | 16 | |
| 05:45 | | 4 | 12 | 0 2 | 4 | 14 | 17:45 | | | | 5 | 23 | 11 | 35 | 16 | 58 |
| 06:00 06:15 | | ა 5 | | 1 | 4 6 | | 18:00 18:15 | | | | 9 8 | | 8 | | 16 16 | |
| 06:30 | | 7 | | 2 | 9 | | 18:30 | | | | 7 | | 11 | | 18 | |
| 06:45 07:00 | | 13 14 | 28 | 1 5 3 | 14 17 | 33 | 18:45 19:00 | | | | <u>2</u> 1 | 26 | <u>3</u> 8 | 29 | 5 12 | 55 |
| 07:15 | | 10 | | 1 | 11 | | 19:15 | | | | 2 | | 4 | | 6 | |
| 07:30 07:45 | | 13 13 | 50 | 4 3 11 | 17 16 | 61 | 19:30 19:45 | | | | 3 5 | 14 | 6 5 | 23 | 9 10 | 37 |
| 08:00 | | 14 | | 4 | 18 | U I | 20:00 | | | | 2 | 14 | 4 | 23 | 6 | 37 |
| 08:15 | | 11 | | 2 | 13 | | 20:15 | | | | 4 | | 3 | | 7 | |
| 08:30 08:45 | | 14 11 | 50 | 7 3 16 | 21 14 | 66 | 20:30 20:45 | | | | 2 | 10 | 2 4 | 13 | 6 | 23 |
| 09:00 | | 13 | | 3 | 16 | | 21:00 | | | | 2 | - | 4 | - | 6 | |
| 09:15 09:30 | | 14 7 | | 1 0 | 15 7 | | 21:15 21:30 | | | | 1 3 | | 2 0 | | 3 | |
| 09:45 | | 5 | 39 | 3 7 | 8 | 46 | 21:45 | | | | 0 | 6 | 2 | 8 | 2 | 14 |
| 10:00 | | 8 | | 7 | 15 o | | 22:00 22:15 | | | | 0 | | 4 | | 4 | |
| 10:15 10:30 | | 5 13 | | 7 | 8 20 | | 22:30 | | | | 2 | | 0 | | 2 | |
| 10:45 | | 3 | 29 | 4 21 | 7 | 50 | 22:45 | | | | 1 | 4 | 1 | 6 | 2 | 10 |
| 11:00 11:15 | | 9 7 | | 3 | 12 13 | | 23:00 23:15 | | | | U 1 | | 1 1 | | 2 | |
| 11:30 | | 8 | | 3 | 11 | | 23:30 | | | | 1 | • | 1 | | 2 | |
| 11:45 TOTALS | | 7 | 31 253 | 9 21 93 | 16 | 52 | 23:45 TOTALS | | | | 0 | 239 | 0 | 3 | 0 | 5 474 |
| | | | | | | 346 | | | | | | | | 235 | | 474 57.99/ |
| SPLIT % | | | 73.1% | 26.9% | | 42.2% | | | | | | 50.4% | | 49.6% | | 57.8% |
| | DAILY TOTALS | | | NB | SB | | EB | | WB | | | | | | | otal |
| | | | | 0 | 0 | | 492 | | 328 | | | | | | 82 | 20 |
| AM Peak Hour AM Pk Volume | | | 07:45 52 | 11:15 24 | | 07:45 68 | PM Peak Hour PM Pk Volume | | | | | 14:30 50 | | 16:00 | | 14:30 76 |
| Pk Hr Factor | | | 52 0.929 | 24 0.667 | | 0.810 | Pk Hr Factor | | | | | 50 0.735 | | 42 0.808 | | 0.704 |
| 7 - 9 Volume | 0 0 | | 100 | 27 | | 127 | 4 - 6 Volume | | 0 | 0 | | 54 | | 77 | | 131 |
| 7 - 9 Peak Hour | | | 07:45 | 07:45 | | | 4 - 6 Peak Hour | | | | | 16:00 | | 16:00 | | 16:00 |
| 7 - 9 Pk Volume Pk Hr Factor | | | 52 0.929 | 16 0.571 | | 68 0.810 | 4 - 6 Pk Volume Pk Hr Factor | | | | | 31 0.861 | | 42 0.808 | | 73 0.961 |
| 1 K TII T dollor | 3.000 | | 0.727 | 0.071 | | 0.010 | TRAIL TUCTOR | | 0.000 | 0.00 | | 0.001 | | 0.000 | | 0.701 |

VOLUME Happy Trail W/O Sinclair Rd

Day: Wednesday Date: 11/17/2021 City: Davenport Project #: FL21_130268_002

| | | NB 0 | | SB 0 | EB WB 472 322 | | | | | | | | Total 794 | | |
|---------------------------------|-------------|------------------------|-------------|-----------------------|------------------|--------------|---------------------------------|-------|--------------|----------|-------------|---------------|--------------|----------|-------------|
| AM Period | NB SB | EB | | WB | | TOTAL | PM Period | NB | SB | EB | | WB | | TO | TAL |
| 00:00 00:15 | | 0 | | 2 1 | | 2 2 | 12:00 12:15 | | | 10 6 | | 7 6 | | 17 12 | |
| 00:30 | | 0 | | Ö | | 0 | 12:30 | | | 8 | | 6 | | 14 | |
| 00:45 01:00 | | 0 | 11 | 1 4 0 | | 1 5 0 | 12:45 13:00 | | | 3 | 27 | <u>4</u> 3 | 23 | | 50 |
| 01:15 | | 0 | | 1 | | 1 | 13:15 | | | 13 | | 5 | | 18 | |
| 01:30 01:45 | | 0 | | 0 0 1 | | 0 0 1 | 13:30 13:45 | | | 7 7 | 30 | 4 6 | 18 | 11 13 | 48 |
| 02:00 | | 0 | | 0 | | 0 | 14:00 | | | 7 | 30 | 2 | 10 | 9 | 40 |
| 02:15 02:30 | | 0 | | 0 | | 0 | 14:15 14:30 | | | 7 12 | | 9 5 | | 16 17 | |
| 02:45 | | 0 | 2 | 1 1 | | 1 3 | 14:45 | | | 8 | 34 | 6 | 22 | 14 | 56 |
| 03:00 03:15 | | 1 | | 1 0 | | 2 | 15:00 15:15 | | | 8 6 | | 3 8 | | 11 14 | |
| 03:30 | | 0 | | 1 | | 1 | 15:30 | | | 5 | | 6 | | 11 | |
| 03:45 04:00 | | <u>2</u> 1 | 3 | 2 4 1 | | <u>4</u> 7 | 15:45 16:00 | | | 6 4 | 25 | <u>9</u> 7 | 26 | 15 11 | 51 |
| 04:15 | | 1 | | 0 | | 1 | 16:15 | | | 4 | | 13 | | 17 | |
| 04:30 04:45 | | 1 | 5 | 0 0 1 | | 1 2 6 | 16:30 16:45 | | | 3 7 | 18 | 11 4 | 35 | 14 11 | 53 |
| 05:00 | | 2 | | 0 | | 2 | 17:00 | | | 12 | | 4 | | 16 | |
| 05:15 05:30 | | 2 | | 0 | | 2 | 17:15 17:30 | | | / 4 | | 9 6 | | 16 10 | |
| 05:45 | | 5 | 11 | 0 | | 5 11 | 17:45 | | | 5 | 28 | 3 | 22 | 8 | 50 |
| 06:00 06:15 | | 6 4 | | 0 | | 6 4 | 18:00 18:15 | | | 12 5 | | 12 8 | | 24 13 | |
| 06:30 | | 5 | 0.0 | 0 | | 5 | 18:30 | | | 6 | 0.4 | 6 | 0.4 | 12 | |
| 06:45 07:00 | | 13 14 | 28 | 5 5 2 | | 18 33 16 | 18:45 19:00 | | | 8 | 34 | 8 10 | 34 | 19 18 | 68 |
| 07:15 | | 17 | | 5 | | 22 | 19:15 | | | 3 | | 4 | | 7 | |
| 07:30 07:45 | | 10 | 48 | 1 3 1 | | 8 13 59 | 19:30 19:45 | | | 4 2 | 17 | 2 3 | 19 | 6 5 | 36 |
| 08:00 | | 13 | | 2 | | 15 | 20:00 | | | 4 | | 3 | | 7 | |
| 08:15 08:30 | | / 9 | | 7 | | 9 16 | 20:15 20:30 | | | 0 1 | | 5 3 | | 5 4 | |
| 08:45 | | 4 | 33 | 2 13 | | 6 46 | 20:45 | | | 2 | 7 | 6 | 17 | 8 | 24 |
| 09:00 09:15 | | 20 8 | | 4 8 | | 24 16 | 21:00 21:15 | | | 5 1 | | 0 | | 6 1 | |
| 09:30 | | 5 | 41 | 4 | | 9 | 21:30 | | | 2 | 0 | 1 | 0 | 3 | 17 |
| 09:45 10:00 | | <u>8</u> 15 | 41 | 3 19 | ' | 11 60 15 | 21:45 22:00 | | | <u> </u> | 9 | <u>6</u> 1 | 8 | 2 | 17 |
| 10:15 | | 7 | | 2 | | 9 | 22:15 | | | 4 | | 3 | | 7 | |
| 10:30 10:45 | | 3 | 30 | 3 6 | | 6 6 36 | 22:30 22:45 | | | 0 | 5 | 1 | 6 | 1 1 | 11 |
| 11:00 | | 10 | | 3 | | 13 | 23:00 | | | 0 | | 0 | | 0 | |
| 11:15 11:30 | | 5 7 | | 5 5 | | 10 12 | 23:15 23:30 | | | 1 1 | | 2 1 | | 3 2 | |
| 11:45 | | 12 | 34 | 9 22 | | 21 56 | 23:45 | | | 0 | 2 | 2 | 5 | 2 | 7 |
| TOTALS | | | 236 | 87 | | 323 | TOTALS | | | | 236 | | 235 | | 471 |
| SPLIT % | | | 73.1% | 26. | 9% | 40.7% | SPLIT % | | | | 50.1% | | 49.9% | | 59.3% |
| | DAILY TOTAL | AILY TOTALS NB SB 0 0 | | | EB WB 472 322 | | | | Total 794 | | | | | | |
| AM Peak Hour | | | 06:45 | 11: | | 06:45 | PM Peak Hour | | | | 14:15 | | 15:45 | | 18:00 |
| AM Pk Volume | | | 51 0.750 | 28 | | 64 0.727 | PM Pk Volume | | | | 35 0.720 | | 40 | | 68 |
| Pk Hr Factor 7 - 9 Volume | 0 | 0 | 0.750 81 | 0.7 | | 0.727 105 | Pk Hr Factor 4 - 6 Volume | 0 | | 0 | 0.729 46 | | 0.769 57 | | 0.708 |
| 7 - 9 Peak Hour | | | 07:00 | 07: | 45 | 07:00 | 4 - 6 Peak Hour | | | | 16:45 | | 16:00 | | 16:15 |
| 7 - 9 Pk Volume Pk Hr Factor | | | 48 0.706 | 1 ₄ 0.5 | | 59 0.670 | 4 - 6 Pk Volume Pk Hr Factor | | | | 30 0.625 | | 35 0.673 | | 58 0.853 |
| TIXTII T dCtOI | | | 0.700 | 0.0 | | 0.070 | T KTII T dottor | 0.000 | | | 0.023 | | 0.073 | | 0.000 |

VOLUME Happy Trail W/O Sinclair Rd

City: Davenport Project #: FL21_130268_002

39

0.696

0.750

66

0.825

Day: Thursday Date: 11/18/2021

Pk Hr Factor

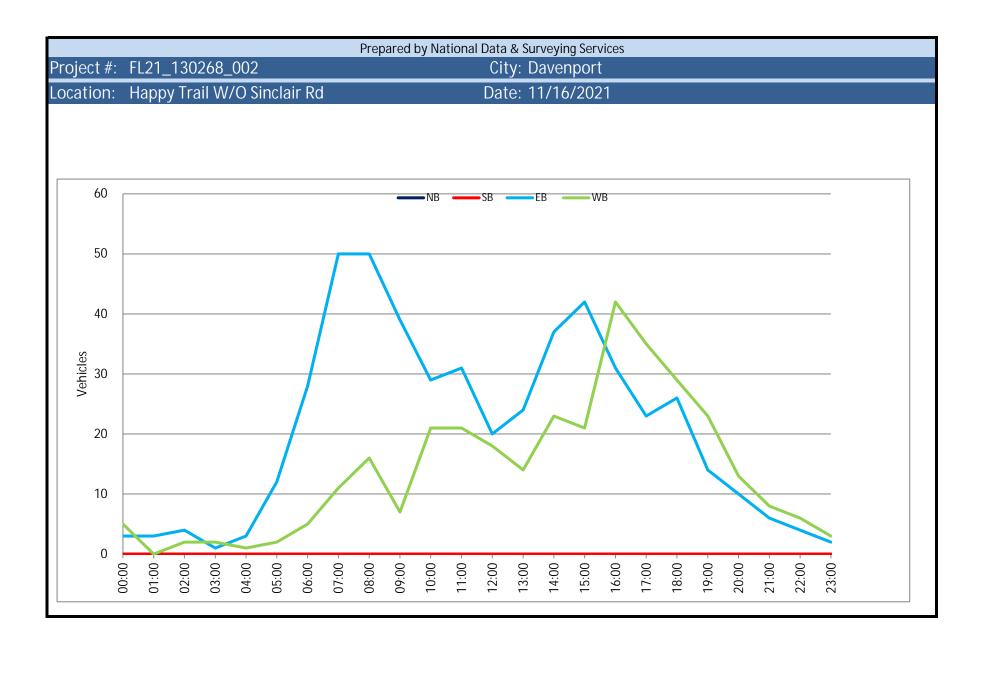
0.803

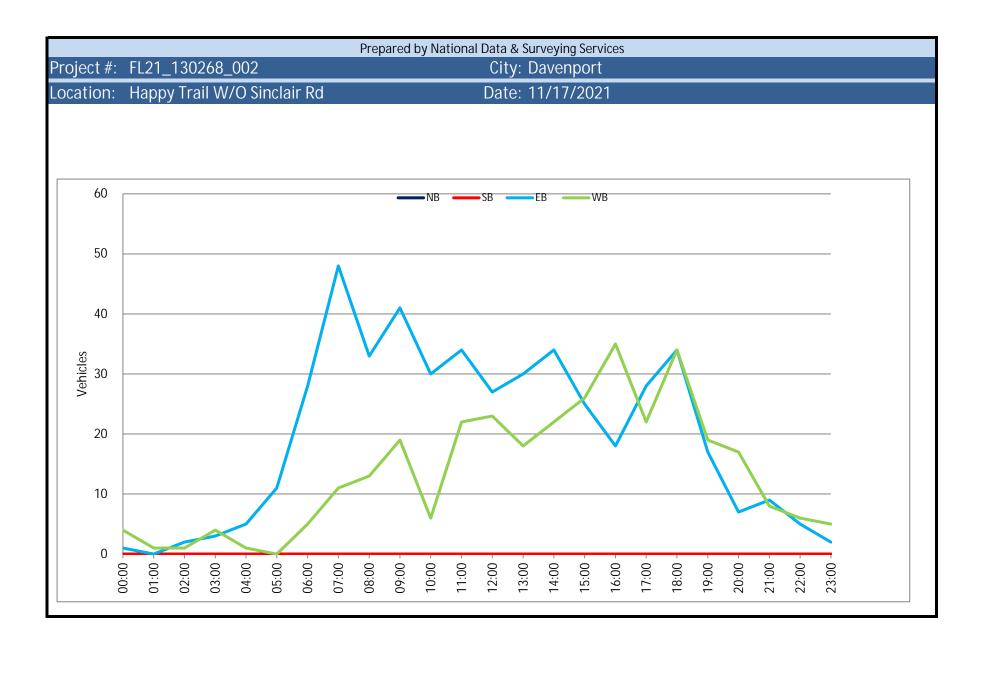
0.750

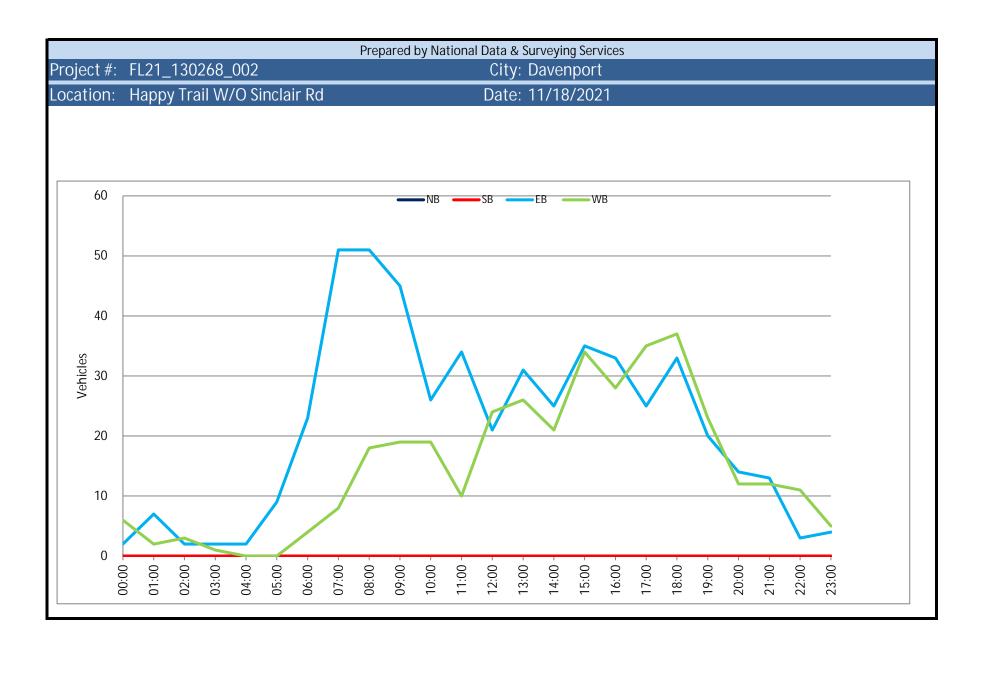
0.913

Pk Hr Factor

SB EB WB NB **Total DAILY TOTALS** 358 511 869 0 0 PM Period SB **TOTAL** AM Period SB WB **TOTAL** NB WB NB EB EB 00:00 12:00 2 14 00:15 0 2 12:15 9 2 00:30 12:30 14 0 00:45 0 12:45 2 0 6 0 8 21 24 8 45 01:00 13:00 10 13:15 10 01:15 0 19 13:30 01:30 5 14 6 6 01:45 7 9 13:45 11 31 26 14 57 02:00 14:00 0 0 13 6 02:15 0 0 0 14:15 2 9 02:30 14:30 2 2 11 6 02:45 0 2 3 5 14:45 25 21 13 46 03:00 15:00 0 5 10 15 03:15 0 15:15 21 14 7 03:30 15:30 0 3 7 03:45 0 15:45 13 13 26 2 3 35 34 69 04:00 16:00 11 18 04:15 0 16:15 8 0 0 4 04:30 16:30 10 0 18 16:45 0 8 04:45 2 0 2 33 28 17 61 05:00 17:00 0 13 6 2 2 17:15 9 05:15 16 05:30 17:30 3 3 14 20 0 6 05:45 17:45 3 3 9 0 9 25 11 6 35 60 06:00 18:00 17 9 8 8 18:15 12 06:15 13 25 0 18:30 06:30 5 8 16 06:45 18:45 12 23 27 33 37 70 07:00 19:00 11 11 14 07:15 12 15 19:15 8 3 6 07:30 19 19:30 20 8 07:45 13 8 19:45 13 51 20 23 43 20:00 08:00 18 20 08:15 15 5 20 20:15 2 4 6 20 20:30 08:30 15 5 6 8 20:45 08:45 18 69 51 6 14 12 26 21:00 09:00 13 2 09:15 18 25 21:15 10 8 21:30 09:30 11 14 6 09:45 19 12 21:45 25 45 64 13 12 22:00 10:00 9 15 10:15 6 5 11 22:15 0 4 22:30 10:30 5 7 7 10:45 6 26 19 45 22:45 11 14 6 23:00 11:00 9 11:15 8 12 23:15 2 11:30 10 23:30 2 11:45 10 34 10 13 44 23:45 0 **TOTALS** 268 254 90 **TOTALS** 257 344 525 73.8% 39.6% SPLIT % 51.0% SPLIT % 26.2% 49.0% 60.4% NB SB EB WB Total **DAILY TOTALS** 358 511 869 0 0 **AM Peak Hour** 07:30 08:30 PM Peak Hour 15:15 17:30 17:30 07:30 PM Pk Volume AM Pk Volume 61 24 73 41 40 73 Pk Hr Factor 0.803 0.857 0.913 Pk Hr Factor 0.732 0.714 0.730 7 - 9 Volume 102 26 58 128 4 - 6 Volume 63 121 07:30 08:00 4 - 6 Peak Hour 7 - 9 Peak Hour 07:30 16:00 16:45 16:45 7 - 9 Pk Volume 61 18 73 4 - 6 Pk Volume 33







VOLUME

Bella Citta Blvd W/O S Goodman Rd

Day: Tuesday Date: 11/16/2021

| | DAILY TOTALS | 5 | | NB | | SB | | EB | | /B | | | | | | otal |
|---------------------------------|--------------|----------|--------------|----------|--------------|----------------|--------------|---------------------------------|-----|-----------|-----------|--------------|----------|--------------|------------|--------------|
| | DITTE TOTALS | | | 0 | | 0 | | 4,551 | 4,5 | 578 | | | | | 9,1 | 129 |
| AM Period | NB SB | EB | | WB | | TO | TAL | PM Period | NB | SB | EB | | WB | | TO | TAL |
| 00:00 | | 12 | | 28 | | 40 | | 12:00 | | | 75 | | 62 | | 137 | |
| 00:15 | | 10 | | 38 | | 48 | | 12:15 | | | 71 | | 64 | | 135 | |
| 00:30 | | 10 | 20 | 32 | 107 | 42 | 1// | 12:30 | | | 65 45 | 27/ | 58 54 | 220 | 123 | E1.4 |
| 00:45 01:00 | | | 39 | 29 22 | 127 | 36 27 | 166 | 12:45 13:00 | | | 65 71 | 276 | 54 66 | 238 | 119 137 | 514 |
| 01:00 | | 5 7 | | 13 | | 20 | | 13:15 | | | 55 | | 62 | | 117 | |
| 01:30 | | 7 | | 15 | | 22 | | 13:30 | | | 81 | | 76 | | 157 | |
| 01:45 | | 4 | 23 | 9 | 59 | 13 | 82 | 13:45 | | | 74 | 281 | 73 | 277 | 147 | 558 |
| 02:00 | | 4 | | 17 | | 21 | | 14:00 | | | 50 | | 70 | | 120 | |
| 02:15 | | 2 | | 15 | | 17 | | 14:15 | | | 64 | | 73 | | 137 | |
| 02:30 | | 1 | 11 | 9 | ΓO | 10 | () | 14:30 | | | 59 72 | 245 | 81 | 212 | 140 | ГГО |
| 02:45 03:00 | | 4 8 | 11 | 11 5 | 52 | 15 13 | 63 | 14:45 15:00 | | | 72 137 | 245 | 89 89 | 313 | 161 226 | 558 |
| 03:15 | | 6 | | 6 | | 12 | | 15:15 | | | 109 | | 78 | | 187 | |
| 03:30 | | 5 | | 7 | | 12 | | 15:30 | | | 87 | | 65 | | 152 | |
| 03:45 | | 3 | 22 | 4 | 22 | 7 | 44 | 15:45 | | | 72 | 405 | 75 | 307 | 147 | 712 |
| 04:00 | | 12 | | 4 | | 16 | | 16:00 | | | 74 | | 86 | | 160 | |
| 04:15 | | 9 | | 6 | | 15 | | 16:15 | | | 94 | | 60 | | 154 | |
| 04:30 | | 21 | Ε0 | 8 | 22 | 29 | 00 | 16:30 | | | 88 | 220 | 62 | 202 | 150 | / 21 |
| 04:45 | | 16 26 | 58 | 14 9 | 32 | 30 35 | 90 | 16:45 17:00 | | | 73 | 329 | 94 91 | 302 | 167 | 631 |
| 05:00 05:15 | | 26 30 | | 9 10 | | 35 40 | | 17:00 17:15 | | | 85 76 | | 91 79 | | 176 155 | |
| 05:30 | | 29 | | 11 | | 40 | | 17:13 | | | 75 75 | | 77 | | 152 | |
| 05:45 | | 29 | 114 | 13 | 43 | 42 | 157 | 17:45 | | | 66 | 302 | 89 | 336 | 155 | 638 |
| 06:00 | | 45 | | 17 | | 62 | | 18:00 | | | 75 | | 95 | | 170 | |
| 06:15 | | 67 | | 14 | | 81 | | 18:15 | | | 65 | | 84 | | 149 | |
| 06:30 | | 74 | 070 | 17 | 0.1 | 91 | 074 | 18:30 | | | 53 | 000 | 64 | 200 | 117 | F 40 |
| 06:45 | | 84 56 | 270 | 43 53 | 91 | 127 109 | 361 | 18:45 19:00 | | | 46 40 | 239 | 66 68 | 309 | 112 108 | 548 |
| 07:00 07:15 | | 55 | | 55 75 | | 130 | | 19:00 19:15 | | | 56 | | 56 | | 112 | |
| 07:30 | | 89 | | 84 | | 173 | | 19:30 | | | 38 | | 70 | | 108 | |
| 07:45 | | 133 | 333 | 54 | 266 | 187 | 599 | 19:45 | | | 33 | 167 | 63 | 257 | 96 | 424 |
| 08:00 | | 56 | | 54 | | 110 | | 20:00 | | | 39 | | 63 | | 102 | |
| 08:15 | | 91 | | 42 | | 133 | | 20:15 | | | 29 | | 46 | | 75 | |
| 08:30 | | 91 | 220 | 37 | 170 | 128 | 400 | 20:30 | | | 29 | 100 | 53 | 212 | 82 | 225 |
| 08:45 09:00 | | 82 74 | 320 | 45 56 | 178 | 127 130 | 498 | 20:45 21:00 | | | 26 34 | 123 | 50 68 | 212 | 76 102 | 335 |
| 09:15 | | 54 | | 54 | | 108 | | 21:15 | | | 31 | | 48 | | 79 | |
| 09:30 | | 76 | | 51 | | 127 | | 21:30 | | | 19 | | 67 | | 86 | |
| 09:45 | | 66 | 270 | 40 | 201 | 106 | 471 | 21:45 | | | 18 | 102 | 49 | 232 | 67 | 334 |
| 10:00 | | 57 | | 45 | | 102 | | 22:00 | | | 14 | | 61 | | 75 | |
| 10:15 | | 71 | | 38 | | 109 | | 22:15 | | | 18 | | 49 | | 67 | |
| 10:30 | | 66 45 | 250 | 54 53 | 100 | 120 | 440 | 22:30 | | | 15 | EE | 37 53 | 100 | 52 | 2E.4 |
| 10:45 11:00 | | 65 54 | 259 | 52 41 | 189 | 117 95 | 448 | 22:45 23:00 | | | 8 13 | 55 | 52 29 | 199 | 60 42 | 254 |
| 11:15 | | 72 | | 50 | | 122 | | 23:15 | | | 13 | | 33 | | 42 46 | |
| 11:30 | | 72 | | 59 | | 131 | | 23:30 | | | 9 | | 43 | | 52 | |
| 11:45 | | 67 | 265 | 47 | 197 | 114 | 462 | 23:45 | | | 8 | 43 | 34 | 139 | 42 | 182 |
| TOTALS | | | 1984 | | 1457 | | 3441 | TOTALS | | | | 2567 | | 3121 | | 5688 |
| SPLIT % | | | 57.7% | | 42.3% | | 37.7% | SPLIT % | | | | 45.1% | | 54.9% | | 62.3% |
| | | | | ALD | | | | | | (D | | | | | | |
| | DAILY TOTALS | 5 | | NB 0 | | <u>SB</u> 0 | | EB 4,551 | | /B 578 | | | | | | otal 129 |
| | | | | U | | 0 | | | 4,0 | | | | | | 7, | |
| AM Peak Hour | | | 07:45 | | 07:15 | | 07:30 | PM Peak Hour | | | | 14:45 | | 17:30 | | 14:45 |
| AM Pk Volume | | | 371 | | 267 | | 603 | PM Pk Volume | | | | 405 | | 345 | | 726 |
| Pk Hr Factor | | 0 | 0.697 | | 0.795 | | 0.806 | Pk Hr Factor | | | 0 | 0.739 | | 0.908 | | 0.803 |
| 7 - 9 Volume | | | 653 | | 444 | | 1097 | 4 - 6 Volume | | | | 631 | | 638 | | 1269 |
| 7 - 9 Peak Hour | | | 07:45 271 | | 07:15 267 | | | 4 - 6 Peak Hour | | | | 16:15 340 | | 16:45 | | 16:45 650 |
| 7 - 9 Pk Volume Pk Hr Factor | | | 371 0.697 | | 267 0.795 | | 603 0.806 | 4 - 6 Pk Volume Pk Hr Factor | | | | 340 0.904 | | 341 0.907 | | 650 0.923 |
| TRITTACIO | 0.000 | .000 | 0.077 | | 0.793 | | 0.000 | T K TH T dCtOl | 0.0 | 700 | 0.000 | 0.704 | | 0.707 | | 0.723 |
| | | | | | | | | | | | | | | | | |

VOLUME

Bella Citta Blvd W/O S Goodman Rd

Day: Wednesday Date: 11/17/2021

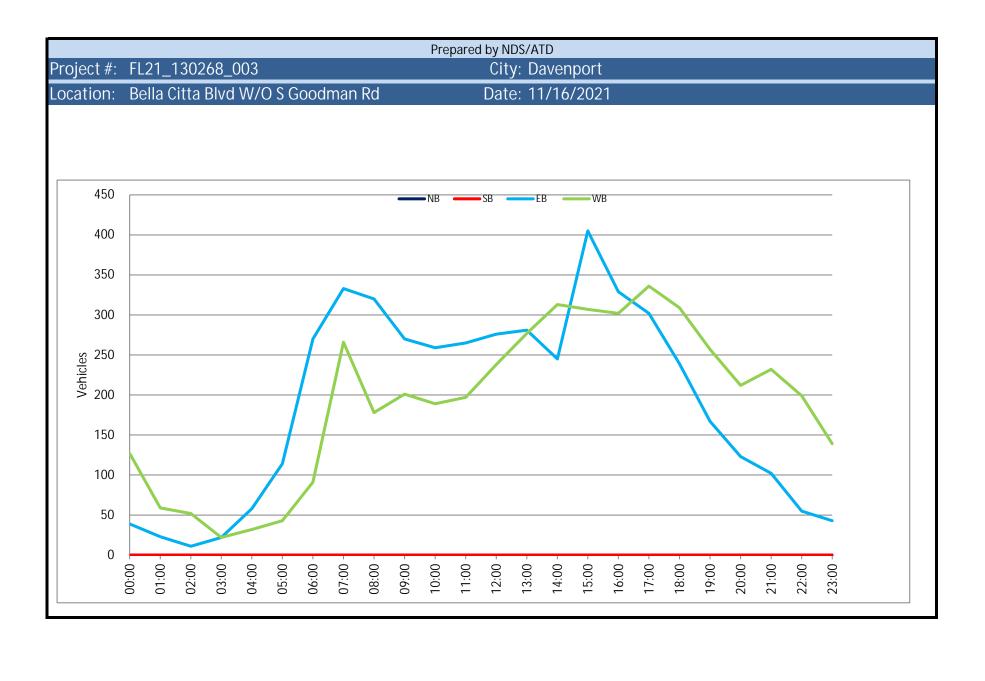
| | DAILY TOTALS | | | NB | | SB | | EB | | <u>/B</u> | | | | | | otal |
|---------------------------------|----------------|---------------|--------------|----------------|--------------|------------|--------------|---------------------------------|-----|-----------|-----------|--------------|-----------------|--------------|------------|--------------|
| | DI NET TOTILES | | | 0 | | 0 | | 4,497 | 4,5 | 808 | | | | | 9,(| 005 |
| AM Period | NB SB | EB | | WB | | TO | TAL | PM Period | NB | SB | EB | | WB | | TO | TAL |
| 00:00 | | 8 | | 25 | | 33 | | 12:00 | | | 82 50 | | 64 | | 146 | |
| 00:15 00:30 | | 5 1 | | 23 22 | | 28 26 | | 12:15 12:30 | | | 58 76 | | 64 58 | | 122 134 | |
| 00:45 | | 4 | 21 | 18 | 88 | 22 | 109 | 12:45 | | | 73 | 289 | 70 | 256 | 143 | 545 |
| 01:00 | | 5 | | 15 | | 20 | | 13:00 | | | 74 | | 53 | | 127 | |
| 01:15 | | 1 | | 16 | | 17 | | 13:15 13:30 | | | 76 | | 63 | | 139 127 | |
| 01:30 01:45 | | 2 | 13 | 11 6 | 48 | 16 8 | 61 | 13:45 | | | 67 68 | 285 | 60 69 | 245 | 137 | 530 |
| 02:00 | | 0 | | 5 | | 5 | | 14:00 | | | 69 | | 60 | | 129 | |
| 02:15 | | 0 | | 9 9 | | 9 | | 14:15 | | | 67 62 | | 72 | | 139 | |
| 02:30 02:45 | | 3 1 | 4 | 8 | 31 | 12 9 | 35 | 14:30 14:45 | | | 62 59 | 257 | 67 95 | 294 | 129 154 | 551 |
| 03:00 | | 6 | · · | 5 | 0. | 11 | | 15:00 | | | 132 | | 78 | | 210 | 301 |
| 03:15 | | 8 | | 4 | | 12 | | 15:15 | | | 116 | | 79 70 | | 195 | |
| 03:30 03:45 | | <i>1</i> 7 | 28 | 6 5 | 20 | 13 12 | 48 | 15:30 15:45 | | | 69 88 | 405 | 78 65 | 300 | 147 153 | 705 |
| 04:00 | | 8 | 20 | 1 | 20 | 9 | 10 | 16:00 | | | 51 | 100 | 84 | 300 | 135 | 700 |
| 04:15 | | 13 | | 6 | | 19 | | 16:15 | | | 75 | | 72 | | 147 | |
| 04:30 04:45 | | 12 11 | 44 | 3 16 | 26 | 15 27 | 70 | 16:30 16:45 | | | 78 77 | 281 | 72 84 | 312 | 150 161 | 593 |
| 05:00 | | 24 | 44 | 7 | 20 | 31 | 70 | 17:00 | | | 81 | 201 | 89 | 312 | 170 | 373 |
| 05:15 | | 35 | | 13 | | 48 | | 17:15 | | | 70 | | 70 | | 140 | |
| 05:30 05:45 | | 18 35 | 112 | 8 9 | 37 | 26 44 | 149 | 17:30 17:45 | | | 77 88 | 316 | 88 93 | 340 | 165 181 | 656 |
| 06:00 | | 50 | 112 | <u>9</u> 12 | 37 | 62 | 149 | 18:00 | | | 68 | 310 | 93 83 | 340 | 151 | 030 |
| 06:15 | | 54 | | 15 | | 69 | | 18:15 | | | 65 | | 86 | | 151 | |
| 06:30 | | 75 74 | 252 | 30 | 00 | 105 | 2.45 | 18:30 | | | 70 | 252 | 76 | 21.4 | 146 | F// |
| 06:45 07:00 | | 74 62 | 253 | 35 41 | 92 | 109 103 | 345 | 18:45 19:00 | | | 49 41 | 252 | 69 59 | 314 | 118 100 | 566 |
| 07:15 | | 72 | | 77 | | 149 | | 19:15 | | | 47 | | 65 | | 112 | |
| 07:30 | | 100 | 0.40 | 94 | 0.40 | 194 | (10 | 19:30 | | | 26 | 4.4 | 65 | 057 | 91 | 101 |
| 07:45 08:00 | | 115 76 | 349 | 51 49 | 263 | 166 125 | 612 | 19:45 20:00 | | | 50 32 | 164 | 68 62 | 257 | 118 94 | 421 |
| 08:15 | | 90 | | 43 | | 133 | | 20:15 | | | 35 | | 57 | | 92 | |
| 08:30 | | 92 | 0.40 | 48 | 100 | 140 | | 20:30 | | | 26 | 44- | 49 | 000 | 75 | 0.11 |
| 08:45 09:00 | | 85 69 | 343 | 49 48 | 189 | 134 117 | 532 | 20:45 21:00 | | | 22 26 | 115 | 61 51 | 229 | 83 77 | 344 |
| 09:15 | | 54 | | 46 | | 100 | | 21:15 | | | 14 | | 53 | | 67 | |
| 09:30 | | 67 | | 56 | | 123 | | 21:30 | | | 22 | | 48 | | 70 | |
| 09:45 10:00 | | 68 61 | 258 | 41 53 | 191 | 109 114 | 449 | 21:45 22:00 | | | 23 12 | 85 | <u>55</u> 55 | 207 | 78 67 | 292 |
| 10:00 | | 71 | | 53 51 | | 122 | | 22:15 | | | 12 | | 43 | | 55 | |
| 10:30 | | 67 | | 56 | | 123 | | 22:30 | | | 18 | | 43 | | 61 | |
| 10:45 | | | 277 | 53 | 213 | 131 101 | 490 | 22:45 23:00 | | | 12 11 | 54 | 45 | 186 | 57 55 | 240 |
| 11:00 11:15 | | 55 55 | | 46 57 | | 1112 | | 23:00 | | | 8 | | 44 39 | | 55 47 | |
| 11:30 | | 77 | | 60 | | 137 | | 23:30 | | | 9 | | 33 | | 42 | |
| 11:45 | | 66 | 253 | 62 | 225 | 128 | 478 | 23:45 | | | 11 | 39 | 29 | 145 | 40 | 184 |
| TOTALS | | | 1955 | | 1423 | | 3378 | TOTALS | | | | 2542 | | 3085 | | 5627 |
| SPLIT % | | | 57.9% | | 42.1% | | 37.5% | SPLIT % | | | | 45.2% | | 54.8% | | 62.5% |
| | | | | NB | | SB | | EB | \/ | /B | | | | | To | otal |
| | DAILY TOTALS | | | 0 | | 0 | | 4,497 | | 508 | | | | | | 005 |
| AM Peak Hour | | | 07:30 | | 07:15 | | 07:15 | PM Peak Hour | | | | 15:00 | | 17:30 | | 14:45 |
| AM Pk Volume | | | 381 | | 271 | | 634 | PM Pk Volume | | | | 405 | | 350 | | 706 |
| Pk Hr Factor | | | 0.828 | | 0.721 | | 0.817 | Pk Hr Factor | | | | 0.767 | | 0.941 | | 0.840 |
| 7 - 9 Volume | 0 | 0 | 692 | | 452 | | 1144 | 4 - 6 Volume | C |) | 0 | 597 | | 652 | | 1249 |
| 7 - 9 Peak Hour | | | 07:30 | | 07:15 | | | 4 - 6 Peak Hour | | | | 17:00 | | 17:00 | | 17:00 |
| 7 - 9 Pk Volume Pk Hr Factor | | | 381 0.828 | | 271 0.721 | | 634 0.817 | 4 - 6 Pk Volume Pk Hr Factor | | | | 316 0.898 | | 340 0.914 | | 656 0.906 |
| TRITITACIO | 0.000 | | 0.020 | | 0.721 | | 0.017 | TRTII TACIOI | 0.0 | | 0.000 | 0.070 | | 0.714 | | 0.700 |

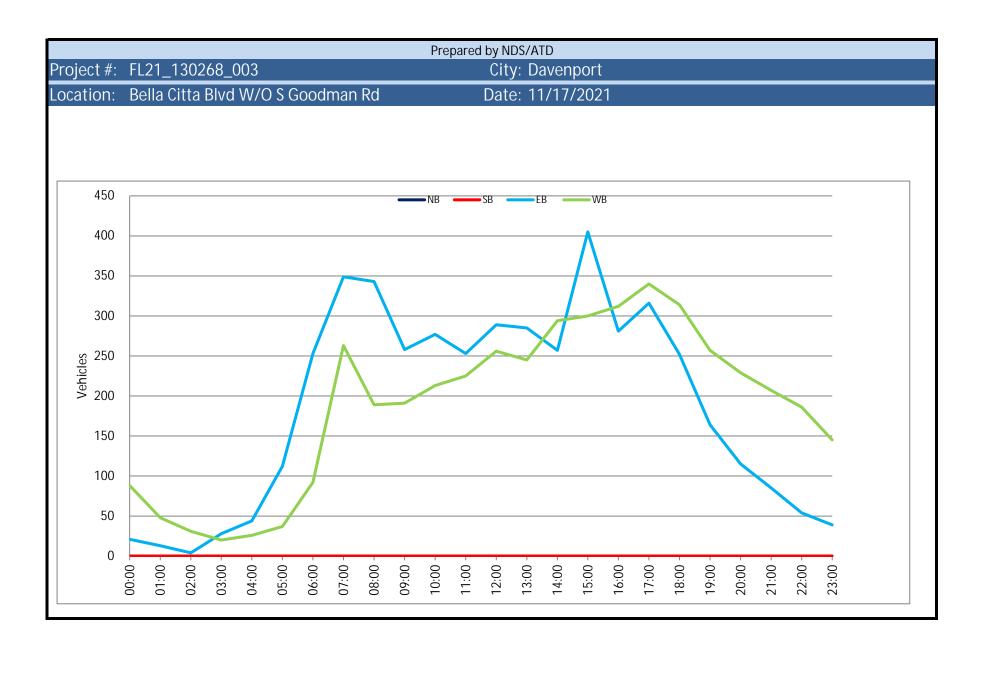
VOLUME

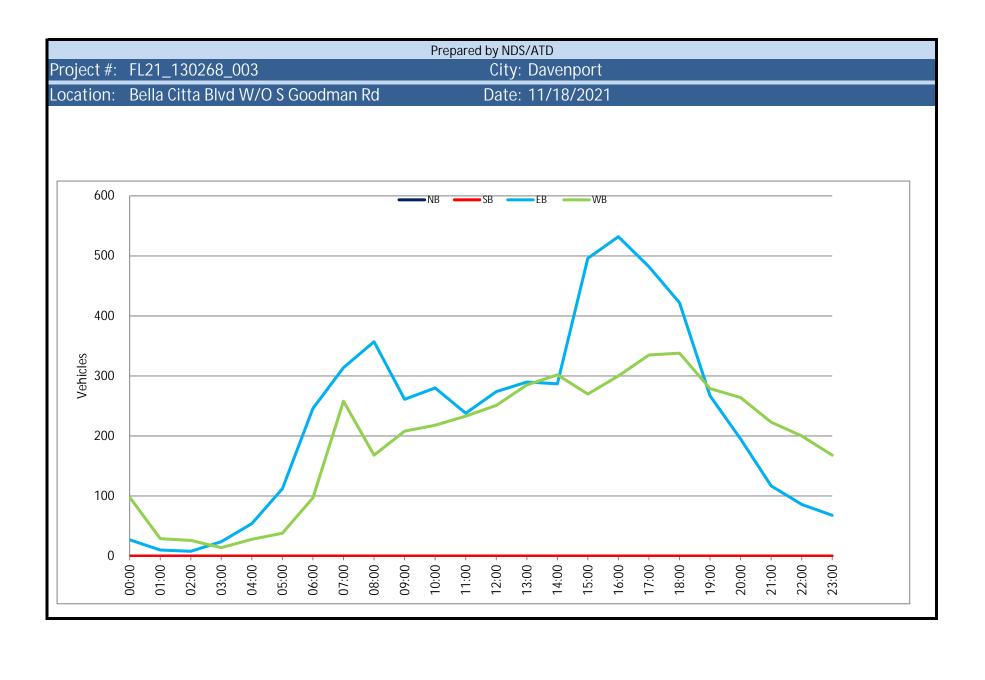
Bella Citta Blvd W/O S Goodman Rd

Day: Thursday Date: 11/18/2021

| | DAILY TOTALS | | | NB | | SB | | EB | \ | WB | | | | | | Tc | otal |
|------------------------------------|--------------|------------|--------------|-----------------|--------------|------------|--------------|------------------------------------|----|------|-------|------------|--------------|-----------|--------------|------------|--------------|
| | DAILT TOTALS | | | 0 | | 0 | | 5,447 | 4 | ,630 | | | | | | 10, | 077 |
| AM Period | NB SB | EB | | WB | | TO | TAL | PM Period | NB | S | В | EB | | WB | | TO | TAL |
| 00:00 | | 6 10 | | 34 25 | | 40 | | 12:00 | | | | 57 70 | | 72 | | 129 | |
| 00:15 00:30 | | 10 7 | | 25 18 | | 35 25 | | 12:15 12:30 | | | | 79 69 | | 55 57 | | 134 126 | |
| 00:45 | | 4 | 27 | 21 | 98 | 25 | 125 | 12:45 | | | | 69 | 274 | 67 | 251 | 136 | 525 |
| 01:00 01:15 | | 4 | | 6 9 | | 10 12 | | 13:00 13:15 | | | | 73 80 | | 62 86 | | 135 166 | |
| 01:13 | | 3 1 | | 3 | | 4 | | 13:30 | | | | 71 | | 70 | | 141 | |
| 01:45 | | 2 | 10 | 11 | 29 | 13 | 39 | 13:45 | | | | 66 | 290 | 67 | 285 | 133 | 575 |
| 02:00 02:15 | | 3 | | / 6 | | 10 8 | | 14:00 14:15 | | | | 76 71 | | 70 83 | | 146 154 | |
| 02:30 | | 2 | | 7 | | 9 | | 14:30 | | | | 62 | | 69 | | 131 | |
| 02:45 | | 1 | 8 | 6 | 26 | 7 | 34 | 14:45 | | | | 78 | 287 | 80 | 302 | 158 | 589 |
| 03:00 03:15 | | 4 6 | | 5 4 | | 9 10 | | 15:00 15:15 | | | | 125 125 | | 74 61 | | 199 186 | |
| 03:30 | | 7 | | 2 | | 9 | | 15:30 | | | | 113 | | 74 | | 187 | |
| 03:45 | | 7 9 | 24 | 3 | 14 | 10 12 | 38 | 15:45 16:00 | | | | 133 | 496 | 61 71 | 270 | 194 | 766 |
| 04:00 04:15 | | 9 14 | | 3 6 | | 20 | | 16:15 | | | | 135 143 | | 7 i 51 | | 206 194 | |
| 04:30 | | 19 | | 4 | | 23 | | 16:30 | | | | 129 | | 84 | | 213 | |
| 04:45 05:00 | | 12 23 | 54 | 15 6 | 28 | 27 29 | 82 | 16:45 17:00 | | | | 125 111 | 532 | 94 75 | 300 | 219 186 | 832 |
| 05.00 05:15 | | 23 22 | | 9 | | 31 | | 17:00 | | | | 124 | | 75 84 | | 208 | |
| 05:30 | | 34 | 440 | 11 | 0.0 | 45 | 450 | 17:30 | | | | 126 | 400 | 81 | 005 | 207 | 047 |
| 05:45 06:00 | | 33 48 | 112 | 12 13 | 38 | 45 61 | 150 | 17:45 18:00 | | | | 121 128 | 482 | 95 91 | 335 | 216 219 | 817 |
| 06:15 | | 63 | | 24 | | 87 | | 18:15 | | | | 119 | | 87 | | 206 | |
| 06:30 | | 63 | 247 | 26 | 07 | 89 | 2.42 | 18:30 | | | | 82 | 400 | 80 | 220 | 162 | 7/0 |
| 06:45 07:00 | | 72 53 | 246 | 34 52 | 97 | 106 105 | 343 | 18:45 19:00 | | | | 93 76 | 422 | 80 66 | 338 | 173 142 | 760 |
| 07:15 | | 64 | | 75 | | 139 | | 19:15 | | | | 86 | | 74 | | 160 | |
| 07:30 | | 90 107 | 214 | 79 52 | 250 | 169 | E72 | 19:30 | | | | 53 52 | 247 | 74 45 | 270 | 127 | E 14 |
| 07:45 08:00 | | 107 105 | 314 | 52 47 | 258 | 159 152 | 572 | 19:45 20:00 | | | | 42 | 267 | 65 67 | 279 | 117 109 | 546 |
| 08:15 | | 85 | | 41 | | 126 | | 20:15 | | | | 49 | | 71 | | 120 | |
| 08:30 08:45 | | 98 69 | 357 | 42 38 | 168 | 140 107 | 525 | 20:30 20:45 | | | | 58 46 | 195 | 62 64 | 264 | 120 110 | 459 |
| 09:00 | | 63 | 337 | <u>50</u> 51 | 100 | 114 | 323 | 21:00 | | | | 32 | 195 | 63 | 204 | 95 | 409 |
| 09:15 | | 57 | | 47 | | 104 | | 21:15 | | | | 26 | | 49 | | 75 | |
| 09:30 09:45 | | 61 80 | 261 | 56 54 | 208 | 117 134 | 469 | 21:30 21:45 | | | | 30 29 | 117 | 52 59 | 223 | 82 88 | 340 |
| 10:00 | | 71 | 201 | 58 | 200 | 129 | 407 | 22:00 | | | | 23 | 117 | 51 | 223 | 74 | 340 |
| 10:15 | | 62 | | 55 | | 117 | | 22:15 | | | | 19 | | 57 | | 76 | |
| 10:30 10:45 | | 76 71 | 280 | 50 55 | 218 | 126 126 | 498 | 22:30 22:45 | | | | 21 23 | 86 | 48 44 | 200 | 69 67 | 286 |
| 11:00 | | 66 | 200 | 61 | 210 | 127 | 170 | 23:00 | | | | 16 | | 57 | 200 | 73 | 200 |
| 11:15 | | 65 | | 63 44 | | 128 | | 23:15 | | | | 24 | | 48 25 | | 72 55 | |
| 11:30 11:45 | | 57 50 | 238 | 46 63 | 233 | 103 113 | 471 | 23:30 23:45 | | | | 20 8 | 68 | 35 28 | 168 | 55 36 | 236 |
| TOTALS | | <u> </u> | 1931 | <u> </u> | 1415 | . 10 | 3346 | TOTALS | | | | | 3516 | | 3215 | 33 | 6731 |
| | | | | | | | | | | | | | | | | | |
| SPLIT % | | | 57.7% | | 42.3% | | 33.2% | SPLIT % | | | | | 52.2% | | 47.8% | | 66.8% |
| | DAILY TOTALS | | | NB | | SB | | EB | ١ | WB | | | | | | To | otal |
| | DAILT TOTALS | | | 0 | | 0 | | 5,447 | 4 | ,630 | | | | | | 10, | 077 |
| AM Peak Hour | | | 07:45 | | 07:00 | | 07:15 | PM Peak Hour | | | | | 15:45 | | 17:30 | | 17:15 |
| AM Pk Volume | | | 395 | | 258 | | 619 | PM Pk Volume | | | | | 540 | | 354 | | 850 |
| Pk Hr Factor | | | 0.923 | | 0.816 | | 0.916 | Pk Hr Factor | | | | | 0.944 | | 0.932 | | 0.970 |
| 7 - 9 Volume | 0 0 | | 671 | | 426 | | 1097 | 4 - 6 Volume | | 0 | 0 | | 1014 | | 635 | | 1649 |
| 7 - 9 Peak Hour 7 - 9 Pk Volume | | | 07:45 395 | | 07:00 258 | | 07:15 619 | 4 - 6 Peak Hour 4 - 6 Pk Volume | | | | | 16:00 532 | | 16:30 337 | | 16:00 832 |
| Pk Hr Factor | | | 0.923 | | 258 0.816 | | 0.916 | Pk Hr Factor | | | | | 0.930 | | 0.896 | | 0.950 |
| | 0.000 | | 3.720 | | 3,310 | | 3.710 | | | | 5,000 | | 3,700 | | 3.370 | | 3.700 |







VOLUME

S Goodman Rd N/O Bella Citta Blvd

Day: Tuesday Date: 11/16/2021

| | D | AILY T | \cap T \triangle | ALS. | | NB | | SB | EB | | WB | | | | | | | otal |
|------------------------------|--------------|--------------|----------------------|--------------|-------|-------|-------|--------------|------------------------------|----------|-------|--------------|--------------|------|----|-------|------------|---------------|
| | <i>ا</i> ر ک | / | 017 | (LO | | 1,831 | | 2,693 | 0 | | 0 | | | | | | 4, | 524 |
| AM Period | NB | | SB | | EB | WB | | TOTAL | PM Period | NB | | SB | E | В | WE | 3 | | TAL |
| 00:00 00:15 | 6 3 | | / 8 | | | | | 13 11 | 12:00 12:15 | 23 29 | | 32 23 | | | | | 55 52 | |
| 00:30 00:45 | 6 1 | 16 | 1 | 22 | | | | 7 7 38 | 12:30 12:45 | 26 28 | 106 | 21 28 | 104 | | | | 47 56 | 210 |
| 01:00 | 0 | 10 | 0 | | | | | 0 | 13:00 | 24 | 100 | 25 | 104 | | | | 49 | 210 |
| 01:15 01:30 | 5 2 | | 0 1 | | | | | 5 3 | 13:15 13:30 | 28 26 | | 30 33 | | | | | 58 59 | |
| 01:45 | 0 | 7 | 2 | 3 | | | | 2 10 | 13:45 | 25 | 103 | 29 | 117 | | | | 54 | 220 |
| 02:00 02:15 | 2 1 | | 2 2 | | | | | 4 3 | 14:00 14:15 | 18 26 | | 35 31 | | | | | 53 57 | |
| 02:30 02:45 | 1 | 4 | 3 | 8 | | | | 4 3 14 | 14:30 14:45 | 37 27 | 108 | 44 | 1.40 | | | | 81 | 257 |
| 03:00 | 2 | 6 | 1 | 0 | | | | 3 | 15:00 | 48 | 100 | 46 | 149 | | | | 66 94 | 257 |
| 03:15 03:30 | 2 0 | | 4 0 | | | | | 6 0 | 15:15 15:30 | 29 43 | | 51 39 | | | | | 80 82 | |
| 03:45 | 0 | 4 | 1 | 6 | | | | 1 10 | 15:45 | 33 | 153 | 60 | 196 | | | | 93 | 349 |
| 04:00 04:15 | 1 0 | | 1 2 | | | | | 2 | 16:00 16:15 | 36 48 | | 62 54 | | | | | 98 102 | |
| 04:30 | 2 | 7 | 1 | , | | | | 3 | 16:30 | 22 | 120 | 80 | O O 4 | | | | 102 | 470 |
| 04:45 05:00 | 2 | / | 2 | 6 | | | | 6 13 4 | 16:45 17:00 | 33 32 | 139 | 138 : 137 | 334 | | | | 171 169 | 473 |
| 05:15 05:30 | 2 9 | | 5 1 | | | | | 7 10 | 17:15 17:30 | 27 27 | | 109 94 | | | | | 136 121 | |
| 05:45 | 11 | 24 | 4 | 12 | | | | 15 36 | 17:45 | 35 | 121 | 119 | 459 | | | | 154 | 580 |
| 06:00 06:15 | 15 18 | | 4 10 | | | | | 19 28 | 18:00 18:15 | 25 26 | | 119 101 | | | | | 144 127 | |
| 06:30 | 20 | 70 | 18 | 4.7 | | | | 38 | 18:30 | 25 | 0.0 | 87 | 000 | | | | 112 | 407 |
| 06:45 07:00 | 25 25 | 78 | 14 14 | 46 | | | | 39 124 39 | 18:45 19:00 | 22 8 | 98 | 81 : 72 | 388 | | | | 103 80 | 486 |
| 07:15 | 25 | | 25 | | | | | 50 | 19:15 | 10 | | 33 | | | | | 43 | |
| 07:30 07:45 | 43 61 | 154 | 31 28 | 98 | | | | 74 89 252 | 19:30 19:45 | 12 7 | 37 | | 173 | | | | 52 35 | 210 |
| 08:00 08:15 | 38 44 | | 23 11 | | | | | 61 55 | 20:00 20:15 | 19 13 | | 23 19 | | | | | 42 32 | |
| 08:30 | 62 | | 17 | | | | | 79 | 20:30 | 14 | | 10 | | | | | 24 | |
| 08:45 09:00 | 58 62 | 202 | 14 23 | 65 | | | | 72 267 85 | 20:45 21:00 | 3 8 | 49 | 16 6 | 68 | | | | 19 14 | 117 |
| 09:15 | 26 | | 36 | | | | | 62 | 21:15 | 9 | | 15 | | | | | 24 | |
| 09:30 09:45 | 34 25 | 147 | 48 25 | 132 | | | | 82 50 279 | 21:30 21:45 | 11 9 | 37 | 8 9 | 38 | | | | 19 18 | 75 |
| 10:00 | 31 | | 25 | | | | | 56 | 22:00 | 8 | | 13 | | | | | 21 | |
| 10:15 10:30 | 21 20 | | 25 27 | | | | | 46 47 | 22:15 22:30 | 5 9 | | 8 17 | | | | | 13 26 | |
| 10:45 11:00 | 22 26 | 94 | 24 18 | 101 | | | | 46 195 44 | 22:45 23:00 | 9 5 | 31 | 9 11 | 47 | | | | 18 16 | 78 |
| 11:15 | 22 | | 31 | | | | | 53 | 23:15 | 4 | | 5 | | | | | 9 | |
| 11:30 11:45 | 23 20 | 91 | 26 21 | 96 | | | | 49 41 187 | 23:30 23:45 | 7 3 | 19 | 5 4 | 25 | | | | 12 7 | 44 |
| TOTALS | | 830 | | 595 | | | | 1425 | TOTALS | | 1001 | | 2098 | | | | | 3099 |
| SPLIT % | | 58.2% | | 41.8% | | | | 31.5% | SPLIT % | | 32.3% | | 7.7% | | | | | 68.5% |
| | | | | | | NB | | SB | EB | | WB | | | | | | Ια | otal |
| | D | AILY T | OTA | NLS | | 1,831 | | 2,693 | 0 | | 0 | | | | | | | 524 |
| AM Peak Hour | | 08:15 | | 09:15 | | | | 08:45 | PM Peak Hour | | 15:30 | | 16:45 | | | | | 16:45 |
| AM Pk Volume | | 226 | | 134 | | | | 301 | PM Pk Volume | | 160 | | 478 | | | | | 597 |
| Pk Hr Factor 7 - 9 Volume | | 0.911 356 | | 0.698 163 | 0 | | 0 | 0.885 519 | Pk Hr Factor 4 - 6 Volume | | 0.833 | | 0.866 793 | 0 | | 0 | | 0.873 1053 |
| 7 - 9 Peak Hour | | 07:45 | | 07:15 | | | | | 4 - 6 Peak Hour | | 16:00 | | 16:45 | | | | | 16:45 |
| 7 - 9 Pk Volume | | 205 | | 107 | | | | 284 | 4 - 6 Pk Volume | | 139 | | 478 | | | | | 597 |
| Pk Hr Factor | | 0.827 | | 0.863 | 0.000 | | 0.000 | 0.798 | Pk Hr Factor | | 0.724 | | 0.866 | 0.00 | | 0.000 | | 0.873 |

VOLUME

S Goodman Rd N/O Bella Citta Blvd

Day: Wednesday Date: 11/17/2021

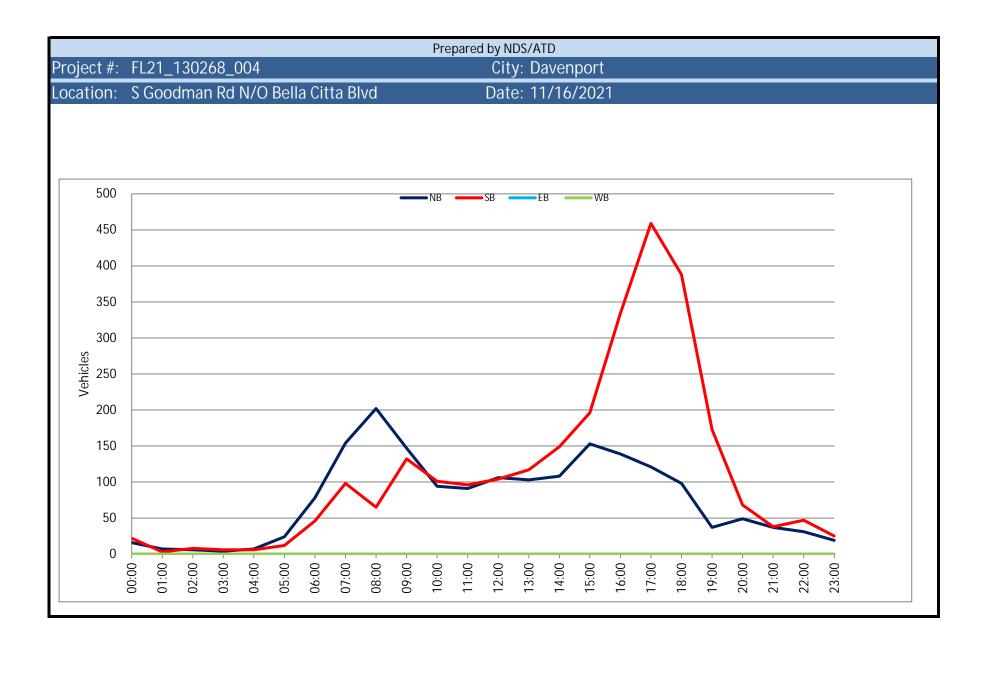
| DAILY TOTALS AM Period NB SB EB WB TOTAL PM Period NB SB EB WB 00:00 6 7 13 12:00 18 19 00:15 2 3 5 12:15 22 20 00:30 3 1 4 12:30 26 22 00:45 1 12 1 12 2 24 12:45 19 85 29 90 01:00 1 3 4 13:00 32 20 01:15 3 0 3 13:15 15 34 01:30 1 1 2 13:30 35 32 01:45 0 5 1 5 1 10 13:45 25 107 26 112 | 4,308 TOTAL 37 42 48 48 175 52 49 67 |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------|
| 00:00 6 7 00:15 2 3 00:30 3 1 00:45 1 12 12:00 18 19 12:15 22 20 12:30 26 22 12:45 19 85 29 90 13:00 3 13:00 32 20 13:00 3 13:15 15 34 13:00 1 1 1 1 1 | 37 42 48 48 175 52 49 |
| 00:15 2 3 00:30 3 1 00:45 1 12 1 2 24 2 24 12:45 19 85 29 90 01:00 1 3 4 13:00 32 20 01:15 3 0 3 13:15 15 34 01:30 1 1 2 13:30 35 32 | 42 48 48 175 52 49 |
| 00:30 3 1 00:45 1 12 1 12 01:00 1 3 3 01:15 3 01:30 1 1 1 2 13:30 3 13:30 35 32 | 48 48 175 52 49 |
| 01:00 1 3 01:15 3 0 01:30 1 1 1 2 13:30 35 34 35 35 36 32 37 34 31:30 35 32 32 | 52 49 |
| 01:15 3 13:15 15 34 01:30 1 1 2 13:30 35 32 | 49 |
| 01:30 | |
| 01:45 0 5 1 5 | |
| | 51 219 59 |
| 02:00 2 0 02:15 1 02:00 2 1 14:00 30 29 1 14:15 27 39 | 66 |
| 02:30 0 3 14:30 26 37 | 63 |
| 02:45 0 3 2 5 2 8 14:45 40 123 38 143 03:00 0 1 1 15:00 44 37 | 78 266 81 |
| 03:15 2 0 15:15 30 53 | 83 |
| 03:30 | 84 |
| 03:45 1 3 1 3 1 3 141 83 221 04:00 0 3 3 16:00 23 72 | 114 362 95 |
| 04:15 2 0 2 16:15 33 58 | 91 |
| 04:30 1 1 04:45 2 5 2 4 10:30 30 73 4 11 16:45 39 125 99 302 | 103 |
| 04:45 2 5 2 6 05:00 2 3 4 11 16:45 39 125 99 302 5 17:00 26 114 | 138 427 140 |
| 05:15 1 1 2 17:15 30 102 | 132 |
| 05:30 8 3 05:45 13 24 5 12 11 17:30 25 112 18 36 17:45 32 113 130 458 | 137 162 571 |
| 05:43 13 24 3 12 06:00 14 5 19 18:00 17 78 | 95 |
| 06:15 25 11 36 18:15 18 75 | 93 |
| 06:30 22 15 06:45 26 87 15 46 41 133 18:30 23 90 41 133 18:45 9 67 58 301 | 113 67 368 |
| 07:00 34 16 50 19:00 14 45 | 59 |
| 07:15 30 28 58 19:15 15 31 10:20 15 31 | 46 |
| 07:30 61 33 07:45 51 176 25 102 94 19:30 15 26 76 278 19:45 11 55 18 120 | 41 29 175 |
| 08:00 32 16 48 20:00 16 22 | 38 |
| 08:15 39 22 08:30 49 18 61 20:15 67 20:30 17 19 | 40 36 |
| 08:45 | 29 143 |
| 09:00 37 18 55 21:00 14 9 | 23 |
| 09:15 28 33 09:30 24 28 61 21:15 13 7 52 21:30 13 9 | 20 22 |
| 09:45 20 109 20 99 40 208 21:45 8 48 9 34 | 17 82 |
| 10:00 24 23 47 22:00 9 9 10:15 27 27 27 27 29:15 16 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29:15 29 | 18 |
| 10:15 27 27 10:30 31 16 54 22:15 16 47 22:30 3 5 5 | 28 8 |
| 10:45 30 112 25 91 55 203 22:45 8 36 10 36 | 18 72 |
| 11:00 19 22 11:15 34 29 41 23:00 7 20 63 23:15 8 19 | 27 27 |
| 11:30 | 19 |
| 11:45 21 98 26 105 47 203 23:45 3 28 11 59 | 14 87 |
| TOTALS 806 555 1361 TOTALS 999 1948 | 2947 |
| SPLIT % 59.2% 40.8% 31.6% SPLIT % 33.9% 66.1% | 68.4% |
| DAILY TOTALS NB SB EB WB 1 005 0 500 | Total |
| DAILY TOTALS 1,805 2,503 0 0 | 4,308 |
| AM Peak Hour 07:30 11:00 07:30 PM Peak Hour 14:45 17:00 | 17:00 |
| AM Pk Volume 183 105 279 PM Pk Volume 150 458 | 571 |
| Pk Hr Factor 0.750 0.905 0.742 Pk Hr Factor 0.852 0.881 | 0.881 |
| 7 - 9 Volume 348 171 0 0 519 4 - 6 Volume 238 760 0 0 7 - 9 Peak Hour 07:30 07:30 07:30 4 - 6 Peak Hour 16:15 17:00 | 998 17:00 |
| 7 - 9 Peak Hour 07:30 07:00 07:30 4 - 6 Peak Hour 16:15 17:00 7 - 9 Pk Volume 183 102 0 279 4 - 6 Pk Volume 128 458 0 0 | 571 |
| Pk Hr Factor 0.750 0.773 0.000 0.000 0.742 Pk Hr Factor 0.821 0.881 0.000 0.000 | |

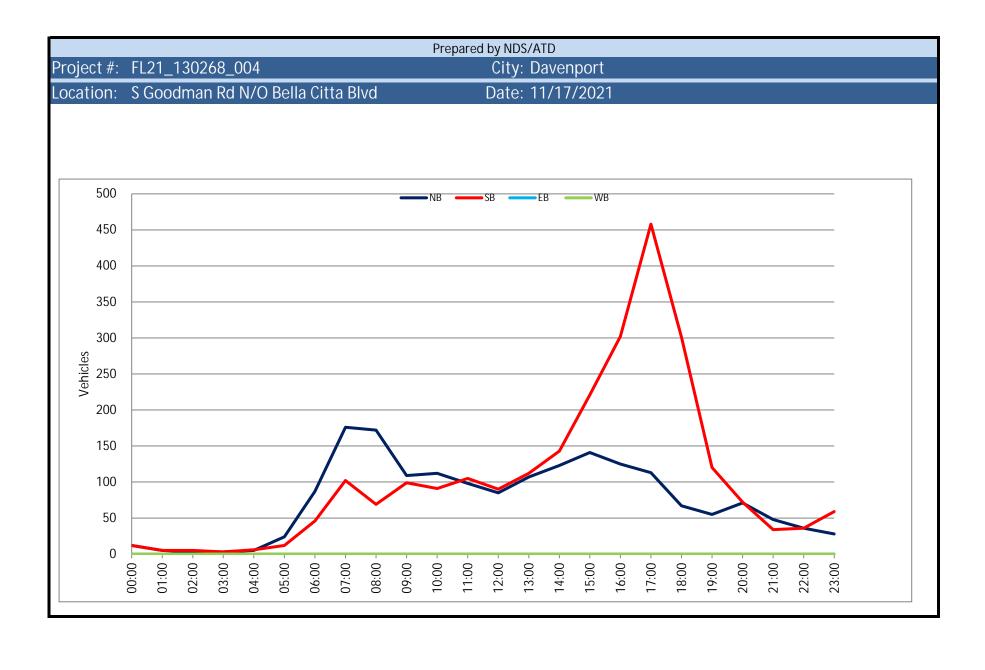
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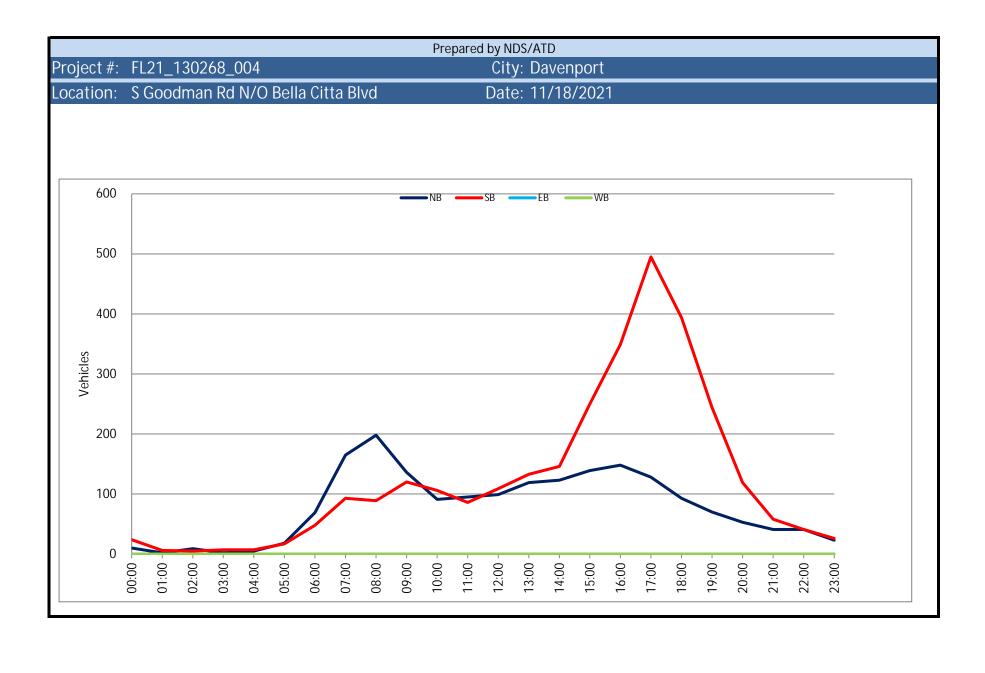
S Goodman Rd N/O Bella Citta Blvd

Day: Thursday Date: 11/18/2021

| | DA | AILY T | ΓΩΤΔ | 15 | | NB | | SB | | EB | | WB | | | | | | | To | tal |
|------------------------------|----------|--------------|----------|--------------|------|-------|-------|-------------------|--------------|------------------------------|----------|----------------------------------------|------------|--------------|----|-------|----|-------|------------|---------------|
| | Ur | AILI I | | ILJ | | 1,877 | | 2,972 | | 0 | | 0 | | | | | | | 4,8 | 349 |
| AM Period | NB | | SB | | EB | WB | | TO | TAL | PM Period | NB | | SB | | EB | | WB | | TO | TAL |
| 00:00 00:15 | 3 3 | | 5 9 | | | | | 8 12 | | 12:00 12:15 | 25 30 | | 31 20 | | | | | | 56 50 | |
| 00:15 | 3 | | 4 | | | | | 7 | | 12.15 | 23 | | 20 26 | | | | | | 49 | |
| 00:45 | 1 | 10 | 6 | 24 | | | | 7 | 34 | 12:45 | 21 | 99 | 32 | 109 | | | | | 53 | 208 |
| 01:00 | 1 | | 1 | | | | | 2 | | 13:00 13:15 | 37 | | 36 | | | | | | 73 | |
| 01:15 01:30 | 0 0 | | 3 1 | | | | | 3 1 | | 13:15 | 32 26 | | 35 31 | | | | | | 67 57 | |
| 01:45 | 1 | 2 | <u> </u> | 6 | | | | 2 | 8 | 13:45 | 24 | 119 | 31 | 133 | | | | | 55 | 252 |
| 02:00 | 0 | | 0 | | | | | 0 | | 14:00 | 32 | | 26 | | | | | | 58 | |
| 02:15 02:30 | 2 2 | | 1 1 | | | | | 3 | | 14:15 14:30 | 25 28 | | 34 43 | | | | | | 59 71 | |
| 02:45 | 5 | 9 | 3 | 5 | | | | 8 | 14 | 14:45 | 38 | 123 | 43 | 146 | | | | | 81 | 269 |
| 03:00 | 0 | | 1 | | | | | 1 | | 15:00 | 47 | | 43 | | | | | | 90 | |
| 03:15 03:30 | 2 0 | | 2 1 | | | | | 1 | | 15:15 15:30 | 28 34 | | 66 79 | | | | | | 94 113 | |
| 03:45 | 0 | 2 | 3 | 7 | | | | 3 | 9 | 15:45 | 30 | 139 | 62 | 250 | | | | | 92 | 389 |
| 04:00 | 1 | | 2 | | | | | 3 | | 16:00 | 29 | | 77 | | | | | | 106 | |
| 04:15 04:30 | 1 | | 1 1 | | | | | 2 | | 16:15 16:30 | 37 38 | | 72 81 | | | | | | 109 119 | |
| 04:45 | 2 | 5 | 3 | 7 | | | | 5 | 12 | 16:45 | 44 | 148 | 119 | 349 | | | | | 163 | 497 |
| 05:00 | 1 | | 3 | | | | | 4 | | 17:00 | 29 | | 135 | | | | | | 164 | |
| 05:15 05:30 | 3 1 | | 3 1 | | | | | 6 5 | | 17:15 17:30 | 46 32 | | 130 107 | | | | | | 176 139 | |
| 05:45 | 13 | 18 | 7 | 17 | | | | 20 | 35 | 17:45 | 21 | 128 | 123 | 495 | | | | | 144 | 623 |
| 06:00 | 12 | | 6 | | | | | 18 | | 18:00 | 18 | | 111 | | | | | | 129 | |
| 06:15 06:30 | 19 14 | | 9 15 | | | | | 28 29 | | 18:15 18:30 | 27 18 | | 118 94 | | | | | | 145 112 | |
| 06:45 | 24 | 69 | 18 | 48 | | | | 42 | 117 | 18:45 | 30 | 93 | 71 | 394 | | | | | 101 | 487 |
| 07:00 | 32 | | 18 | | | | | 50 | | 19:00 | 13 | | 78 | | | | | | 91 | |
| 07:15 07:30 | 32 45 | | 20 30 | | | | | 52 75 | | 19:15 19:30 | 24 20 | | 78 48 | | | | | | 102 68 | |
| 07:45 | 56 | 165 | 25 | 93 | | | | 81 | 258 | 19:45 | 13 | 70 | 40 | 244 | | | | | 53 | 314 |
| 08:00 | 38 | | 25 | | | | | 63 | | 20:00 | 10 | | 41 | | | | | | 51 | |
| 08:15 08:30 | 44 62 | | 19 21 | | | | | 63 83 | | 20:15 20:30 | 16 12 | | 36 20 | | | | | | 52 32 | |
| 08:45 | 54 | 198 | 24 | 89 | | | | 78 | 287 | 20:45 | 15 | 53 | 22 | 119 | | | | | 37 | 172 |
| 09:00 | 56 | | 22 | | | | | 78 | | 21:00 | 13 | | 12 | | | | | | 25 | |
| 09:15 09:30 | 26 24 | | 39 33 | | | | | 65 57 | | 21:15 21:30 | 8 11 | | 14 14 | | | | | | 22 25 | |
| 09.30 | 30 | 136 | 33 26 | 120 | | | | 56 | 256 | 21:45 | 9 | 41 | 18 | 58 | | | | | 23 27 | 99 |
| 10:00 | 26 | <u> </u> | 22 | | | | | 48 | | 22:00 | 5 | | 14 | | | | | | 19 | |
| 10:15 10:30 | 24 21 | | 32 30 | | | | | 56 51 | | 22:15 22:30 | 13 15 | | 10 7 | | | | | | 23 22 | |
| 10:30 | 20 | 91 | 30 22 | 106 | | | | 42 | 197 | 22:30 | 8 | 41 | , 10 | 41 | | | | | 22 18 | 82 |
| 11:00 | 29 | | 18 | | | | | 47 | | 23:00 | 8 | | 5 | | | | | | 13 | |
| 11:15 11:30 | 30 9 | | 23 23 | | | | | 53 32 | | 23:15 23:30 | 7 2 | | 15 3 | | | | | | 22 5 | |
| 11:30 | 9 27 | 95 | 23 22 | 86 | | | | 32 49 | 181 | 23:45 | 6 | 23 | ა 3 | 26 | | | | | 5 9 | 49 |
| TOTALS | | 800 | _ | 608 | | | | | 1408 | TOTALS | | 1077 | | 2364 | | | | | | 3441 |
| SPLIT % | | 56.8% | | 43.2% | | | | | 29.0% | SPLIT % | | 31.3% | | 68.7% | | | | | | 71.0% |
| | | | | | | NB | | SB | | EB | | WB | | | | | | | To | ital |
| | DA | AILY T | OTA | \LS | | 1,877 | | 2,972 | | 0 | | 0 | | | | | | | | 349 |
| | | | | | | 1,077 | | Z, /12 | | | | —————————————————————————————————————— | | | | | | | 4,0 | |
| AM Peak Hour | | 08:15 | | 09:00 | | | | | 08:30 | PM Peak Hour | | 16:30 | | 17:00 | | | | | | 16:45 |
| AM Pk Volume | | 216 | | 120 | | | | | 304 | PM Pk Volume | | 157 | | 495 | | | | | | 642 |
| Pk Hr Factor 7 - 9 Volume | | 0.871 363 | | 0.769 182 | 0 | | 0 | | 0.916 545 | Pk Hr Factor 4 - 6 Volume | | 0.853 276 | | 0.917 844 | | 0 | | 0 | | 0.912 1120 |
| 7 - 9 Peak Hour | | 07:45 | | 07:15 | | | | | | 4 - 6 Peak Hour | | 16:30 | | 17:00 | | | | | | 16:45 |
| 7 - 9 Pk Volume | | 200 | | 100 | | | | | | 4 - 6 Pk Volume | | 157 | | 495 | | | | | | 642 |
| Pk Hr Factor | | 0.806 | | 0.833 | 0.00 | 0 | 0.000 | | 0.873 | Pk Hr Factor | | 0.853 | | 0.917 | (| 0.000 | | 0.000 | | 0.912 |







VOLUME

S Goodman Rd S/O Bella Citta Blvd

Day: Tuesday Date: 11/16/2021

| | DAI | ILY T | OTA | I.S | | NB | | SB | | EB | | WB | | | | | | | | otal |
|---------------------------------|----------|--------------|---------------|--------------|------|-------|-------|------------|---------------|---------------------------------|-----------|--------------|------------|---------------|----|-------|----|-------|------------|---------------|
| | | | 017 | iLO | | 5,140 | | 5,975 | | 0 | | 0 | | | | | | | 11, | 115 |
| AM Period | NB | | SB | | EB | WB | | TOT | ΓAL | PM Period | NB | | SB | | EB | | WB | | | TAL |
| 00:00 00:15 | 29 38 | | 14 15 | | | | | 43 53 | | 12:00 12:15 | 66 78 | | 88 79 | | | | | | 154 157 | |
| 00:30 | 36 | | 9 | | | | | 45 | | 12:30 | 71 | | 73 | | | | | | 144 | |
| 00:45 01:00 | 30 22 | 133 | 13 5 | 51 | | | | 43 27 | 184 | 12:45 13:00 | 64 74 | 279 | 75 80 | 315 | | | | | 139 154 | 594 |
| 01:00 | 16 | | 5 | | | | | 21 | | 13:15 | 74 78 | | 73 | | | | | | 151 | |
| 01:30 | 16 | | 7 | 0.0 | | | | 23 | 0.4 | 13:30 | 82 | 04.4 | 94 | 000 | | | | | 176 | |
| 01:45 02:00 | 9 17 | 63 | <u>6</u> 4 | 23 | | | | 15 21 | 86 | 13:45 14:00 | 80 72 | 314 | 85 69 | 332 | | | | | 165 141 | 646 |
| 02:15 | 14 | | 2 | | | | | 16 | | 14:15 | 83 | | 79 | | | | | | 162 | |
| 02:30 | 9 | EO | 3 | 1.4 | | | | 12 | <i>(</i> 7 | 14:30 | 94 | 245 | 79 | 210 | | | | | 173 | 440 |
| 02:45 03:00 | 13 6 | 53 | <u>5</u> 8 | 14 | | | | 18 14 | 67 | 14:45 15:00 | 96 101 | 345 | 91 147 | 318 | | | | - | 187 248 | 663 |
| 03:15 | 6 | | 8 | | | | | 14 | | 15:15 | 80 | | 133 | | | | | | 213 | |
| 03:30 03:45 | 7 4 | 23 | 5 1 | 25 | | | | 12 8 | 48 | 15:30 15:45 | 93 88 | 362 | 111 112 | 503 | | | | | 204 200 | 865 |
| 04:00 | 4 | 23 | 12 | 23 | | | | 16 | 40 | 16:00 | 98 | 302 | 112 | 303 | | | | | 210 | 003 |
| 04:15 | 6 | | 11 | | | | | 17 | | 16:15 | 80 | | 120 | | | | | | 200 | |
| 04:30 04:45 | 8 17 | 35 | 20 17 | 60 | | | | 28 34 | 95 | 16:30 16:45 | 65 85 | 328 | 149 169 | 550 | | | | | 214 254 | 878 |
| 05:00 | 10 | 33 | 27 | 00 | | | | 37 | 75 | 17:00 | 83 | 320 | 182 | 330 | | | | | 265 | 070 |
| 05:15 | 10 | | 33 | | | | | 43 | | 17:15 | 75 70 | | 154 | | | | | | 229 | |
| 05:30 05:45 | 19 23 | 62 | 29 32 | 121 | | | | 48 55 | 183 | 17:30 17:45 | 78 87 | 323 | 143 148 | 627 | | | | | 221 235 | 950 |
| 06:00 | 26 | <u> </u> | 43 | | | | | 69 | 100 | 18:00 | 68 | 020 | 142 | <u> </u> | | | | | 210 | 700 |
| 06:15 06:30 | 28 34 | | 73 89 | | | | | 101 123 | | 18:15 18:30 | 79 56 | | 135 107 | | | | | | 214 163 | |
| 06:45 | | 147 | 89 | 294 | | | | 148 | 441 | 18:45 | 62 | 265 | 107 | 485 | | | | | 163 | 750 |
| 07:00 | 65 | | 57 | | | | | 122 | | 19:00 | 51 | | 87 | | | | | | 138 | |
| 07:15 07:30 | 80 94 | | 60 87 | | | | | 140 181 | | 19:15 19:30 | 58 64 | | 81 60 | | | | | | 139 124 | |
| 07:45 | | 320 | 127 | 331 | | | | 208 | 651 | 19:45 | 57 | 230 | 48 | 276 | | | | | 105 | 506 |
| 08:00 | 81 | | 68 | | | | | 149 | | 20:00 | 66 | | 46 | | | | | | 112 | |
| 08:15 08:30 | 70 72 | | 86 81 | | | | | 156 153 | | 20:15 20:30 | 51 60 | | 40 32 | | | | | | 91 92 | |
| 08:45 | 74 | 297 | 67 | 302 | | | | 141 | 599 | 20:45 | 46 | 223 | 35 | 153 | | | | | 81 | 376 |
| 09:00 09:15 | 85 61 | | 64 71 | | | | | 149 132 | | 21:00 21:15 | 73 54 | | 37 43 | | | | | | 110 97 | |
| 09.15 | 56 | | 95 | | | | | 151 | | 21:30 | 74 | | 23 | | | | | | 97 97 | |
| 09:45 | 46 | 248 | 72 | 302 | | | | 118 | 550 | 21:45 | 53 | 254 | 22 | 125 | | | | | 75 | 379 |
| 10:00 10:15 | 61 48 | | 67 85 | | | | | 128 133 | | 22:00 22:15 | 63 50 | | 21 22 | | | | | | 84 72 | |
| 10:30 | 65 | | 84 | | | | | 149 | | 22:30 | 38 | | 24 | | | | | | 62 | |
| 10:45 | | 240 | 81 | 317 | | | | 147 | 557 | 22:45 | 59 | 210 | 15 | 82 | | | | | 74 | 292 |
| 11:00 11:15 | 58 60 | | 63 91 | | | | | 121 151 | | 23:00 23:15 | 31 36 | | 21 17 | | | | | | 52 53 | |
| 11:30 | 65 | | 81 | | | | | 146 | | 23:30 | 46 | | 10 | | | | | | 56 | |
| 11:45 | | 239 | 77 | 312 | | | | 133 | 551 | 23:45 | 34 | 147 | 9 | 57 | | | | | 43 | 204 |
| TOTALS | 1 | 1860 | | 2152 | | | | | 4012 | TOTALS | | 3280 | | 3823 | | | | | | 7103 |
| SPLIT % | 4 | 6.4% | | 53.6% | | | | | 36.1% | SPLIT % | | 46.2% | | 53.8% | | | | | | 63.9% |
| | DΔ | ILY T | ΌΤΔ | 15 | | NB | | SB | | EB | | WB | | | | | | | | otal |
| | | | 01/ | - | | 5,140 | | 5,975 | | 0 | | 0 | | | | | | | 11, | 115 |
| AM Peak Hour | (| 07:15 | | 07:30 | | | | | 07:30 | PM Peak Hour | | 14:15 | | 16:30 | | | | | | 16:45 |
| AM Pk Volume | | 336 | | 368 | | | | | 694 | PM Pk Volume | | 374 | | 654 | | | | | | 969 |
| Pk Hr Factor | | 0.894 | | 0.724 | | | | | 0.834 | Pk Hr Factor | | 0.926 | | 0.898 | | 0 | | 0 | | 0.914 |
| 7 - 9 Volume 7 - 9 Peak Hour | | 617 07:15 | | 633 07:30 | | | | | 1250 07:30 | 4 - 6 Volume 4 - 6 Peak Hour | | 651 16:00 | | 1177 16:30 | | | | | | 1828 16:45 |
| 7 - 9 Pk Volume | | 336 | | 368 | | | | | | 4 - 6 Pk Volume | | 328 | | 654 | | | | | | 969 |
| Pk Hr Factor | | 0.894 | | 0.724 | 0.00 | 00 | 0.000 | | 0.834 | Pk Hr Factor | | 0.837 | | 0.898 | (| 0.000 | | 0.000 | | 0.914 |

VOLUME

S Goodman Rd S/O Bella Citta Blvd

Day: Wednesday Date: 11/17/2021

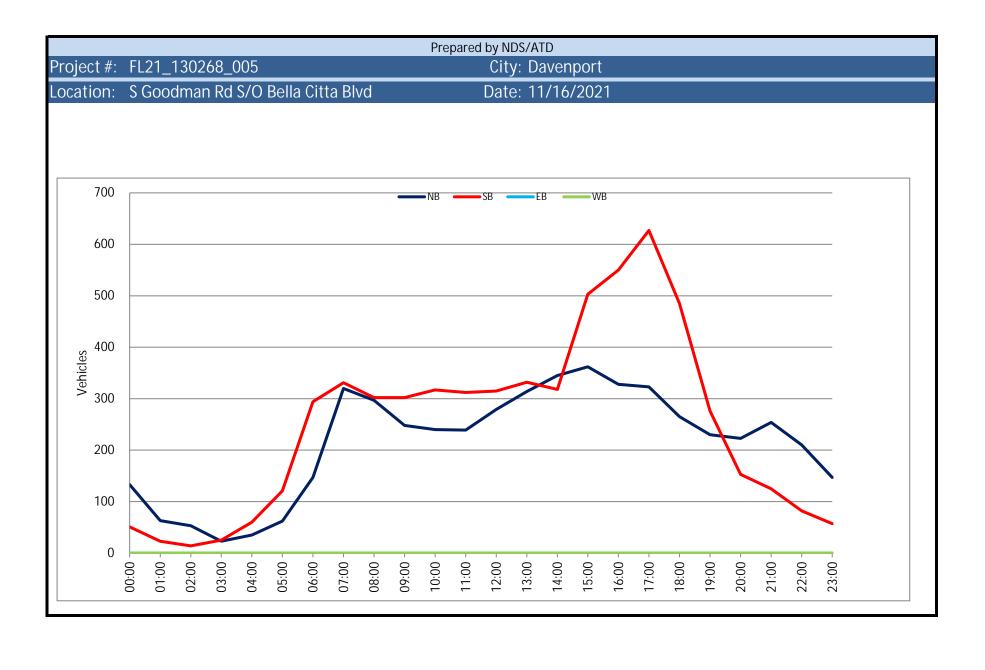
| | ח | AILY T | $\cap T \wedge$ | VI C | | NB | SB | | EB | | WB | | | | | | To | otal |
|---------------------------------|--------------|---------------|-----------------|--------------|-------|-------|------------|--------------|---------------------------------|----------|--------------|------------|--------------|------|----|-------|------------|--------------|
| | Uf | √ILI I | O1F | 1LJ | | 5,202 | 5,88 | 39 | 0 | | 0 | | | | | | 11, | ,091 |
| AM Period | NB | | SB | | EB | WB | T | OTAL | PM Period | NB | | SB | | EB | WB | | TO | TAL |
| 00:00 | 30 | | 14 | | | | 44 | | 12:00 | 73 | | 92 | | | | ! | 165 | |
| 00:15 | 25 | | 8 | | | | 33 | | 12:15 | 76 | | 68 | | | | | 144 | |
| 00:30 00:45 | 25 18 | 98 | 5 1 | 31 | | | 30 22 | 129 | 12:30 12:45 | 71 75 | 295 | 85 88 | 333 | | | | 156 163 | 628 |
| 01:00 | 15 | 70 | | 31 | | | 22 | 127 | 13:00 | 70 | 293 | | 333 | | | | 149 | 020 |
| 01:15 | 19 | | 1 | | | | 20 | | 13:15 | 66 | | 98 | | | | | 164 | |
| 01:30 | 12 | 5 0 | 6 | 4 7 | | | 18 | | 13:30 | 79 | 000 | 83 | 0.40 | | | | 162 | |
| 01:45 02:00 | 6 7 | 52 | 3 | 17 | | | 9 | 69 | 13:45 14:00 | 83 73 | 298 | 83 81 | 343 | | | | 166 154 | 641 |
| 02:00 | 10 | | 0 | | | | 10 | | 14:15 | 77 | | 84 | | | | | 161 | |
| 02:30 | 9 | | 6 | | | | 15 | | 14:30 | 76 | | 82 | | | | | 158 | |
| 02:45 | 7 | 33 | 2 | 8 | | | 9 | 41 | 14:45 | 105 | 331 | 67 | 314 | | | | 172 | 645 |
| 03:00 03:15 | 5 5 | | / 7 | | | | 12 12 | | 15:00 15:15 | 91 77 | | 138 137 | | | | | 229 214 | |
| 03:30 | 6 | | 8 | | | | 14 | | 15:30 | 94 | | 97 | | | | | 191 | |
| 03:45 | 5 | 21 | 7 | 29 | | | 12 | 50 | 15:45 | 74 | 336 | 149 | 521 | | | | 223 | 857 |
| 04:00 | 1 | | 11 | | | | 12 | | 16:00 | 91 | | 107 | | | | | 198 | |
| 04:15 04:30 | 7 4 | | 12 13 | | | | 19 17 | | 16:15 16:30 | 77 76 | | 105 125 | | | | | 182 201 | |
| 04:45 | 18 | 30 | 13 | 49 | | | 31 | 79 | 16:45 | 94 | 338 | 147 | 484 | | | | 241 | 822 |
| 05:00 | 8 | | 26 | | | | 34 | | 17:00 | 87 | | 167 | | | | | 254 | |
| 05:15 | 14 | | 36 | | | | 50 | | 17:15 | 71 | | 143 | | | | | 214 | |
| 05:30 05:45 | 15 21 | 58 | 20 39 | 121 | | | 35 60 | 179 | 17:30 17:45 | 75 83 | 316 | 151 176 | 637 | | | | 226 259 | 953 |
| 06:00 | 21 | 30 | 50 | 121 | | | 71 | 177 | 18:00 | 70 | 310 | 116 | 037 | | | | 186 | 755 |
| 06:15 | 32 | | 57 | | | | 89 | | 18:15 | 75 | | 111 | | | | | 186 | |
| 06:30 | 48 | 151 | 86 | 271 | | | 134 | | 18:30 | 69 | 277 | 130 | 4.40 | | | | 199 | 70/ |
| 06:45 07:00 | 50 61 | 151 | 78 64 | 271 | | | 128 125 | | 18:45 19:00 | 63 61 | 277 | 92 74 | 449 | | | | 155 135 | 726 |
| 07:15 | 82 | | 75 | | | | 157 | | 19:15 | 70 | | 68 | | | | | 138 | |
| 07:30 | 122 | | 100 | | | | 222 | | 19:30 | 68 | | 40 | | | | | 108 | |
| 07:45 | 71 72 | 336 | 109 83 | 348 | | | 180 155 | | 19:45 20:00 | 70 67 | 269 | 59 43 | 241 | | | | 129 110 | 510 |
| 08:00 08:15 | 64 | | os 94 | | | | 158 | | 20:00 | 68 | | 43 48 | | | | | 116 | |
| 08:30 | 77 | | 90 | | | | 167 | | 20:30 | 58 | | 37 | | | | | 95 | |
| 08:45 | 79 | 292 | 76 | 343 | | | 155 | | 20:45 | 76 | 269 | 28 | 156 | | | | 104 | 425 |
| 09:00 09:15 | 70 56 | | 72 69 | | | | 142 125 | | 21:00 21:15 | 62 64 | | 32 19 | | | | | 94 83 | |
| 09:13 | 60 | | 75 | | | | 135 | | 21:30 | 58 | | 28 | | | | | 86 | |
| 09:45 | 53 | 239 | 80 | 296 | | | 133 | 535 | 21:45 | 61 | 245 | 30 | 109 | | | | 91 | 354 |
| 10:00 | 66 | | 73 | | | | 139 | | 22:00 | 59 | | 16 | | | | | 75 | |
| 10:15 10:30 | 69 72 | | 89 68 | | | | 158 140 | | 22:15 22:30 | 55 45 | | 20 22 | | | | | 75 67 | |
| 10:45 | 66 | 273 | 86 | 316 | | | 152 | | 22:45 | 51 | 210 | 20 | 78 | | | | 71 | 288 |
| 11:00 | 59 | | 71 | | | | 130 | | 23:00 | 43 | | 23 | | | | | 66 | |
| 11:15 | 79 72 | | 72 | | | | 151 | | 23:15 | 43 | | 23 | | | | | 66 | |
| 11:30 11:45 | 72 70 | 280 | 93 79 | 315 | | | 165 149 | | 23:30 23:45 | 39 30 | 155 | 14 20 | 80 | | | | 53 50 | 235 |
| TOTALS | 7.0 | 1863 | , , | 2144 | | | 147 | 4007 | TOTALS | 30 | 3339 | | 3745 | | | | 30 | 7084 |
| | | | | | | | | | | | | | | | | | | |
| SPLIT % | | 46.5% | | 53.5% | | | | 36.1% | SPLIT % | | 47.1% | | 52.9% | | | | | 63.9% |
| | D | AILY T | $\cap T A$ | 115 | | NB | SB | | EB | | WB | | | | | | To | otal |
| | — D <i>F</i> | TIL I | -O1F | TE3 | | 5,202 | 5,88 | 39 | 0 | | 0 | | | | | | 11, | ,091 |
| AM Peak Hour | | 07:15 | | 07:30 | | | | 07:30 | PM Peak Hour | | 14:45 | | 17:00 | | | | | 17:00 |
| AM Pk Volume | | 347 | | 386 | | | | 715 | PM Pk Volume | | 367 | | 637 | | | | | 953 |
| Pk Hr Factor | | 0.711 | | 0.885 | | | | 0.805 | Pk Hr Factor | | 0.874 | | 0.905 | | | | | 0.920 |
| 7 - 9 Volume | | 628 | | 691 | | | | 1319 | 4 - 6 Volume | | 654 | | 1121 | | | | | 1775 |
| 7 - 9 Peak Hour | | 07:15 | | 07:30 | | | | | 4 - 6 Peak Hour | | 16:00 | | 17:00 | | | | | 17:00 |
| 7 - 9 Pk Volume Pk Hr Factor | | 347 0.711 | | 386 0.885 | | | | 715 0.805 | 4 - 6 Pk Volume Pk Hr Factor | | 338 0.899 | | 637 0.905 | | | | | 953 0.920 |
| I KTII TUOTOI | | 5.711 | | 3.000 | 3.000 | | | 0.000 | The factor | | 3.077 | | 3.700 | 0.00 | | 0.000 | | 0.720 |

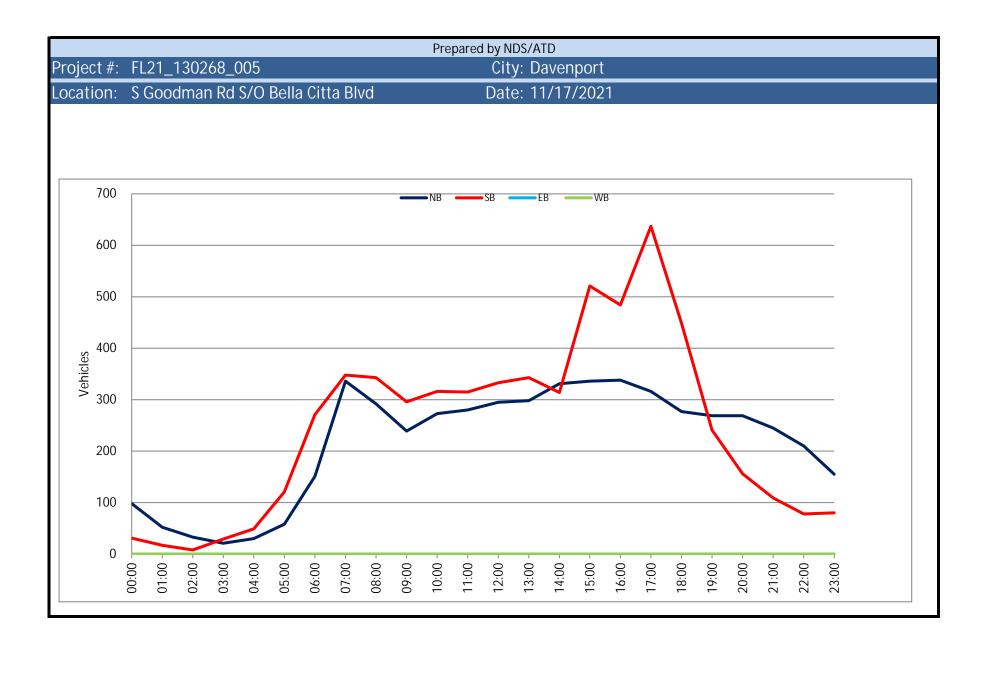
VOLUME

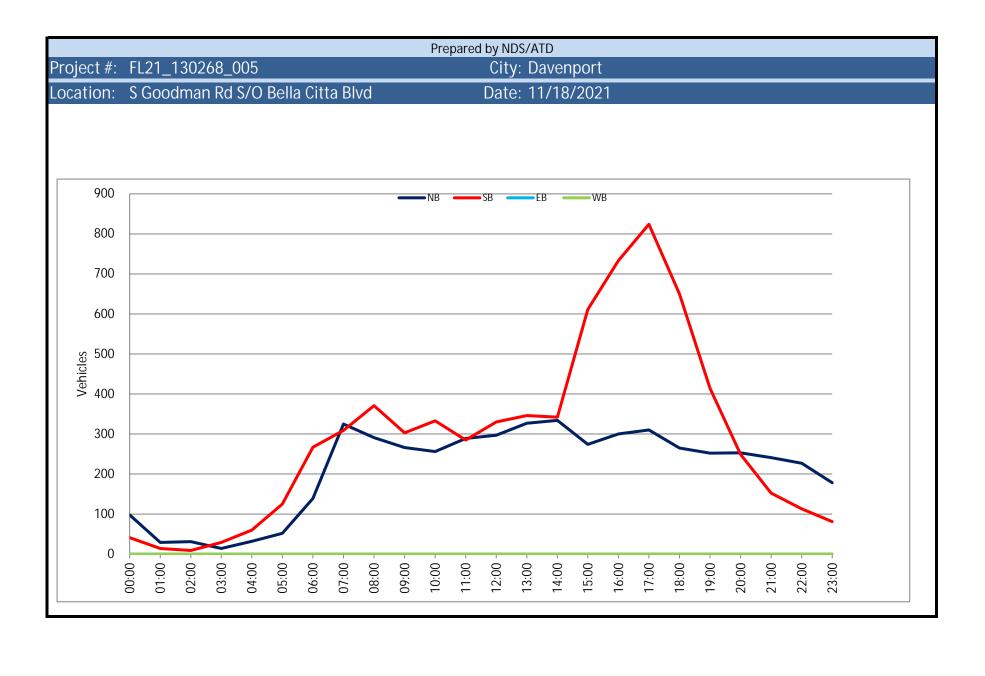
S Goodman Rd S/O Bella Citta Blvd

Day: Thursday Date: 11/18/2021

| | D | AILY 7 | ΓΩΤΔ | ALS | | NB | | SB | | EB | | WB | | | | | | | | otal |
|---------------------------|------------|-------------|--------------|--------------|-------|-------|-------|------------|--------------|------------------------------|----------|----------------|------------|---------------|----|-------|----|-------|------------|---------------|
| | υ i | | | 1LJ | | 5,080 | | 6,991 | | 0 | | 0 | | | | | | | 12, | ,071 |
| AM Period | NB | | SB | | EB | WB | | | TAL | PM Period | NB | | SB | | EB | | WB | | | TAL |
| 00:00 00:15 | 34 24 | | 8 15 | | | | | 42 39 | | 12:00 12:15 | 83 72 | | 74 86 | | | | | | 157 158 | |
| 00:30 | 20 | | 10 | | | | | 30 | | 12:30 | 67 | | 82 | | | | | | 149 | |
| 00:45 | 20 | 98 | 8 | 41 | | | | 28 10 | 139 | 12:45 13:00 | 75 80 | 297 | 88 90 | 330 | | | | | 163 170 | 627 |
| 01:00 01:15 | 6 8 | | 4 5 | | | | | 13 | | 13:15 | 93 | | 90 90 | | | | | | 183 | |
| 01:30 | 3 | 00 | 2 | 4.4 | | | | 5 | 40 | 13:30 | 81 | 007 | 87 | 0.47 | | | | | 168 | /70 |
| 01:45 02:00 | 12 7 | 29 | 3 | 14 | | | | 15 10 | 43 | 13:45 14:00 | 73 86 | 327 | 79 86 | 346 | | | | | 152 172 | 673 |
| 02:15 | 8 | | 3 | | | | | 11 | | 14:15 | 83 | | 80 | | | | | | 163 | |
| 02:30 02:45 | 8 8 | 31 | 2 1 | 9 | | | | 10 9 | 40 | 14:30 14:45 | 78 87 | 334 | 86 90 | 342 | | | | | 164 177 | 676 |
| 03:00 | 4 | <u> </u> | 4 | , | | | | 8 | 70 | 15:00 | 82 | 551 | 129 | J12 | | | | | 211 | 070 |
| 03:15 03:30 | 5 2 | | 7 8 | | | | | 12 10 | | 15:15 15:30 | 56 73 | | 158 157 | | | | | | 214 230 | |
| 03.30 | 3 | 14 | 10 | 29 | | | | 13 | 43 | 15:45 | 63 | 274 | 167 | 611 | | | | | 230 | 885 |
| 04:00 | 3 | | 10 | | | | | 13 | | 16:00 | 57 | | 169 | | | | | | 226 | |
| 04:15 04:30 | 7 5 | | 15 20 | | | | | 22 25 | | 16:15 16:30 | 72 89 | | 199 177 | | | | | | 271 266 | |
| 04:45 | 17 | 32 | 15 | 60 | | | | 32 | 92 | 16:45 | 82 | 300 | 188 | 733 | | | | | 270 | 1033 |
| 05:00 05:15 | 6 11 | | 25 24 | | | | | 31 35 | | 17:00 17:15 | 63 91 | | 205 215 | | | | | | 268 306 | |
| 05:30 | 11 | | 37 | | | | | 48 | | 17:30 | 79 | | 199 | | | | | | 278 | |
| 05:45 | 24 19 | 52 | 39 48 | 125 | | | | 63 67 | 177 | 17:45 18:00 | 77 63 | 310 | 205 193 | 824 | | | | | 282 256 | 1134 |
| 06:00 06:15 | 38 | | 46 67 | | | | | 105 | | 18:15 | 66 | | 189 | | | | | | 255 | |
| 06:30 | 33 | 400 | 71 | 0.47 | | | | 104 | 407 | 18:30 | 60 | 0.45 | 138 | | | | | | 198 | 045 |
| 06:45 07:00 | 49 64 | 139 | 81 51 | 267 | | | | 130 115 | 406 | 18:45 19:00 | 76 50 | 265 | 130 125 | 650 | | | | - | 206 175 | 915 |
| 07:15 | 92 | | 69 | | | | | 161 | | 19:15 | 62 | | 128 | | | | | | 190 | |
| 07:30 07:45 | 92 77 | 325 | 88 101 | 309 | | | | 180 178 | 634 | 19:30 19:45 | 77 63 | 252 | 84 77 | 414 | | | | | 161 140 | 666 |
| 08:00 | 64 | 323 | 109 | 307 | | | | 173 | 034 | 20:00 | 55 | 232 | 61 | 414 | | | | | 116 | 000 |
| 08:15 | 74 | | 93 | | | | | 167 | | 20:15 | 64 | | 61 | | | | | | 125 | |
| 08:30 08:45 | 85 68 | 291 | 100 69 | 371 | | | | 185 137 | 662 | 20:30 20:45 | 65 69 | 253 | 69 58 | 249 | | | | | 134 127 | 502 |
| 09:00 | 82 | | 60 | | | | | 142 | | 21:00 | 71 | | 39 | | | | | | 110 | |
| 09:15 09:30 | 53 63 | | 76 77 | | | | | 129 140 | | 21:15 21:30 | 50 56 | | 33 37 | | | | | | 83 93 | |
| 09:45 | 68 | 266 | 90 | 303 | | | | 158 | 569 | 21:45 | 64 | 241 | 43 | 152 | | | | | 107 | 393 |
| 10:00 10:15 | 75 64 | | 84 79 | | | | | 159 143 | | 22:00 22:15 | 51 67 | | 32 26 | | | | | | 83 93 | |
| 10:30 | 59 | | 94 | | | | | 153 | | 22:30 | 60 | | 25 | | | | | | 85 | |
| 10:45 | 58 | 256 | 76 | 333 | | | | 134 | 589 | 22:45 | 49 | 227 | 30 | 113 | | | | | 79 | 340 |
| 11:00 11:15 | 80 78 | | 74 73 | | | | | 154 151 | | 23:00 23:15 | 62 48 | | 18 32 | | | | | | 80 80 | |
| 11:30 | 47 | 202 | 72 | 205 | | | | 119 | F 7 4 | 23:30 | 36 | 170 | 22 | 01 | | | | | 58 | 252 |
| 11:45 TOTALS | 84 | 289 1822 | 66 | 285 2146 | | | | 150 | 574 3968 | 23:45 TOTALS | 32 | 178 3258 | 9 | 81 4845 | | | | | 41 | 259 8103 |
| | | | | | | | | | | | | | | | | | | | | |
| SPLIT % | | 45.9% | | 54.1% | | | | | 32.9% | SPLIT % | | 40.2% | | 59.8% | | | | | | 67.1% |
| | D | AILY 7 | TOT <u>A</u> | ALS | | NB | | SB / 001 | | EB | | WB | | | | | | | | otal |
| | | | | | | 5,080 | | 6,991 | | 0 | | 0 | | | | | | | 12, | ,071 |
| AM Peak Hour | | 07:00 | | 07:45 | | | | | 07:45 | PM Peak Hour | | 14:00 | | 17:00 | | | | | | 17:00 |
| AM Pk Volume Pk Hr Factor | | 325 | | 403 | | | | | 703 0.950 | PM Pk Volume Pk Hr Factor | | 334 | | 824 0.059 | | | | | | 1134 |
| 7 - 9 Volume | | 0.883 | | 0.924 680 | 0 | | 0 | | 1296 | 4 - 6 Volume | | 0.960 610 | | 0.958 1557 | | 0 | | 0 | | 0.926 2167 |
| 7 - 9 Peak Hour | | 07:00 | | 07:45 | | | | | | 4 - 6 Peak Hour | | 16:30 | | 17:00 | | | | | | 17:00 |
| 7 - 9 Pk Volume | | 325 | | 403 | | | | | | 4 - 6 Pk Volume | | 325 | | 824 | | | | | | 1134 |
| Pk Hr Factor | | 0.883 | | 0.924 | 0.000 | | 0.000 | | 0.950 | Pk Hr Factor | | 0.893 | | 0.958 | (| 0.000 | | 0.000 | | 0.926 |

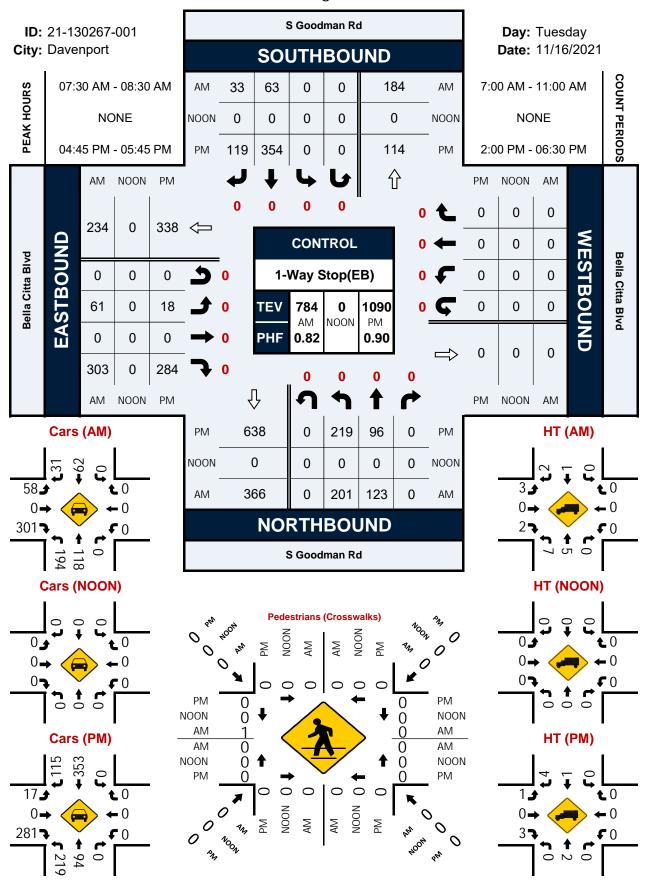


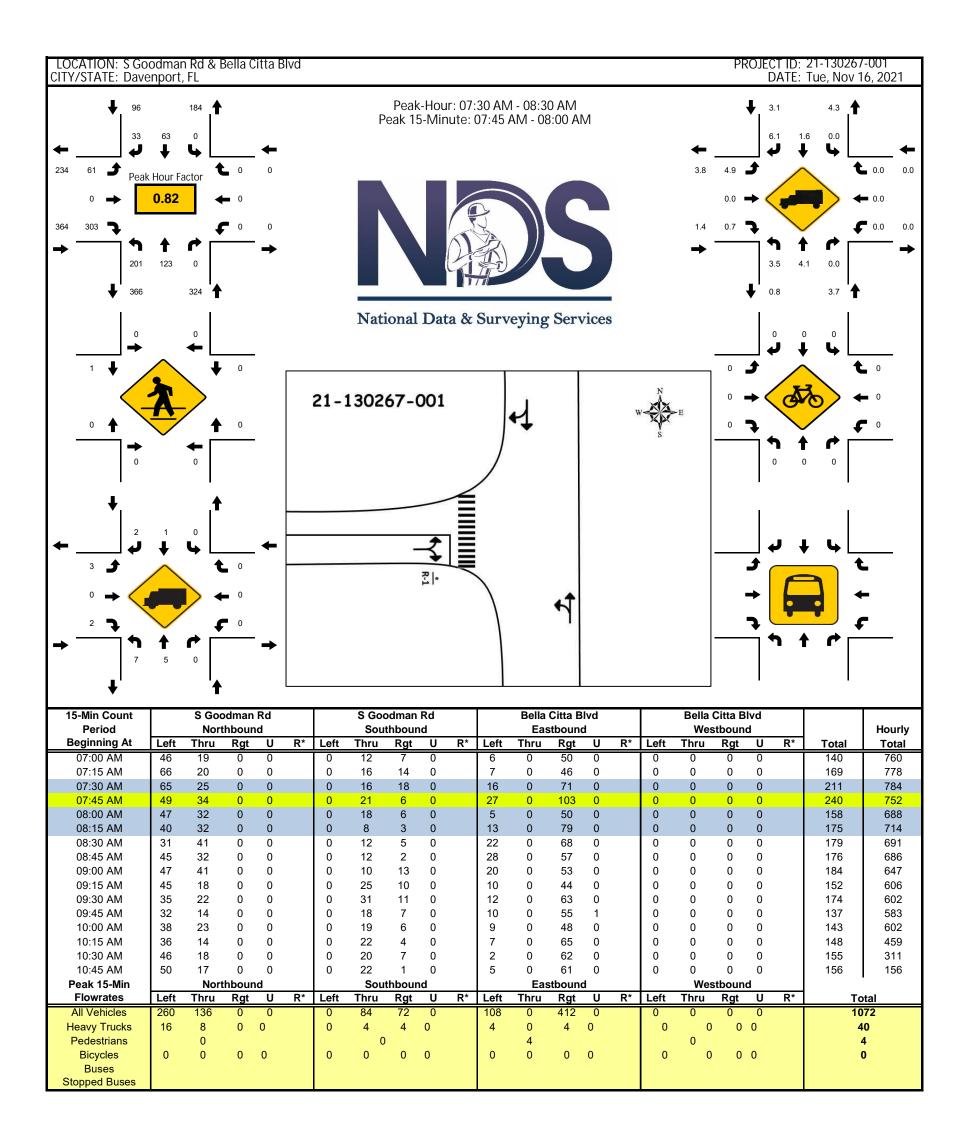


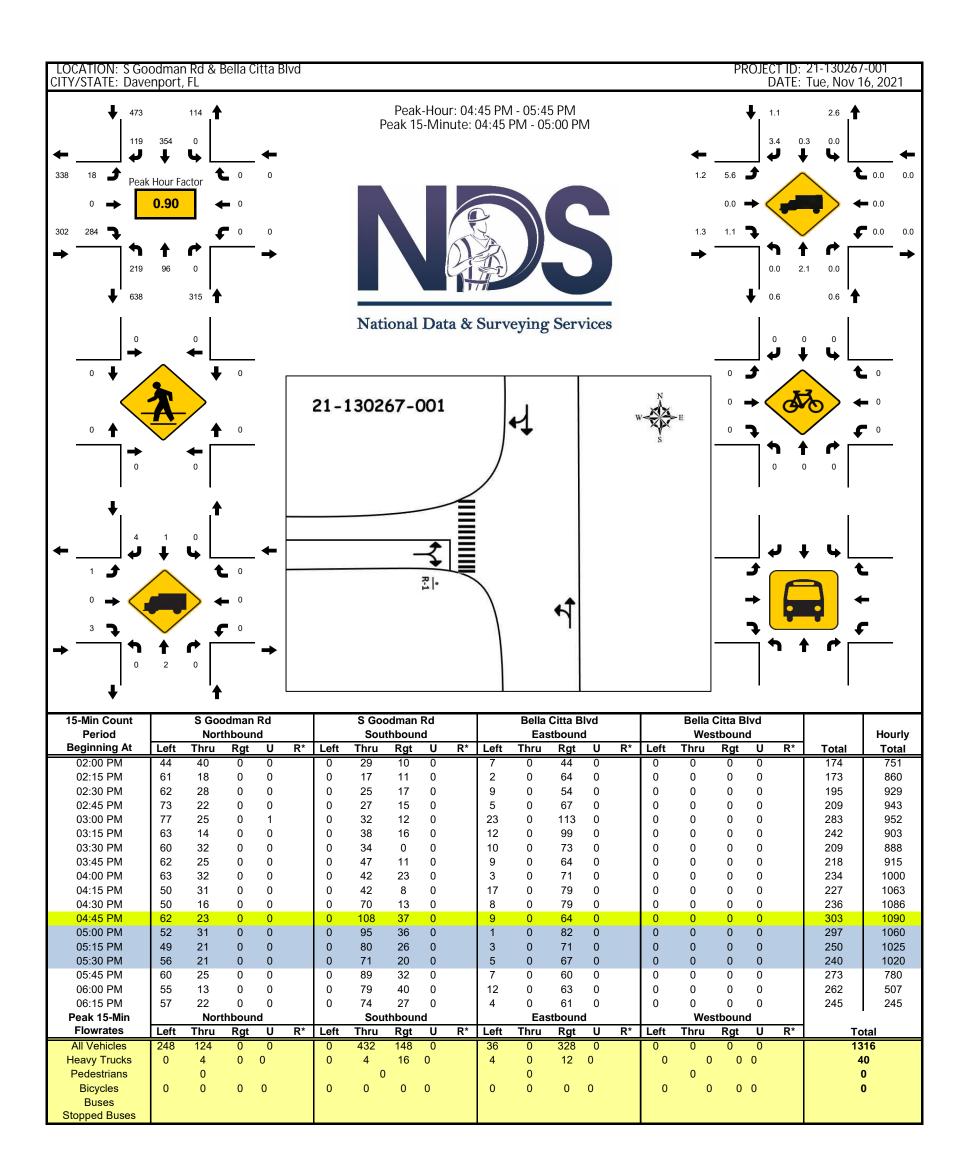


S Goodman Rd & Bella Citta Blvd

Peak Hour Turning Movement Count

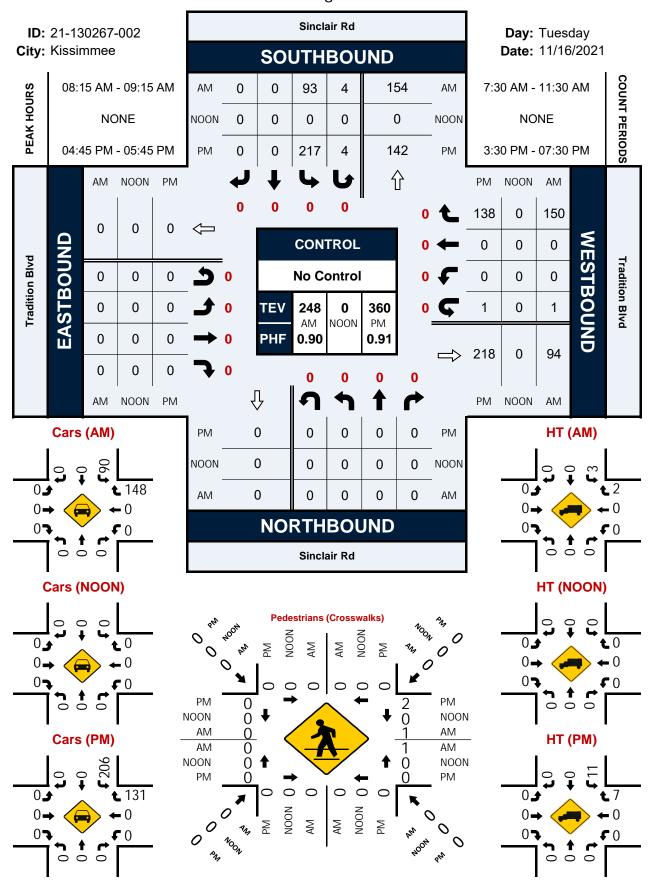


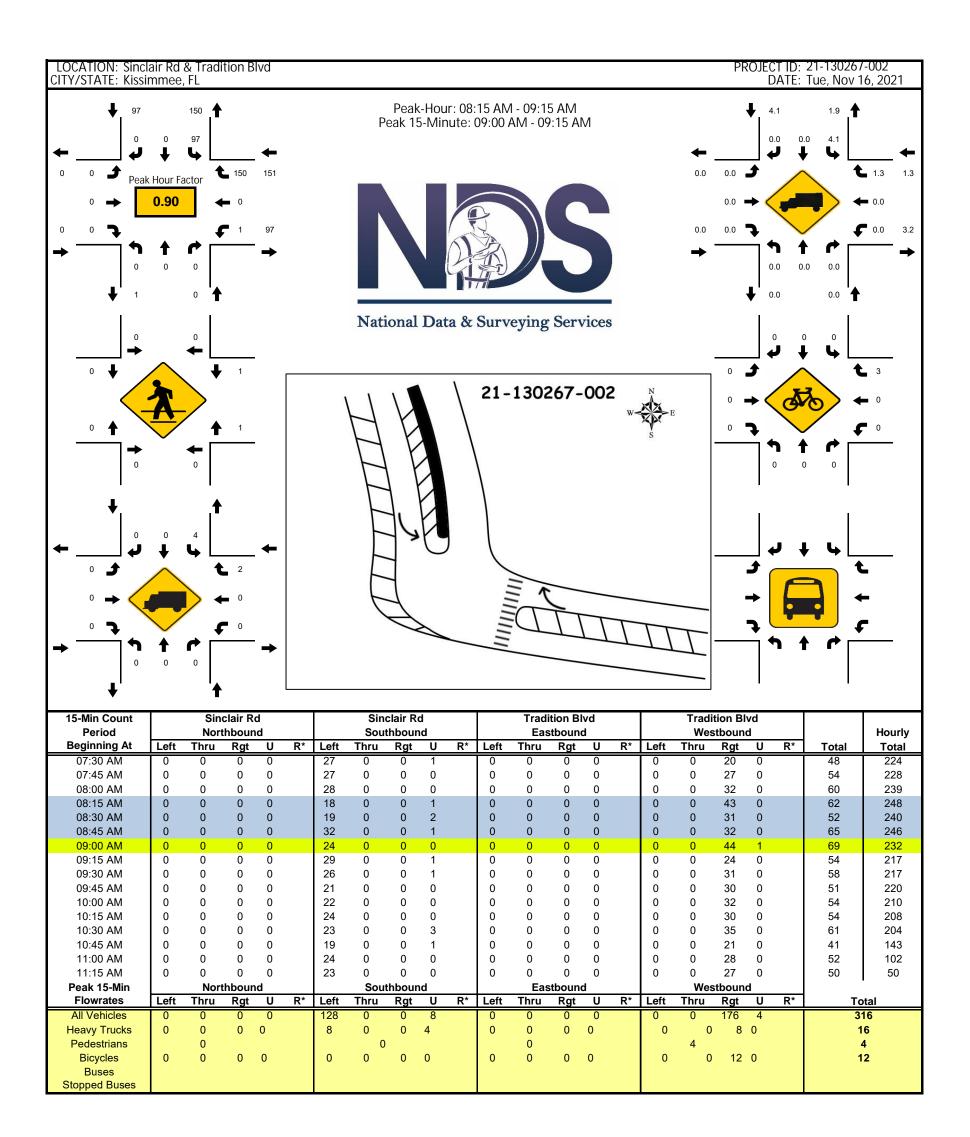


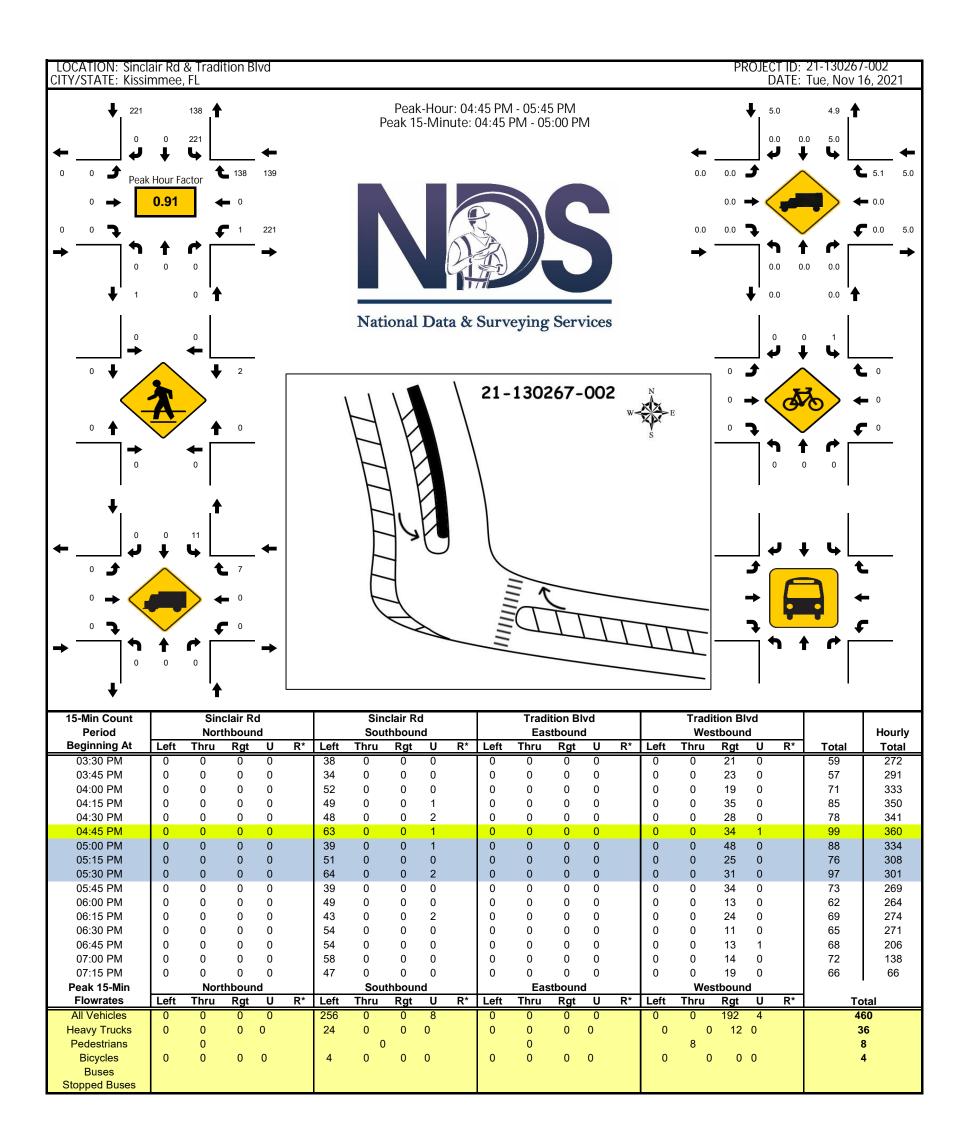


Sinclair Rd & Tradition Blvd

Peak Hour Turning Movement Count







APPENDIX C

FDOT Florida Traffic Online (FTO) Data

2020 PEAK SEASON FACTOR CATEGORY REPORT - REPORT TYPE: ALL

CATEGORY: 9200 OSCEOLA COUNTYWIDE

| CATEGO | DRY: 9200 OSCEOLA COUNTYWII | DE | MOCE. 0 01 |
|----------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|
| WEEK | DATES | SF | MOCF: 0.91 PSCF |
| ====================================== | 01/01/2020 - 01/04/2020 01/05/2020 - 01/11/2020 01/19/2020 - 01/18/2020 01/19/2020 - 01/25/2020 01/26/2020 - 02/01/2020 02/02/2020 - 02/01/2020 02/02/2020 - 02/01/2020 02/09/2020 - 02/25/2020 02/16/2020 - 02/29/2020 02/16/2020 - 02/29/2020 03/01/2020 - 03/07/2020 03/01/2020 - 03/07/2020 03/08/2020 - 03/21/2020 03/15/2020 - 03/28/2020 03/29/2020 - 03/28/2020 03/29/2020 - 04/04/2020 04/05/2020 - 04/11/2020 04/12/2020 - 04/18/2020 04/19/2020 - 04/18/2020 04/19/2020 - 05/02/2020 05/03/2020 - 05/02/2020 05/03/2020 - 05/02/2020 05/03/2020 - 05/02/2020 05/03/2020 - 05/02/2020 05/10/2020 - 05/16/2020 05/17/2020 - 05/16/2020 05/17/2020 - 05/13/2020 05/24/2020 - 05/30/2020 05/24/2020 - 06/2020 06/07/2020 - 06/2020 06/21/2020 - 06/27/2020 06/21/2020 - 07/11/2020 07/15/2020 - 07/11/2020 07/15/2020 - 07/11/2020 07/12/2020 - 07/18/2020 07/19/2020 - 07/18/2020 07/19/2020 - 07/18/2020 07/19/2020 - 08/01/2020 07/19/2020 - 08/01/2020 08/09/2020 - 08/01/2020 08/03/2020 - 08/01/2020 09/13/2020 - 09/12/2020 09/13/2020 - 09/12/2020 09/13/2020 - 09/12/2020 09/27/2020 - 09/12/2020 09/13/2020 - 09/12/2020 09/13/2020 - 09/12/2020 09/27/2020 - 10/03/2020 10/18/2020 - 10/10/2020 10/18/2020 - 10/24/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/21/2020 11/101/2020 - 11/21/2020 11/101/2020 - 11/21/2020 11/101/2020 - 11/28/2020 11/101/2020 - 11/21/2020 11/101/2020 - 11/21/2020 | | 1.04 0.99 0.93 0.93 0.92 0.91 0.95 0.99 1.03 1.07 1.11 1.25 1.40 1.54 1.68 1.57 1.47 1.36 1.26 1.24 1.21 1.19 1.16 1.13 1.14 1.14 1.14 1.14 1.14 1.11 1.10 1.10 |
| 53 | 12/27/2020 - 12/31/2020 | 0.85 | 0.93 |

^{*} PEAK SEASON

APPENDIX D

Volume Development Worksheet

Design Traffic Volume Characteristics

Intersection #1: Sinclair Road & Tradition Boulevard

Model Volumes

| | Year 204 | 5 Model Volumes (P | SWADT) ¹ | MOCF ² | Year 2045 AADT ³ |
|-----------|--------------|--------------------|---------------------|-------------------|-----------------------------|
| | Two-Way Vol. | Approach | Departure | MOCE | Year 2045 AADT |
| South Leg | 16,865 | 8440 | 8424 | 0.91 | 15,347 |
| North Leg | 22,412 | 12014 | 10399 | 0.91 | 20,395 |
| East Leg | 13,167 | 5769 | 7399 | 0.91 | 11,982 |

Existing Volumes

| | | 2021 Daily Tr | affic Counts ⁴ | | SF ² | Adjusted AADT | l |
|-----------|-------|---------------|---------------------------|---------|-----------------|---------------|---|
| | Day 1 | Day 2 | Day 3 | Average | эг | Aujusteu AADT | l |
| North Leg | 3,480 | 3,484 | 4,062 | 3,675 | 0.96 | 3,528 | l |
| East Leg | 3,480 | 3,484 | 4,062 | 3,675 | 0.96 | 3,528 | l |

Edst Lety 3,460 3,460 4,00

1. Peak Season Weekday Average Daily Traffic (PSWADT) obtained from model outputs (subject to rounding errors).

2. Per FDOT's Florida Traffic Online for Osceola County

3. Annual Average Daily Traffic (AADT) = PSWADT x MOCF

4. From data collection

2045 Buildout AADT for TURNS5 Input

| | 2045 AADT | Appr | oach | Depa | rture |
|-----------|-----------|------|--------|------|--------|
| South leg | 17,500 | 50% | 8,800 | 50% | 8,700 |
| North Leg | 22,500 | 54% | 12,100 | 46% | 10,400 |
| East Leg | 12,000 | 44% | 5,300 | 56% | 6,700 |

Design Traffic Volume Characteristics

Intersection #2: Goodman Road & Sinclair Road/Bella Citta Boulevard

Model Volumes

| | Year 204 | 15 Model Volumes (P | SWADT) ¹ | MOCF ² | Year 2045 AADT ³ |
|-----------|--------------|---------------------|---------------------|-------------------|-----------------------------|
| | Two-Way Vol. | o-Way Vol. Approach | | WIOCF | real 2045 AADT |
| South Leg | 9,701 | 4,975 | 4,724 | 0.91 | 8,828 |
| North Leg | 5,519 | 2,701 | 2,817 | 0.91 | 5,022 |
| West Leg | 13,879 | 6,879 | 6,999 | 0.91 | 12,630 |
| East Leg | 16,200 | 8,090 | 8,106 | 0.91 | 14,742 |

Existing Volumes

| | | 2021 Daily Tr | affic Counts ⁴ | | SF ² | Adjusted AADT |
|-----------|--------|---------------|---------------------------|---------|-----------------|---------------|
| | Day 1 | Day 2 | Day 3 | Average | ЭГ | Aujusteu AADT |
| South Leg | 11,115 | 11,091 | 12,071 | 11,426 | 0.96 | 10,969 |
| North Leg | 4,524 | 4,308 | 4,849 | 4,560 | 0.96 | 4,378 |
| West Leg | 9,129 | 9,005 | 10,077 | 9,404 | 0.96 | 9,028 |

Peak Season Weekday Average Daily Traffic (PSWADT) obtained from model outputs (subject to rounding errors).
 Per FDOT's Florida Traffic Online for Osceola County
 Annual Average Daily Traffic (AADT) = PSWADT x MOCF

2045 Buildout AADT for TURNS5 Input

| | 2045 AADT | Appr | oach | Depa | rture |
|-----------|-----------|------|-------|------|-------|
| South Leg | 14,500 | 51% | 7,400 | 49% | 7,100 |
| North Leg | 5,000 | 49% | 2,400 | 51% | 2,600 |
| West Leg | 17,000 | 50% | 8,400 | 50% | 8,600 |
| East Leg | 17,500 | 50% | 8,700 | 50% | 8,800 |

^{4.} From data collection

Kimley»Horn INTERSECTION VOLUME DEVELOPMENT SHEET

INTERSECTION #1

Sinclair Rd & Tradition Blvd

AM Peak Hour Factor: 0.90

| Weekday | | Sinclair Rd | | | Sinclair Ro | | | - | | Tradition Blvd | | | |
|----------------------------|------|-------------|------|------|-------------|------|------|-----------|------|----------------|-----------|------|--|
| AM Peak Hour | | Northbound | l | | Southbound | l | | Eastbound | | | Westbound | | |
| 08:15 AM - 09:15 AM | L | Т | R | L | Т | R | L | Т | R | L | Т | R | |
| Raw TMC | 0 | 0 | 0 | 97 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 150 | |
| Seasonal Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | |
| Heavy Vehicle | 0% | 0% | 0% | 4% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 1% | |
| Existing Volume (2021) | 0 | 0 | 0 | 93 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 144 | |
| D-Factor (Calculated) | | 0.61 | | | 0.39 | | | 0.39 | | | 0.61 | | |
| TURNS5 | | | | | | | | | | | | | |
| 2025 DHV (Model Volumes) | 0 | 134 | 26 | 153 | 81 | 0 | 0 | 0 | 0 | 25 | 0 | 245 | |
| Adjustments | | | | | | | | | | | | | |
| 2025 Design Hourly Volumes | 0 | 134 | 26 | 153 | 81 | 0 | 0 | 0 | 0 | 25 | 0 | 245 | |
| 2045 DHV (Model Volumes) | 0 | 809 | 152 | 296 | 490 | 0 | 0 | 0 | 0 | 156 | 0 | 502 | |
| Adjustments | | | | | | | | | | | | | |
| 2045 Design Hourly Volumes | 0 | 809 | 152 | 295 | 495 | 0 | 0 | 0 | 0 | 158 | 0 | 501 | |

PM Peak Hour Factor: 0.91

| Weekday | | Sinclair Ro | l | | Sinclair Ro | ł | | - | | Т | radition Bl | vd |
|----------------------------|------|-------------|------|------|-------------|------|------|-----------|------|------|-------------|------|
| PM Peak Hour | | Northbound | | | Southbound | t | | Eastbound | | | Westbound | t |
| 04:45 PM - 05:45 PM | L | Т | R | L | Т | R | L | Т | R | L | Т | R |
| Raw TMC | 0 | 0 | 0 | 221 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 138 |
| Seasonal Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicle | 0% | 0% | 0% | 5% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 5% |
| Existing Volume (2021) | 0 | 0 | 0 | 212 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 132 |
| D-Factor (Calculated) | | 0.39 | | | 0.61 | | | 0.61 | | | 0.39 | |
| TURNS5 | | | | | | | | | | | | |
| 2025 DHV (Model Volumes) | 0 | 78 | 24 | 236 | 130 | 0 | 0 | 0 | 0 | 25 | 0 | 148 |
| Adjustments | | | | | | | | | | | | |
| 2025 Design Hourly Volumes | 0 | 78 | 24 | 236 | 130 | 0 | 0 | 0 | 0 | 25 | 0 | 148 |
| 2045 DHV (Model Volumes) | 0 | 440 | 174 | 446 | 789 | 0 | 0 | 0 | 0 | 173 | 0 | 248 |
| Adjustments | | | | | | | | | | | | |
| 2045 Design Hourly Volumes | 0 | 440 | 174 | 446 | 789 | 0 | 0 | 0 | 0 | 173 | 0 | 248 |

Notes:

Kimley»Horn INTERSECTION VOLUME DEVELOPMENT SHEET

INTERSECTION #2

S Goodman Rd

&

Bella Citta Blvd / Sinclair Rd

AM Peak Hour Factor:

0.82

| Weekday | | | S Good | man Rd | | | | Bel | la Citta Blv | /d / Sinclai | r Rd | |
|----------------------------|------|------------|--------|--------|------------|------|------|-----------|--------------|--------------|-----------|------|
| AM Peak Hour | | Northbound | | | Southbound | i | | Eastbound | | | Westbound | 1 |
| 07:30 AM - 08:30 AM | L | Т | R | L | Т | R | L | Т | R | L | Т | R |
| Raw TMC | 201 | 123 | 0 | 0 | 63 | 33 | 61 | 0 | 303 | 0 | 0 | 0 |
| Seasonal Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicle | 3% | 4% | 0% | 0% | 2% | 6% | 5% | 0% | 1% | 0% | 0% | 0% |
| Existing Volume (2021) | 193 | 118 | 0 | 0 | 60 | 32 | 59 | 0 | 291 | 0 | 0 | 0 |
| D-Factor (Calculated) | | 0.49 | | | 0.51 | | | 0.61 | | | 0.39 | |
| TURNS5 | | | | | | | | | | | | |
| 2025 DHV (Model Volumes) | 304 | 118 | 89 | 20 | 120 | 67 | 88 | 68 | 411 | 58 | 32 | 12 |
| Adjustments | | | | | | | | | | | | |
| 2025 Design Hourly Volumes | 304 | 118 | 89 | 20 | 120 | 67 | 88 | 68 | 411 | 58 | 32 | 12 |
| 2045 DHV (Model Volumes) | 240 | 59 | 340 | 98 | 63 | 69 | 89 | 511 | 333 | 263 | 281 | 70 |
| Adjustments | | | | | | | | | | | | |
| 2045 Design Hourly Volumes | 240 | 59 | 340 | 98 | 63 | 69 | 89 | 511 | 333 | 263 | 281 | 70 |

PM Peak Hour Factor:

0.90

| Weekday | | | S Good | lman Rd | | | | | Bella C | itta Blvd | | |
|----------------------------|----------------------------------|------------|--------|---------|------------|------|------|-----------|---------|-----------|-----------|------|
| PM Peak Hour | | Northbound | i | | Southbound | i | | Eastbound | | | Westbound | |
| 04:45 PM - 05:45 PM | 04:45 PM - 05:45 PM L T R | | | L | Т | R | L | Т | R | L | Т | R |
| Raw TMC | 219 | 96 | 0 | 0 | 354 | 119 | 18 | 0 | 284 | 0 | 0 | 0 |
| Seasonal Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicle | 0% | 2% | 0% | 0% | 0% | 3% | 6% | 0% | 1% | 0% | 0% | 0% |
| Existing Volume (2021) | 210 | 92 | 0 | 0 | 340 | 114 | 17 | 0 | 273 | 0 | 0 | 0 |
| D-Factor (Calculated) | | 0.30 | | | 0.70 | | | 0.47 | | | 0.53 | |
| TURNS5 | | | | | | | | | | | | |
| 2025 DHV (Model Volumes) | 232 | 42 | 39 | 18 | 157 | 109 | 45 | 41 | 351 | 76 | 53 | 10 |
| Adjustments | | | | | | | | | | | | |
| 2025 Design Hourly Volumes | 232 | 42 | 39 | 18 | 157 | 109 | 45 | 41 | 351 | 76 | 53 | 10 |
| 2045 DHV (Model Volumes) | 186 | 23 | 183 | 105 | 103 | 107 | 43 | 341 | 335 | 386 | 399 | 50 |
| Adjustments | | | | | | | | | | | | |
| 2045 Design Hourly Volumes | 186 | 23 | 183 | 105 | 103 | 107 | 43 | 341 | 335 | 386 | 399 | 50 |

Notes:

| APPENDIX E |
|-----------------------------------------------------|
| Osceola County 2021 Roadway Network Capacity Report |

2021 Roadway Network Capacity Report (Updated 12/15/2021)

| Count | | | Adjusted Service Volumes | | | | | | et PM Peak Hour | | | | | | | | \neg | | | | | | |
|------------------|-----------------|-------------------------------------------------|----------------------------------------|-----------------------------------------|--------------|----------------|----------------|----------------|-----------------|-----------------------|------------|------------------|-------------------|--------------|--------------|----------------|----------------|----------------|--------------|------------------------|------------|----------------|--------------|
| Station # | Count Source | ROADWAY | FROM | то | В | С | D | Е | Count Year | Count Date (mm/dd) | Week | ADT | AADT | NB/EB | SB/WB | Pk Hr Total | Pk Dir | K-Factor | D-Factor | Pk Hr Pk Dir Vol | LOS | Capacity | V/C |
| 177 | OC | Bass Road | Yowell Rd | US 192 | 460 | 740 | 790 | 790 | 2021 | 4/22 | 17 | 7,762 | 7,840 | 204 | 349 | 553 | SB/WB | 0.071 | 0.63 | 349 | В | 790 | 0.44 |
| 183.1 | OC | Bella Citta Blvd | Oasis Club Blvd | Westside Blvd | 330 | 530 | 570 | 570 | 2021 | 3/24 | 13 | 11,620 | 11,504 | 460 | 484 | 944 | SB/WB | 0.081 | 0.51 | 484 | С | 570 | 0.85 |
| 184 467 | OC OC | Bella Citta Blvd Bill Beck Blvd | Westside Blvd US 192-441 | S Goodman Rd Fortune Rd | 330 | 530 1,200 | 570 1,590 | 570 1,680 | 2021 | 3/24 9/23 | 13 39 | 10,368 4,263 | 10,264 4.647 | 410 342 | 330 227 | 740 569 | NB/EB NB/EB | 0.071 | 0.55 0.60 | 410 342 | C | 570 1.590 | 0.72 |
| 474 | OC | Boggy Creek Rd (East) | Simpson Rd | Austin Tyndell Park | 460 | 740 | 790 | 790 | 2021 | 9/30 | 40 | 23,281 | 25,143 | 850 | 896 | 1,746 | SB/WB | 0.075 | 0.51 | 896 | F | 790 | 1.13 |
| 475 | OC | Boggy Creek Rd (East) | Austin Tyndell Park | Narcoossee Rd (CR 15) | 400 | 800 | 1,140 | 1,440 | 2021 | 9/30 | 40 | 18,225 | 19,683 | 721 | 917 | 1,638 | SB/WB | 0.090 | 0.56 | 917 | D | 1,140 | 0.80 |
| 510 | OC | Brown Chapel Rd | US 192-441 | Lakeshore Blvd | 480 | 770 | 830 | 830 | 2021 | 9/29 | 40 | 7,373 | 7,963 | 290 | 342 | 632 | SB/WB | 0.086 | 0.54 | 342 | В | 830 | 0.41 |
| 462 456 | 00 | Buenaventura Blvd Buenaventura Blvd | Simpson Rd Florida Pkwy | Florida Pkwy Osceola Pkwy | 1.400 | 1,200 | 1,590 1,760 | 1,680 | 2021 | 4/22 4/22 | 17 17 | 24,071 29,508 | 24,312 | 890 946 | 931 1334 | 1,821 2,280 | SB/WB SB/WB | 0.076 | 0.51 | 931 1,334 | C B | 1,590 1,760 | 0.59 |
| 452 | OC | Buenaventura Blvd | Osceola Pkwy | Orange County Line | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 4/22 | 17 | 35,172 | 35,524 | 1159 | 1557 | 2,716 | SB/WB | 0.077 | 0.57 | 1,557 | C | 1,760 | 0.70 |
| 605 | OC | Canoe Creek Rd (CR 523) | US 441/SR 15/Holopaw Rd | Sullivan Dr | 240 | 430 | 740 | 1,480 | 2021 | 10/21 | 43 | 2,644 | 2,750 | 109 | 163 | 272 | SB/WB | 0.103 | 0.60 | 163 | В | 430 | 0.38 |
| 523 | OC | Canoe Creek Rd (CR 523) | Sullivan Dr | Deer Run Rd | 420 | 800 | 1,120 | 1,420 | 2021 | 10/21 | 43 | 7,016 | 7,297 | 251 | 334 | 585 | SB/WB | 0.083 | 0.57 | 334 | В | 800 | 0.42 |
| 522 508 | OC | Canoe Creek Rd (CR 523) Canoe Creek Rd (CR 523) | Deer Run Rd Old Canoe Creek Rd | Old Canoe Creek Rd Nolte Rd | 480 480 | 770 770 | 830 830 | 830 830 | 2021 2021 | 10/6 10/6 | 41 | 17,719 16,547 | 18,782 17,540 | 637 662 | 893 659 | 1,530 1,321 | SB/WB NB/EB | 0.086 | 0.58 | 893 662 | F C | 830 830 | 1.08 |
| 521 | OC | Canoe Creek Rd (CR 523) | Nolte Rd | US 192-441 | 480 | 770 | 830 | 830 | 2021 | 10/6 | 41 | 14.131 | 14,979 | 465 | 733 | 1,198 | SB/WB | 0.085 | 0.61 | 733 | Č | 830 | 0.88 |
| 311 | ОС | Carroll St | Columbia Ave | Dyer Blvd | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 9/23 | 39 | 16,677 | 18,178 | 593 | 760 | 1,353 | SB/WB | 0.081 | 0.56 | 760 | В | 1,760 | 0.43 |
| 312 | OC | Carroll St | Dyer Blvd | Thacker Ave | 1,330 | 1,620 | 1,680 | 1,680 | 2021 | 10/14 | 42 | 11,989 | 12,469 | 551 | 508 | 1,059 | NB/EB | 0.088 | 0.52 | 551 | В | | 0.33 |
| 309 313 | OC OC | Carroll St | Thacker Ave John Young Pkwy | John Young Pkwy Main St/US 441-17/92 | 1,400 480 | 1,700 770 | 1,760 830 | 1,760 830 | 2021 2021 | 9/23 9/23 | 39 39 | 17,533 16,949 | 19,111 18,474 | 690 638 | 835 771 | 1,525 1,409 | SB/WB SB/WB | 0.087 | 0.55 0.55 | 835 771 | B D | 1,760 830 | 0.47 |
| 314 | OC | Carroll St | Main St/US 441-17/92 | Old Dixie Hwy | 480 | 770 | 830 | 830 | 2021 | 10/14 | 42 | 13,708 | 14.256 | 653 | 488 | 1,409 | NB/EB | 0.083 | 0.55 | 653 | C | 830 | 0.79 |
| 315 | OC | Carroll St | Old Dixie Hwy | Michigan Ave | 1,330 | 1,620 | 1,680 | 1,680 | 2021 | 10/14 | 42 | 12,062 | 12,544 | 625 | 467 | 1,092 | NB/EB | 0.091 | 0.57 | 625 | В | 1,680 | 0.37 |
| 153 | OC | Celebration Ave | US 192 | Celebration Blvd | 0 | 600 | 1,350 | 1,530 | 2021 | 3/23 | 13 | 15,595 | 15,439 | 718 | 506 | 1,224 | NB/EB | 0.078 | 0.59 | 718 | D | 1,350 | 0.53 |
| 154 | OC | Celebration Blvd | Celebration PI | World Dr | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 3/23 | 13 | 13,052 | 12,921 | 491 | 583 | 1,074 | SB/WB | 0.082 | 0.54 | 583 | В | 1,760 | 0.33 |
| 122 304 | OC OC | Champions Gate Blvd Clay St | Polk County Line Jack Calhoun Dr | Thacker Ave | 0 460 | 600 740 | 1,350 790 | 1,530 790 | 2021 2021 | 9/16 4/22 | 38 17 | 28,586 15,422 | 31,730 15,576 | 853 549 | 940 943 | 1,793 1,492 | SB/WB SB/WB | 0.063 | 0.52 0.63 | 940 943 | D F | 1,350 790 | 0.70 1.19 |
| 303 | OC | Clay St | Thacker Ave | Randolph Ave | 370 | 590 | 630 | 630 | 2021 | 4/22 | 17 | 6,342 | 6,405 | 198 | 440 | 638 | SB/WB | 0.101 | 0.69 | 440 | Ċ | 630 | 0.70 |
| 537 | OC | Creek Woods Dr | Canoe Creek Rd | Michigan Ave | 460 | 740 | 790 | 790 | 2021 | 3/9 | 11 | 3,217 | 3,153 | 179 | 117 | 296 | NB/EB | 0.092 | 0.60 | 179 | В | 790 | 0.23 |
| 222 | 00 | Cypress Pkwy | Marigold Ave | Pleasant Hilll Rd | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 4/1 | 14 | 43,417 | 43,417 | 1317 | 1652 | 2,969 | SB/WB | 0.068 | 0.56 | 1,652 | С | 1,760 | 0.94 |
| 1001 | OC OC | Cyrils Dr Cyrils Dr | Narcoossee Rd Zuni Rd | Zuni Rd Absher Rd | 370 370 | 590 590 | 630 630 | 630 630 | 2021 | 10/7 10/14 | 41 42 | 6,722 3,248 | 7,125 3,378 | 422 117 | 205 138 | 627 255 | NB/EB SB/WB | 0.093 | 0.67 | 422 138 | C B | 630 630 | 0.67 |
| 524 | OC | Deer Run Rd | Canoe Creek Rd (CR 523) | Hickory Tree Rd | 400 | 800 | 1,140 | 1,440 | 2021 | 10/21 | 43 | 7,277 | 7,568 | 256 | 379 | 635 | SB/WB | 0.087 | 0.60 | 379 | В | 1,140 | 0.33 |
| 352 | ОС | Donegan Ave | John Young Pkwy | US 17/92 | 0 | 530 | 770 | 810 | 2021 | 3/3 | 10 | 11,775 | 11,657 | 427 | 550 | 977 | SB/WB | 0.083 | 0.56 | 550 | D | 770 | 0.71 |
| 353 | OC | Donegan Ave | US 17/92 | Michigan Ave | 480 | 770 | 830 | 830 | 2021 | 3/3 | 10 | 12,549 | 12,424 | 667 | 415 | 1,082 | NB/EB | 0.086 | 0.62 | 667 | С | 830 | 0.80 |
| 224 | 00 | Doverplum Ave | Old Pleasant Hill Rd | Cypress Pkwy | 460 | 740 | 790 | 790 | 2021 | 4/1 | 14 | 6,826 | 6,826 | 470 | 188 | 658 | NB/EB | 0.096 | 0.71 | 470 | C F | | 0.59 |
| 223 229 | 00 | Doverplum Ave Enterprise Dr/Mercantile Ln | Cypress Pkwy Poinciana Blvd | Koa St Cattle Dr | 460 370 | 740 590 | 790 630 | 790 630 | 2021 | 4/6 9/16 | 15 38 | 21,133 1,961 | 21,133 | 844 132 | 676 110 | 1,520 242 | NB/EB NB/FB | 0.072 | 0.56 | 844 132 | B | 790 630 | 1.07 0.21 |
| 520 | OC | Fifth St (St Cloud) | Old Canoe Creek Rd | Vermont Ave | 330 | 530 | 570 | 570 | 2021 | 9/29 | 40 | 2,826 | 3,052 | 155 | 91 | 246 | NB/EB | 0.087 | 0.63 | 155 | В | 570 | 0.27 |
| NA1 | OC | Florence Villa Grove Rd | Polk County Line | Westside Blvd | 460 | 740 | 790 | 790 | 2021 | 9/16 | 38 | 10,460 | 11,611 | 369 | 505 | 874 | SB/WB | 0.084 | 0.58 | 505 | С | 790 | 0.64 |
| 453 | OC | Florida Pkwy | Osceola Pkwy | Buenaventura Blvd | 330 | 530 | 570 | 570 | 2021 | 10/7 | 41 | 4,907 | 5,201 | 231 | 189 | 420 | NB/EB | 0.086 | 0.55 | 231 | В | 570 | 0.41 |
| 972000 972110 | FDOT | Florida's Turnpike Florida's Turnpike | Osceola Pkwy US 192/441 | US 192-441 Kissimmee Park Rd | 2,200 | 3,020 | 3,720 3,720 | 4,020 | 2020 2020 | N/A N/A | N/A N/A | N/A N/A | 61,200 43,100 | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | 3,720 3,720 | NA NA |
| 972110 | FDOT | Florida's Turnpike | Kissimmee Park Rd | Indian River County | 2,200 | 2.880 | 3,400 | 3,600 | 2020 | N/A | N/A | N/A | 27.800 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2.880 | NA |
| 972001 | FDOT | Florida's Turnpike | Orange County Line | Osceola Pkwy | 2,200 | 3,020 | 3,720 | 4,020 | 2020 | N/A | N/A | N/A | 74,500 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 3,720 | NA |
| 119 | OC | Formosa Gardens Blvd | Sinclair Rd | Funie Steed Rd | 400 | 800 | 1,140 | 1,440 | 2021 | 10/21 | 43 | 5,935 | 6,172 | 205 | 305 | 510 | SB/WB | 0.086 | 0.60 | 305 | В | 1,140 | 0.27 |
| 117 | OC | Formosa Gardens Blvd | Funie Steed Rd | US 192 | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 9/16 | 38 | 14,263 | 15,832 | 499 | 680 | 1,179 | SB/WB | 0.083 | 0.58 | 680 | В | 1,760 | 0.39 |
| 469 414 | OC | Fortune Rd Fortune Rd | US 192-441 Simpson Rd | Simpson Rd Lakeshore Blvd | 420 | 1,200 840 | 1,590 1,200 | 1,680 | 2021 | 9/23 | 39 41 | 29,602 15,425 | 32,266 16.351 | 1390 975 | 949 733 | 2,339 1.708 | NB/EB NB/EB | 0.079 | 0.59 | 1,390 975 | D D | 1,590 1,200 | 0.87 |
| 561 | OC | Friars Cove Rd | Florida's Turnpike | Canoe Creek Rd (CR 523) | 270 | 430 | 460 | 460 | 2021 | 10/7 | 41 | 4.837 | 5,127 | 183 | 279 | 462 | SB/WB | 0.096 | 0.60 | 279 | C | 460 | 0.61 |
| 118 | ОС | Funie Steed Rd | Westside Blvd | Formosa Gardens Blvd | 400 | 800 | 1,140 | 1,440 | 2021 | 9/16 | 38 | 12,526 | 13,904 | 308 | 661 | 969 | SB/WB | 0.077 | 0.68 | 661 | С | 1,140 | 0.58 |
| 112 | OC | Funie Steed Rd | Formosa Gardens Blvd | Old Lake Wilson Rd | 330 | 530 | 570 | 570 | 2021 | 3/24 | 13 | 7,029 | 6,959 | 231 | 226 | 457 | NB/EB | 0.065 | 0.51 | 231 | В | 570 | 0.41 |
| 126 | OC | Goodman Rd Goodman Rd | Westside Blvd Monaco Blvd | Monaco Blvd | 330 460 | 530 740 | 570 790 | 570 790 | 2021 | 4/1 | 14 43 | 4,042 | 4,042 4,468 | 132 124 | 332 | 464 446 | SB/WB SB/WB | 0.115 0.104 | 0.72 | 332 | C B | 570 790 | 0.58 |
| 1261 232 | OC | Ham Brown Rd | Reaves Rd | Happy Trl Cattle Drive Ln | 400 | 800 | 1,140 | 1.440 | 2021 | 10/21 4/7 | 15 | 4,296 16,242 | 16,242 | 789 | 322 774 | 1,563 | NB/EB | 0.096 | 0.72 | 322 789 | C | 1.140 | 0.69 |
| 203 | OC | Ham Brown Rd | Cattle Drive Ln | US 17/92 | 400 | 800 | 1,140 | 1,440 | 2021 | 9/22 | 39 | 15,621 | 17,027 | 439 | 803 | 1,242 | SB/WB | 0.080 | 0.65 | 803 | D | | 0.70 |
| 540 | OC | Hickory Tree Rd | US 192 (West) | Nolte Rd | 480 | 770 | 830 | 830 | 2021 | 9/29 | 40 | 14,780 | 15,962 | 393 | 552 | 945 | SB/WB | 0.064 | 0.58 | 552 | С | 830 | 0.67 |
| 548 | 00 | Hickory Tree Rd | Nolte Rd | Deer Run Rd | 400 | 800 | 1,140 | 1,440 | 2021 | 10/6 | 41 | 3,991 | 4,230 | 186 | 242 | 428 | SB/WB | 0.107 | 0.57 | 242 | В | 1,140 | 0.21 |
| 531 23 | OC OC | Hickory Tree Rd Hoagland Blvd | Deer Run Rd US 17/92 | US 192 (East) US 192 | 420 1.400 | 1.700 | 1,120 1,760 | 1,420 | 2021 | 10/6 5/5 | 41 19 | 3,019 17,243 | 3,200 17.588 | 121 653 | 162 883 | 283 1,536 | SB/WB SB/WB | 0.094 | 0.57 | 162 883 | B | 800 1.760 | 0.20 |
| 302 | OC | Jack Calhoun Dr | N Hoagland Blvd | S Hoagland Blvd | 1,330 | 1,620 | 1,680 | 1,680 | 2021 | 9/23 | 39 | 4,117 | 4,488 | 174 | 173 | 347 | NB/EB | 0.084 | 0.50 | 174 | В | 1,680 | 0.10 |
| 152 | OC | International Drive South | US 192 | Orange County Line | 2,160 | 2,570 | 2,650 | 2,650 | 2021 | 10/14 | 42 | 16,198 | 16,846 | 736 | 481 | 1,217 | NB/EB | 0.075 | 0.60 | 736 | В | 2,650 | 0.28 |
| 160111 | FDOT* | Interstate 4 | Osceola Polk Line Rd (CR 532) | SR 429 | 3,300 | 4,580 | 5,580 | 6,200 | 2019 | N/A | N/A | N/A | 134,000 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 5,580 | NA |
| 920321 | FDOT* | Interstate 4 Interstate 4 | SR 429 World Dr | World Dr US 192 | 3,300 | 4,580 4.580 | 5,580 5,580 | 6,200 | 2019 2019 | N/A N/A | N/A N/A | N/A N/A | 125,000 92,000 | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | N/A N/A | 5,580 5,580 | NA NA |
| 750668 | FDOT* | | US 192 | Orange County Line | 3,300 | 4,580 | 5,580 | 6,200 | 2019 | N/A | N/A | N/A | 133,500 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 5,580 | NA |
| 553 | OC | Jack Brack Rd | Narcoossee Rd (CR 15) | Zuni Rd | 420 | 680 | 720 | 720 | 2021 | 9/30 | 40 | 6,680 | 7,214 | 274 | 283 | 557 | SB/WB | 0.083 | 0.51 | 283 | В | 680 | 0.42 |
| 5531 | OC_ | Jack Brack Rd | Zuni Rd | Absher Rd | 370 | 590 | 630 | 630 | 2021 | 9/30 | 40 | 1,136 | 1,227 | 38 | 81 1427 | 119 2.984 | SB/WB | 0.105 | 0.68 | 81 | B B | 630 2.650 | 0.13 |
| 318 317 | OC | John Young Pkwy John Young Pkwy | US 192 Columbia Ave | Columbia Ave Carroll St | 2,160 | 2,570 | 2,650 2,650 | 2,650 2,650 | 2021 2021 | 9/23 9/23 | 39 39 | 44,213 48,946 | 48,192 53,351 | 1557 1659 | 1802 | 3,461 | NB/EB SB/WB | 0.067 | 0.52 | 1,557 1,802 | В | 2,650 | 0.59 |
| 316 | OC | John Young Pkwy | Carroll St | Orange County Line | 2,160 | 2,570 | 2,650 | 2,650 | 2021 | 3/2 | 10 | 51,656 | 51,139 | 1801 | 1968 | 3,769 | SB/WB | 0.073 | 0.52 | 1,968 | В | 2,650 | 0.74 |
| 554 | OC | Jones Rd | Narcoossee Rd | Gerry Ct | 330 | 530 | 570 | 570 | 2021 | 3/9 | 11 | 3,632 | 3,559 | 128 | 156 | 284 | SB/WB | 0.078 | 0.55 | 156 | В | 570 | 0.27 |
| 405 | OC | Kings Hwy | Pine Island Rd | Neptune Rd | 400 | 800 | 1,140 | 1,440 | 2021 | 9/29 | 40 | 4,488 | 4,847 | 243 | 141 | 384 | NB/EB | 0.086 | 0.63 | 243 | В | | 0.21 |
| 505 | OC | Kissimmee Park Rd | Old Canoe Creek Rd Rhododendrom Ave | Lake Tohopekaliga | 420 460 | 800 740 | 1,120 790 | 1,420 790 | 2021 | 3/9 9/16 | 11 38 | 2,499 12.603 | 2,449 13.989 | 103 542 | 109 502 | 212 1.044 | SB/WB NB/EB | 0.085 | 0.51 | 109 542 | B C | 800 790 | 0.14 |
| 226 227 | OC | Koa St Koa St | Marigold Ave | Marigold Ave Doverplum Ave | 370 | 590 | 630 | 630 | 2021 | 4/1 | 14 | 16,672 | 16,672 | 567 | 623 | 1,190 | SB/WB | 0.003 | 0.52 | 623 | D | 630 | 0.99 |
| 416 | OC | Lakeshore Blvd | Fortune Rd | Partin Settlement Rd | 400 | 800 | 1,140 | 1,440 | 2021 | 9/29 | 40 | 12,999 | 14,039 | 444 | 583 | 1,027 | SB/WB | 0.079 | 0.57 | 583 | С | 1,140 | 0.51 |
| 417 | OC | Lakeshore Blvd | Partin Settlement Rd | Brown Chapel Rd | 400 | 800 | | | 2021 | 10/7 | 41 | 16,156 | | | 940 | 1,633 | SB/WB | 0.101 | 0.58 | 940 | D | 1,140 | 0.82 |
| 516 | 00 | Lakeshore Blvd | Brown Chapel Rd | Mississippi Ave | 400 | 800 | 1,140 | | 2021 | 9/29 | 40 | 9,831 24,255 | 10,617 | 539 | 369 | 908 | NB/EB | 0.092 | 0.59 | 539 | C F | | 0.47 |
| 225 230 | OC OC | Marigold Ave Marigold Ave | Cypress Pkwy Koa St | Koa St Poinciana Pkwy | 480 460 | 770 740 | 830 790 | 830 790 | 2021 2021 | 3/31 4/1 | 14 14 | | 16,091 | 725 640 | 1023 676 | 1,748 1,316 | SB/WB SB/WB | | 0.59 | 1,023 676 | | | 1.23 0.86 |
| 121 | OC | Masters Blvd/Goodman Rd | Champions Gate Blvd | Bella Citta Blvd | 480 | | 830 | 830 | 2021 | 10/7 | 41 | 11,215 | 11,888 | 351 | 636 | 987 | SB/WB | 0.088 | 0.64 | 636 | Č | | 0.00 |
| 335 | OC | Michigan Ave (CR 531) | US 192-441 | Donegan Ave | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 9/23 | 39 | 28,535 | 31,103 | 1159 | 1075 | 2,234 | NB/EB | 0.078 | 0.52 | 1,159 | В | 1,760 | 0.66 |
| 334 | | Michigan Ave (CR 531) | Donegan Ave | Carroll St | | | 1,760 | | | 3/3 | | | 32,545 | | 1325 | 2,596 | SB/WB | | 0.51 | 1,325 | | | 0.75 |
| 333 | 00 | Michigan Ave (CR 531) | Carroll St Lakeshore Blvd | Osceola Pkwy US 192-441 | | | 1,590 460 | | | 3/3 | 10 | | 31,799 | | 1206 | 2,518 | NB/EB SB/WB | | 0.52 | 1,312 | | | 0.83 |
| 556 518 | OC | Michigan Ave (St Cloud) Michigan Ave (St Cloud) | US 192 | Nolte Rd | 270 400 | 800 | 1,140 | 460 1,440 | 2021 2021 | 9/29 10/7 | 40 41 | 2,784 5,662 | 3,007 6,002 | 127 220 | 138 326 | 265 546 | SB/WB SB/WB | 0.095 0.096 | 0.52 | 138 326 | B | | 0.30 |
| 534 | OC | Michigan Ave (St Cloud) | Nolte Rd | Creek Woods Dr | 400 | 800 | 1,140 | | 2021 | 10/6 | 41 | 2,345 | 2,486 | 107 | 125 | 232 | SB/WB | 0.099 | 0.54 | 125 | В | | 0.11 |
| 551 | OC | Narcoossee Rd (CR 15) | Orange County Line | Jones Rd | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 4/1 | 14 | 37,977 | 37,977 | 1275 | 1766 | 3,041 | SB/WB | 0.080 | 0.58 | 1,766 | F | 1,760 | 1.00 |
| 539 | 00 | Narcoossee Rd (CR 15) | Jones Rd | Rummel Rd | | 2,560 | | | | 3/9 | 11 | 36,408 | 35,680 | 1287 | 1710 | 2,997 | SB/WB | 0.082 | 0.57 | 1,710 | | | 0.52 |
| 541 589 | 00 | Narcoossee Rd (CR 15) Narcoossee Rd (CR 15) | Rummel Rd 10th St | 10th St US 192-441 | | | 1,760 1,760 | | 2021 2021 | 3/9 4/7 | 11 15 | 33,080 34,086 | 32,418 | 1121 1218 | 1651 1454 | 2,772 2,672 | SB/WB SB/WB | | 0.60 | 1,651 1,454 | | | 0.94 |
| | | Narcoossee Rd (CR 15) Neptune Rd | Broadway Ave/Main St | US 192-441 Lakeshore Blvd | | | 1,760 | | | 3/2 | 10 | 22,501 | 22,276 | | 700 | 1,622 | NB/EB | | | 1,454 922 | | | 0.83 |
| 504 | 50 | 1 | ot | | .,+00 | .,,,,, | .,,,,,, | ., | 2021 | JI 2 | | ,501 | ,210 | , VEE | | 1,522 | 110/20 | 0.012 | 0.07 | - VAL | | 1,7.00 | 0.02 |

2021 Roadway Network Capacity Report (Updated 12/15/2021)

| March Marc | | | | | | | Adi | | rvice Volu | mes | | | | | | | | | | PM Peak H | lour | | | | |
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| March Marc | Count Station # | | | ROADWAY | FROM | то | | | | | | | Week | ADT | AADT | NB/EB | SB/WB | | Pk Dir | K-Factor | D-Factor | Pk Dir | LOS | Capacity | V/C |
| Out Control | 363 | 00 | C | Neptune Rd | Lakeshore Blvd | Kings Hwy | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 4/22 | 17 | 27,963 | 28,243 | 1367 | 912 | 2,279 | NB/EB | 0.082 | 0.60 | | В | 1,760 | 0.78 |
| 15 15 15 15 15 15 15 15 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15 15 15 15 15 15 15 15 | | | | | | | | | | | | | | | | | | | | | | | | | |
| March Control Contro | | | | | | | | | | | | | | | | | | | | | | | | | |
| Section Control of | | | | | | Michigan Ave | | | | | | | | | | | | | | | | | | | 0.34 |
| Margin M | | | | | | | | | | | | | | | | | | | | | | | | , | 0.41 |
| Column C | | | | | | | | | | | | | | | | | | 110 | | | | | | | |
| 100 Co. | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 10 10 10 10 10 10 10 | | | | | | | | | | | | | | | | | | | | | | | | | 0.58 |
| Contract No. Prospect of Contract No. Contrac | | | | | | | | | | 1,680 | | | | 27,111 | | | | | | | | | | | 0.78 |
| 150 Co. Co. State Co. Co | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 10 10 10 10 10 10 10 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100 C. C. C. C. C. C. C. | | | | | | | | | | | | | | | | | | | | | | | | | 1.33 |
| 10 10 10 10 10 10 10 10 | 105 | | | Old Lake Wilson Rd (CR 545) | | Westgate Blvd | 1,400 | | 1,760 | | 2021 | 3/23 | 13 | 20,028 | 19,828 | 741 | 928 | 1,669 | SB/WB | 0.083 | 0.56 | 928 | В | 1,760 | 0.53 |
| Section Sect | | | | | | | | | | | | | | | | | | | | | | | | | 0.46 |
| 230 C. O. Sample Mary Proposed Bell Proposed Bell Proposed Reg Prop | | | | | | | | | | | | | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Second Perform Control Per | | | | | | | | | | | | | | | | | | | | | | | | | 0.55 |
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| 1812 G. Concide Port | 180 | 00 | C | | SR 417 | | | | | | 2021 | 10/7 | 41 | 22,502 | | 1137 | 863 | 2,000 | NB/EB | 0.089 | 0.57 | | В | | 0.65 |
| 200 Concest Rept | 183.2 | | | | Vineland Rd (SR 535) | Sunrise City Dr/Storey Lake Blvd | | 1,700 | 1,760 | 1,760 | 2021 | | | 27,120 | 29,290 | | 909 | 2,398 | NB/EB | 0.088 | 0.62 | 1,489 | С | 1,760 | 0.85 |
| 20 Control Press | | | | | | | | ., | | | | | | | | | | | | | | | | | 0.75 |
| 200 C. Concess Pear C. Concess Pear C. C. C. C. C. C. C. C | | | | , | | | _ | | | | | | | | | | | | | | | | | | |
| Add Col. December Party Product Transport Product Transport Transport Product Transport Transp | | | | | | | _ | | | | | | | - , - | | | | | | | | | | | |
| 1911 O. Dorsch Pick Left M (17) S25 Left D. Left D | | | | | Florida's Turnpike | | | | | | | | | | | | | | | | | | | | 0.69 |
| 100 Oct December Peal Law (197 SED) Old Law Wilson Red Us 1702 W 197 For Top T | | | | | | | | | | | | | | | | | | | | | | | | | 0.69 |
| Month Mont | | | | (0.110) | | | | | | | | | | | | | | | | | | | | | |
| April 100 Perin Enterward No. 101 102-41 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 103 1 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 150 Co. Prescription 15 15 15 15 15 15 15 1 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 221 C.C. | | | | | | | | | | | | | | | | | 110 | | | | | | | | 0.18 |
| 22 C.C. Personal Hold Personal State General Assemble Gene | | | | | | | | | | | | | | , | | | | | | | | | | , . | 0.21 |
| 256 C.C. Pleasest Hill Bill Oranizor Youn Pleas. Mr. 1792 Lead Le | | | | | | | | ., | | | | | | | | | | | | | | | | | |
| 233 C.C. Personal Bird Personal Hill Rd P | | | | | i diridiana bira | | | | | | | | | | | | | | | | | | | | |
| 202 C.C. Penecam Bord S. 1702 S. 1702 S. 1703 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 161 CC Promota Birt Co Promota Birt Promota Birt Co Promota Birt Pro | 202 | | | Poinciana Blvd | | | | 1,700 | | | | 10/21 | 43 | 34,041 | | | | 2,407 | | | 0.62 | 1,489 | С | 1,760 | 0.85 |
| 160 CC Promiss Bart Str 150 (Emorate Net) 1.50 (Emor | | | | | | | | | | | | | | | | | | | | | | | | | |
| 199 CC Processing Bird US 192 (Brossons hely) Vinetard Rd (SR RdS) 1,400 1,700 7,700 1,700 2,221 1,977 1,983 1,970 1,970 2,970 7,700 1,970 2,970 2,970 7,700 1,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 2,970 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188 CO Popmenent lie Bed US 192 Vinetand Rel (RS 35) 1,330 1,200 1,800 1,800 2,000 2,000 2,000 3,100 1,000 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 3,100 | | | | | | | | | | | | | | | | | | | | | | | | | 0.44 |
| 211 COC Reserve Ref Pencicians Bird Pencicians Bird Simpson Rd St. 500 0.022 301 301 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 303 | | | | | | | | | | | | | | | | | | | | | | | | | 0.32 |
| 465 COC Royal Philin Dr | | | | | | | | | | | | | | | | | | | | | | | | | 0.35 |
| Second Column Fig. Maintaings Are | | | | | | | | | | | | | | | | | | | | | | | | | |
| 107 OC Sand Hill Ref Fermosa Gesderee Blord Old Lake Wilson Ref (CR 144) 400 770 780 790 790 2021 1071 43 2,888 2,796 74 193 287 89WB 0.090 0.72 193 8 790 0.24 443 OC Sand Lake Ref CR 144 0.00 770 780 0.00 11,965 71,971 2857 381 978 81,978 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 173 OC Sheebeeth Rd US 192 Orange County Line 460 770 790 790 2021 477 15 13,439 13,439 229 779 1,068 SBWB 0.079 0.73 779 0 790 0.02 | | | | | | | | | | | | | | | | | | | | | | | | | 0.24 |
| 173 CC Senta Lapp Dr | | | | | | - 1 | | | | | | | | | | | | | | | | | | | |
| 1412 O.C. Simpson Red US 192-441 Fortune Rd 460 770 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 790 | | | | | | | | | | | | | | | | | | | | | | | | | |
| ATZ OC Simpson Rd | | | | | | | | | | | | | | | | | | | | | | | | | |
| A73 C. Simpson Rd | | | | | | | | | | | | | | | | | | -, | | | | | | | |
| 106 CC Sinclair Rd | | | | | | | | | | | | | | | | | | | | | | | F | | 1.16 |
| 214 CC Southport RG Pieseant Hill Rd Southport RG 420 800 1,120 1,420 2021 916 38 810 677 35 37 72 SBWB 0,118 0,51 37 B 800 0,05 | | | | | | | | | | | | | | | | | | | | | | | F | | 1.32 |
| 97280 FOOT SR 417 Celebration Ave 2,200 3,020 3,720 4,020 2020 NIA 3,720 NIA 97280 FOOT SR 417 Oscoela Pkwy 0scoela Pkwy 2,200 3,020 3,720 4,020 2020 NIA 3,720 NIA 7,720 NIA NI | | | | | | | | | | | | | | | | | | | | | | | | | |
| 972809 FDOT SR 417 Celebration Ave Oscola Pkwy Cargo County Line Cargo County | | | | | | | | | | | | | | | | | | | | | | | | | |
| 972809 FDOT SR 417 OSceola Pkwy Orange County Line 2,200 3,020 3,720 4,020 2020 N/A | 972620 | | | | | | | | | | | | | | | | | | | | | | | | |
| 972810 FDOT SR 429 (Western Bethway) Sinclair Rd US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) US 192 (Apple County Line September 1920 SR 525 (Wilstand Rd) September 1920 SR 525 (Wi | 972630 | | | SR 417 | Osceola Pkwy | | | | | 4,020 | 2020 | | | | | | | | | | | | | | NA |
| Space Pool SR 535 (Wineland Rd) US 192 Poinclaina Blwd O 1,330 1,770 1,870 2020 N/A | | | | | | | | | | | | | | | | | | | | | | | | | |
| 923 C SR 535 (Vineland Rid) Poinciana Bilvd Poinciana Bil | | | OT | SR 429 (Western Beltway) | | | | | | | | | | | | | | | | | | | | | |
| Second FOOT SR 60 Indian River County Line Polk County Line Polk County Line 240 430 740 1,480 2019 N/A N/ | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature Sign | | | | | | | | | | | | | | | | | | | | | | | | | |
| Second S | | | | | | | | | | | 2021 | | | | 5,527 | 233 | 295 | | SB/WB | 0.094 | | 295 | | | 0.64 |
| 307 OC Thacker Ave Oscoela Pkwy John Young Pkwy 1,400 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1,760 1, | | | | | | Harococco Ha (OH 10) | | | | | 2021 | | | | 5,301 | 232 | 313 | | SB/WB | 0.101 | | 313 | _ | | |
| 911 OC US 17/92 Pleasant Hill Rd Portage St 1,560 1,890 1,960 1,960 2021 4/7 15 65,389 65,389 2240 2298 4,538 SB/WB 0,069 0,51 2,298 F 1,960 1,177 2000 1,979 Portage St Emmett St US 192-441 2,400 2,800 2,940 2,940 2,940 2,020 N/A N/A N/A 49,023 N/A | | | | | | | | | | | | | | | | | | | | | | | | | |
| Portage St Emmet St 1,560 1,890 1,960 1,960 2,000 2,940 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,240 2,24 | | | | | | | | | | | | | | | | | | | | | | | | | 1.17 |
| 920314 FDOT* US 17/92 (S Orange Blossom Tr) Polk County Line Osceola Polk Line Rd (CR 532) 510 820 880 880 2019 N/A N/A N/A 16,400 N/A N | | FDC | OT | US 17/92 | Portage St | Emmett St | 1,560 | 1,890 | 1,960 | 1,960 | 2020 | N/A | N/A | N/A | 49,023 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | | 1,960 | NA |
| 914 OC US 17/92 (S Orange Blossom Tr) Oscola Polk Line Rd (CR 532) Old Tampa Hwy Foliociana Blvd 510 820 880 880 2021 3/23 13 3,041 3,0632 1024 1186 2,210 SB/WB 0,071 0,554 1,186 F 880 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 1,23 | 319 | 00 | C | US 17/92 | | | | | | | | | | | | | | | | | | | В | | 0.63 |
| 914 OC US 17/92 (\$ Orange Blossom Tr) Old Tampa Hwy Poinciana Blvd 510 820 880 880 2021 4/6 15 27,331 27,331 876 1085 1,961 \$SBWB 0.072 0.55 1,085 F 880 1.23 92 OC US 17/92 (\$ Orange Blossom Tr) Poinciana Blvd Ham Brown Rd 510 820 880 880 2021 4/1 14 17,438 17,438 881 931 1,812 \$SBWB 0.104 0.51 931 F 880 1.06 92 OC US 17/92 (\$ Orange Blossom Tr) Ham Brown Rd Pleasant Hill Rd 11,560 1,890 1,960 1,960 2021 3/9 11 31,971 31,332 1049 1071 2,120 \$SBWB 0.066 0.51 1,071 B 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 1,980 | | FDO | OT* | US 17/92 (S Orange Blossom Tr) | | | | | | | | | | | | | | | | | | | | | NA 4.05 |
| 922 OC US 17/92 (\$ Orange Blossom Tr) Poinciana Blvd Ham Brown Rd 510 820 880 880 2021 4/1 14 17.438 17.438 1881 931 1,812 SB/WB 0.104 0.51 931 F 880 1.06 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05 | | 00 | iC | US 17/92 (S Orange Blossom Tr) | | | | | | | | | | | | | | | | | | | | | |
| 921 OC US 17/92 (S Orange Blossom Tr) Ham Brown Rd Pleasant Hill Rd 1,560 1,890 1,960 2021 3/9 11 31,971 31,332 1049 1071 2,120 SB/WB 0.066 0.51 1,071 B 1,960 0.55 750020 FDOT* US 192 Lake County Line SR 429 (Western Beltway) 0 2,080 2,880 2021 9/16 83 73,860 81,785 1945 3309 5,254 SB/WB 0.071 0.63 3,309 F 2,680 NA 9001 Dr 0 2,080 2,880 2,830 2021 9/16 83 73,860 81,785 1945 3309 5,254 SB/WB 0.071 0.63 3,309 F 2,680 NA 9001 Dr 1 0,080 2,880 2,830 2021 9/16 83 73,860 NA | | | | | | | | | | | | | 14 | | | | | | | | | | F | | 1.06 |
| FOOT US 192 Lake County Line SR 429 (Western Beltway) O 2,080 2,680 2,830 2019 N/A N/A N/A N/A 52,000 N/A | 921 | 00 | C | US 17/92 (S Orange Blossom Tr) | Ham Brown Rd | Pleasant Hill Rd | 1,560 | 1,890 | 1,960 | 1,960 | 2021 | 3/9 | 11 | 31,971 | 31,332 | 1049 | 1071 | 2,120 | SB/WB | 0.066 | 0.51 | 1,071 | | 1,960 | 0.55 |
| 202311 FDOT* US 192 World Dr 1-4 3.300 4.580 5.580 6.200 2019 N/A N/A N/A N/A 65.500 N/A | | FDO | OT* | US 192 | Lake County Line | | 0 | 2,080 | 2,680 | 2,830 | | | N/A | N/A | 52,000 | | N/A | N/A | N/A | N/A | N/A | | | | NA |
| 920300 FDOT* US 192 I-4 Parkway Blvd/Celebration Pl 0 2,080 2,680 2,830 2019 N/A | | | | | | World Dr | | | | | | | | | | | | | | | | | | | 1.23 |
| 902 OC US 192 Parkway Blvd/Celebration Pl Polynesian Isle Blvd 0 2,080 2,680 2,830 2021 10/7 41 51,082 54,147 2095 1585 3,680 NB/EB 0.072 0.57 2,095 D 2,680 0.78 | | | | | | Parkway Blyd/Celebration PI | | | | | | | | | | | | | | | | | | | |
| | | | | | | Polynesian Isle Blvd | | | | | | | | | | | | | | | | | | | 0.78 |
| | | | | | | | | | | | | | | | | | | | | | | | | | NA |

2021 Roadway Network Capacity Report (Updated 12/15/2021)

| | | | | | | | | /15/2021 |) | | | | | | | | | | | | | | |
|---------|--------|----------------------------------------|---------------------------------------|---------------------------------------|-------|----------|-----------|----------|--------|------------|------|--------|--------|-------|-------|-------|--------|-----------|----------|---------------|-----|----------|------|
| Count | | | | | Adju | sted Ser | vice Volu | ımes | Latest | | | | 1 | | | | | PM Peak F | lour | | | | |
| Station | Count | ROADWAY | FROM | то | | | | | Count | Count Date | Week | ADT | AADT | | | Pk Hr | | | | Pk Hr | 1 | 1 | |
| # | Source | ROADNAT | TROM | 10 | В | C | D | E | Year | (mm/dd) | HOOK | ADI | AADI | NB/EB | SB/WB | Total | Pk Dir | K-Factor | D-Factor | Pk Dir Vol | LOS | Capacity | V/C |
| 904 | OC | US 192 | Vineland Rd (SR 535) | Siesta Lago Dr | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 10/14 | 42 | 55,728 | 57,957 | 1948 | 2019 | 3,967 | SB/WB | 0.071 | 0.51 | 2,019 | В | 2,940 | 0.69 |
| 913 | OC | US 192 | Siesta Lago Dr | Hoagland Blvd | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 4/22 | 17 | 67,034 | 67,704 | 2163 | 2301 | 4,464 | SB/WB | 0.067 | 0.52 | 2,301 | В | 2,940 | 0.78 |
| 905 | OC | US 192 | Hoagland Blvd | Thacker Ave | 0 | 2,080 | 2,680 | 2,830 | 2021 | 3/2 | 10 | 42,919 | 42,490 | 1427 | 1604 | 3,031 | SB/WB | 0.071 | 0.53 | 1,604 | С | 2,680 | 0.60 |
| 925016 | FDOT | US 192 | Thacker Ave | Main St/US 441-17/92 | 0 | 2,080 | 2,680 | 2,830 | 2020 | N/A | N/A | N/A | 43,076 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,680 | NA |
| 921008 | FDOT | US 192 | US 441/SR 15/Holopaw Rd | Brevard County Line | 1,410 | 2,210 | 2,800 | 3,180 | 2020 | N/A | N/A | N/A | 10,429 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,210 | NA |
| 925017 | FDOT* | US 192-441 | Main St/US 441-17/92 | Michigan Ave/Oak St | 2,400 | 2,860 | 2,940 | 2,940 | 2019 | N/A | N/A | N/A | 40,500 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,940 | NA |
| 906 | oc | US 192-441 | Michigan Ave/Oak St | Fortune Rd | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 3/2 | 10 | 60,961 | 60,351 | 2441 | 1955 | 4,396 | NB/EB | 0.072 | 0.56 | 2,441 | С | 2,940 | 0.83 |
| 907 | OC | US 192-441 | Fortune Rd | Shady Ln/Fla Turnpike | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 3/9 | 11 | 40,927 | 40,108 | 1528 | 1819 | 3,347 | SB/WB | 0.082 | 0.54 | 1,819 | В | 2,940 | 0.62 |
| 908 | OC | US 192-441 | Shady Ln/Fla Turnpike | Partin Settlement Rd | 0 | 2,080 | 2,680 | 2,830 | 2021 | 3/9 | 11 | 62,637 | 61,384 | 2052 | 2390 | 4,442 | SB/WB | 0.071 | 0.54 | 2,390 | D | 2,680 | 0.89 |
| 925 | OC | US 192-441 | Partin Settlement Rd | Commerce Center Dr | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 4/6 | 15 | 53,769 | 53,769 | 1590 | 2409 | 3,999 | SB/WB | 0.074 | 0.60 | 2,409 | С | 2,940 | 0.82 |
| 920105 | FDOT | US 192-441 | Commerce Center Dr | Columbia Ave/Budinger Ave | 0 | 2,080 | 2,680 | 2,830 | 2020 | N/A | N/A | N/A | 45,110 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,680 | NA |
| 925021 | FDOT* | US 192-441 | Columbia Ave/Budinger Ave | Mississippi Ave | 0 | 2,080 | 2,680 | 2,830 | 2019 | N/A | N/A | N/A | 40,000 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,680 | NA |
| 927 | OC | US 192-441 | Mississippi Ave | Narcoossee Rd (CR 15)/Hickory Tree Rd | 0 | 2,080 | 2,680 | 2,830 | 2021 | 4/1 | 14 | 42,032 | 42,032 | 1582 | 1550 | 3,132 | NB/EB | 0.075 | 0.51 | 1,582 | С | 2,680 | 0.59 |
| 920255 | FDOT* | US 192-441 | Narcoossee Rd (CR 15)/Hickory Tree Rd | Nova Rd (CR 532) | 2,660 | 3,840 | 4,980 | 5,650 | 2019 | N/A | N/A | N/A | 30,000 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 4,980 | NA |
| 909 | OC | US 192-441 | Nova Rd (CR 532) | Old Melbourne Hwy | 1,770 | 2,560 | 3,320 | 3,760 | 2021 | 3/9 | 11 | 25,782 | 25,266 | 1041 | 955 | 1,996 | NB/EB | 0.077 | 0.52 | 1,041 | В | 3,320 | 0.31 |
| 920304 | FDOT* | US 192-441 | Old Melbourne Hwy | US 441/SR 15/Holopaw Rd | 1,670 | 2,420 | 3,130 | 3,550 | 2019 | N/A | N/A | N/A | 16,800 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 2,420 | NA |
| 920044 | FDOT* | US 441/SR 15/Kenansville Rd | SR 60 | Canoe Creek Rd/CR 523 | 240 | 430 | 740 | 1,480 | 2019 | N/A | N/A | N/A | 1,600 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 430 | NA |
| 921006 | FDOT* | US 441/SR 15/Kenansville Rd/Holopaw Rd | Canoe Creek Rd/CR 523 | US 192 | 240 | 430 | 740 | 1,480 | 2019 | N/A | N/A | N/A | 2,700 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 430 | NA |
| 920100 | FDOT* | US 441-17/92 (N Orange Blossom Tr) | Donegan Ave | Carroll St | 1,560 | 1,890 | 1,960 | 1,960 | 2019 | N/A | N/A | N/A | 37,500 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 1,960 | NA |
| 912 | oc | US 441-17/92 (N Orange Blossom Tr) | Carroll St | Osceola Pkwy | 1,560 | 1,890 | 1,960 | 1,960 | 2021 | 3/3 | 10 | 41,186 | 40,774 | 1444 | 1730 | 3,174 | SB/WB | 0.077 | 0.55 | 1,730 | С | 1,960 | 0.88 |
| 916 | oc | US 441-17/92 (N Orange Blossom Tr) | Osceola Pkwy | Orange County Line | 2,400 | 2,860 | 2,940 | 2,940 | 2021 | 3/2 | 10 | 35,831 | 35,473 | 1339 | 1746 | 3,085 | SB/WB | 0.086 | 0.57 | 1,746 | В | 2,940 | 0.59 |
| 1004 | oc | Vermont Ave | US 192-441 | Lakeshore Blvd | 270 | 430 | 460 | 460 | 2021 | 9/29 | 40 | 2,087 | 2,254 | 106 | 78 | 184 | NB/EB | 0.088 | 0.58 | 106 | В | 460 | 0.23 |
| NA7 | oc | Westside Blvd | Armadillo Ave | Goodman Road | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 10/28 | 44 | 4,357 | 4,488 | 157 | 174 | 331 | SB/WB | 0.076 | 0.53 | 174 | В | 1,760 | 0.10 |
| NA6 | oc | Westside Blvd | Florence Villa Grove Rd | Funie Steed Rd | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 9/16 | 38 | 16,426 | 18,233 | 727 | 890 | 1,617 | SB/WB | 0.098 | 0.55 | 890 | В | 1,760 | 0.51 |
| NA5 | oc | Westside Blvd | Funie Steed Rd | US 192 | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 10/21 | 43 | 13,297 | 13,829 | 491 | 739 | 1,230 | SB/WB | 0.093 | 0.60 | 739 | В | 1,760 | 0.42 |
| 124 | oc | World Dr | 1-4 | US 192 | 1,400 | 1,700 | 1,760 | 1,760 | 2021 | 10/21 | 43 | 17,255 | 17,945 | 593 | 900 | 1,493 | SB/WB | 0.087 | 0.60 | 900 | В | 1,760 | 0.51 |
| 114 | oc | World Dr | US 192 | Osceola Pkwy | 3,300 | 4,580 | 5,580 | 6,200 | 2021 | 9/16 | 38 | 24,762 | 27,486 | 639 | 1134 | 1,773 | SB/WB | 0.072 | 0.64 | 1,134 | В | 5,580 | 0.20 |
| 1005 | oc | Zuni Rd | Jack Brack Rd | Cyrils Dr | 460 | 740 | 790 | 790 | 2021 | 9/30 | 40 | 2,890 | 3,121 | 78 | 314 | 392 | SB/WB | 0.136 | 0.80 | 314 | В | 790 | 0.40 |
| 2022 | oc | Deer Park Rd | US 192 | Gator Branch Rd | 240 | 430 | 740 | 1,480 | 2021 | 4/1 | 14 | 772 | 772 | 33 | 42 | 75 | SB/WB | 0.097 | 0.56 | 42 | В | 430 | 0.10 |
| 2021 | OC | Deer Park Rd | Gator Branch Rd | Nova Rd (CR 532) | 240 | 430 | 740 | 1,480 | 2021 | 4/1 | 14 | 558 | 558 | 34 | 25 | 59 | NB/EB | 0.106 | 0.58 | 34 | В | 430 | 0.08 |
| 2023 | OC | Laurel Ave | KOA St | Marigold Ave | 400 | 800 | 1,140 | 1,440 | 2021 | 4/6 | 15 | 1,344 | 1,344 | 50 | 81 | 131 | SB/WB | 0.097 | 0.62 | 81 | В | 1,140 | 0.07 |
| 2024 | OC | Broad St | US 17/92 | Old Tampa Hwy | 0 | 500 | 730 | 770 | 2021 | 4/6 | 15 | 6,343 | 6,343 | 156 | 361 | 517 | SB/WB | 0.082 | 0.70 | 361 | С | 730 | 0.49 |
| 2025 | oc | Cross Prairie Pkwy | Neptune Rd | Partin Settlement Rd | 0 | 1,140 | 1,510 | 1,600 | 2021 | 4/1 | 14 | 7,752 | 7,752 | 254 | 340 | 594 | SB/WB | 0.077 | 0.57 | 340 | С | 1,510 | 0.23 |
| 2026 | OC | Westside Blvd | Polk County Line | Oasis Club Blvd./Olympic Club Blvd | 0 | 500 | 730 | 770 | 2021 | 10/21 | 43 | 4,096 | 4,260 | 215 | 175 | 390 | NB/EB | 0.095 | 0.55 | 215 | С | 730 | 0.29 |

FDOT Stations - 2020 AADT obtained from 2020 FTO; 2021 AADT is determined by multiplying corresponding SF with 2021 ADT. *2019 volumes were used for some FDOT stations due to the effect of COVID-19 on 2020 volumes.

APPENDIX F

Synchro Outputs

| Intersection | | | | | | | |
|------------------------------|----------|--------------|-----------|-----------|--------------|----------|--------------|
| Int Delay, s/veh | 0 | | | | | | |
| | | EDT | WELL | WOT | MDD | CDI | CDD |
| Movement Configurations | EBL | EBT | WBU | WBT | WBR | SBL | SBR |
| Lane Configurations | <u>ነ</u> | ↑ | 1 | 4 | 1.4.4 | أ | 0 |
| Traffic Vol. veh/h | 0 | 0 | 1 | 0 | 144 | 93 | 0 |
| Future Vol, veh/h | 0 | 0 | 1 0 | 0 | 144 0 | 93 | 0 |
| Conflicting Peds, #/hr | | | | | | | |
| Sign Control RT Channelized | Stop | Stop None | Free - | Free - | Free None | Free - | Free None |
| | 0 | none - | | | | | |
| Storage Length | | 0 | - | 0 | - | 0 | - |
| Veh in Median Storage | | | - | | - | | - |
| Grade, % Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| | | 90 | 90 | | | | |
| Heavy Vehicles, % Mvmt Flow | 0 | 0 | 1 | 0 | 160 | 103 | 0 |
| IVIVIIIL FIOW | U | U | I | U | 160 | 103 | U |
| | | | | | | | |
| Major/Minor N | /linor2 | <u> </u> | Major2 | | | | |
| Conflicting Flow All | 80 | 82 | - | - | 0 | | |
| Stage 1 | 80 | 82 | - | - | - | | |
| Stage 2 | 0 | 0 | - | - | - | | |
| Critical Hdwy | 6.4 | 6.5 | - | - | - | | |
| Critical Hdwy Stg 1 | 5.4 | 5.5 | - | - | - | | |
| Critical Hdwy Stg 2 | - | - | - | - | - | | |
| Follow-up Hdwy | 3.5 | 4 | - | - | - | | |
| Pot Cap-1 Maneuver | 927 | 812 | - | - | - | | |
| Stage 1 | 948 | 831 | - | - | - | | |
| Stage 2 | - | - | - | - | - | | |
| Platoon blocked, % | | | | - | - | | |
| Mov Cap-1 Maneuver | 927 | 0 | - | - | - | | |
| Mov Cap-2 Maneuver | 927 | 0 | - | - | - | | |
| Stage 1 | 948 | 0 | - | - | - | | |
| Stage 2 | - | 0 | - | - | - | | |
| | | | | | | | |
| Approach | EB | | WB | | | | |
| | | | WD | | | | |
| HCM Control Delay, s | 0 | | | | | | |
| HCM LOS | Α | | | | | | |
| | | | | | | | |
| Minor Lane/Major Mvm | t I | EBLn1 E | EBLn2 | WBT | WBR | | |
| Capacity (veh/h) | | - | - | - | - | | |
| HCM Lane V/C Ratio | | - | - | - | - | | |
| HCM Control Delay (s) | | 0 | 0 | - | - | | |
| HCM Lane LOS | | A | A | - | - | | |
| HCM 95th %tile Q(veh) | | - | - | - | - | | |

| Intersection | | | | | | |
|------------------------|-----------|-------|--------|-------|----------|--------|
| Int Delay, s/veh | 9.8 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ¥ | | | 4 | <u>₽</u> | JJIV |
| Traffic Vol, veh/h | 59 | 291 | 193 | 118 | 60 | 32 |
| Future Vol, veh/h | 59 | 291 | 193 | 118 | 60 | 32 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - - | None | - | None | - | None |
| Storage Length | 0 | - | _ | - | _ | TVOTIC |
| Veh in Median Storage | | | _ | 0 | 0 | _ |
| Grade, % | 0 | - | - | 0 | 0 | - |
| | 82 | 82 | 82 | 82 | 82 | 82 |
| Peak Hour Factor | | | | | | |
| Heavy Vehicles, % | 5 | 1 | 3 | 4 | 2 | 6 |
| Mvmt Flow | 72 | 355 | 235 | 144 | 73 | 39 |
| | | | | | | |
| Major/Minor N | Minor2 | ı | Major1 | N | /lajor2 | |
| Conflicting Flow All | 707 | 93 | 112 | 0 | - | 0 |
| Stage 1 | 93 | - | - | - | _ | - |
| Stage 2 | 614 | - | - | - | _ | - |
| Critical Hdwy | 6.45 | 6.21 | 4.13 | - | _ | - |
| Critical Hdwy Stg 1 | 5.45 | - | - | _ | - | _ |
| Critical Hdwy Stg 2 | 5.45 | _ | _ | _ | _ | _ |
| Follow-up Hdwy | | 3.309 | 2 227 | _ | _ | _ |
| Pot Cap-1 Maneuver | 397 | 967 | 1471 | - | _ | - |
| Stage 1 | 923 | - | | _ | _ | _ |
| Stage 2 | 534 | | | | | _ |
| Platoon blocked, % | 334 | - | - | - | | |
| Mov Cap-1 Maneuver | 328 | 967 | 1471 | - | - | - |
| | 328 | 907 | 14/1 | - | - | _ |
| Mov Cap-2 Maneuver | | - | - | - | - | |
| Stage 1 | 762 | - | - | - | - | - |
| Stage 2 | 534 | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 16.7 | | 4.9 | | 0 | |
| HCM LOS | С | | | | - | |
| | | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | <u>nt</u> | NBL | NBT | EBLn1 | SBT | SBR |
| Capacity (veh/h) | | 1471 | - | 728 | - | - |
| HCM Lane V/C Ratio | | 0.16 | - | 0.586 | - | - |
| HCM Control Delay (s) | | 7.9 | 0 | 16.7 | - | - |
| HCM Lane LOS | | Α | Α | С | - | - |
| HCM 95th %tile Q(veh) |) | 0.6 | - | 3.9 | - | - |
| <u> </u> | | | | | | |

| Intersection | | | | | | | |
|------------------------|----------|----------|--------|------|------|------|------|
| Int Delay, s/veh | 0 | | | | | | |
| | | | | == | | | |
| Movement | EBL | EBT | WBU | WBT | WBR | SBL | SBR |
| Lane Configurations | | | | 4 | | ሻ | |
| Traffic Vol, veh/h | 0 | 0 | 1 | 0 | 132 | 212 | 0 |
| Future Vol, veh/h | 0 | 0 | 1 | 0 | 132 | 212 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | _ 0 | _ 0 | _ 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free | Free |
| RT Channelized | - | None | - | - | None | - | None |
| Storage Length | 0 | - | - | - | - | 0 | - |
| Veh in Median Storage, | # - | 0 | - | 0 | - | 0 | - |
| Grade, % | - | 0 | - | 0 | - | 0 | - |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 5 | 5 | 0 |
| Mvmt Flow | 0 | 0 | 1 | 0 | 145 | 233 | 0 |
| | | | | | | | |
| Major/Minor M | linor2 | | Major2 | | | | |
| | | 75 | | | ^ | | |
| Conflicting Flow All | 73 73 | 75 75 | - | - | 0 | | |
| Stage 1 | 0 | 0 | - | - | - | | |
| Stage 2 | 6.4 | 6.5 | - | - | - | | |
| Critical Hdwy | 5.4 | 5.5 | - | - | - | | |
| Critical Hdwy Stg 1 | | | - | - | - | | |
| Critical Hdwy Stg 2 | - 2 E | - | - | - | - | | |
| Follow-up Hdwy | 3.5 | 4 | - | - | - | | |
| Pot Cap-1 Maneuver | 936 | 819 | - | - | - | | |
| Stage 1 | 955 | 836 | - | - | - | | |
| Stage 2 | - | - | - | - | - | | |
| Platoon blocked, % | 001 | | | - | - | | |
| Mov Cap-1 Maneuver | 936 | 0 | - | - | - | | |
| Mov Cap-2 Maneuver | 936 | 0 | - | - | - | | |
| Stage 1 | 955 | 0 | - | - | - | | |
| Stage 2 | - | 0 | - | - | - | | |
| | | | | | | | |
| Approach | EB | | WB | | | | |
| HCM Control Delay, s | 0 | | **** | | | | |
| HCM LOS | A | | | | | | |
| TIOWI LOS | | | | | | | |
| | | | | | | | |
| Minor Lane/Major Mvmt | | EBLn1 I | EBLn2 | WBT | WBR | | |
| Capacity (veh/h) | | - | - | - | - | | |
| HCM Lane V/C Ratio | | - | - | - | - | | |
| HCM Control Delay (s) | | 0 | 0 | - | - | | |
| HCM Lane LOS | | Α | Α | - | - | | |
| HCM 95th %tile Q(veh) | | - | - | - | - | | |
| HCM 95th %tile Q(veh) | | - | - | - | - | | |

| Intersection | | | | | | |
|------------------------|-----------|-------|--------|-------|------------|------|
| Int Delay, s/veh | 7.5 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ¥ | | | 4 | <u>351</u> | JJIV |
| Traffic Vol, veh/h | 17 | 273 | 210 | 92 | 340 | 114 |
| Future Vol, veh/h | 17 | 273 | 210 | 92 | 340 | 114 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | Jiop - | None | - | None | - | None |
| Storage Length | 0 | - | _ | - | _ | - |
| Veh in Median Storage | | _ | _ | 0 | 0 | _ |
| Grade, % | 0 | - | - | 0 | 0 | - |
| | 90 | 90 | | 90 | 90 | 90 |
| Peak Hour Factor | | | 90 | | | |
| Heavy Vehicles, % | 6 | 1 | 0 | 2 | 0 | 3 |
| Mvmt Flow | 19 | 303 | 233 | 102 | 378 | 127 |
| | | | | | | |
| Major/Minor N | Minor2 | N | Major1 | N | /lajor2 | |
| Conflicting Flow All | 1010 | 442 | 505 | 0 | - | 0 |
| Stage 1 | 442 | _ | _ | - | - | - |
| Stage 2 | 568 | _ | | _ | | _ |
| Critical Hdwy | 6.46 | 6.21 | 4.1 | _ | - | _ |
| Critical Hdwy Stg 1 | 5.46 | - | - | _ | _ | _ |
| Critical Hdwy Stg 2 | 5.46 | _ | _ | _ | _ | _ |
| Follow-up Hdwy | 3.554 | | 2.2 | _ | _ | _ |
| Pot Cap-1 Maneuver | 261 | 618 | 1070 | _ | _ | |
| Stage 1 | 639 | 010 | 1070 | _ | _ | _ |
| Stage 2 | 559 | | | | - | _ |
| Platoon blocked, % | 009 | - | - | - | - | _ |
| | 201 | 410 | 1070 | - | - | |
| Mov Cap-1 Maneuver | 201 | 618 | 1070 | - | | - |
| Mov Cap-2 Maneuver | 201 | - | - | - | - | - |
| Stage 1 | 491 | - | - | - | - | - |
| Stage 2 | 559 | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 20.3 | | 6.5 | | 0 | |
| HCM LOS | C | | 0.0 | | U | |
| TIGINI EOS | U | | | | | |
| | | | | | | |
| Minor Lane/Major Mvm | ıt | NBL | NBT I | EBLn1 | SBT | SBR |
| Capacity (veh/h) | | 1070 | - | 551 | - | - |
| HCM Lane V/C Ratio | | 0.218 | - | 0.585 | - | - |
| HCM Control Delay (s) | | 9.3 | 0 | 20.3 | - | - |
| HCM Lane LOS | | Α | Α | С | - | - |
| HCM 95th %tile Q(veh) |) | 0.8 | - | 3.7 | - | - |
| | | | | | | |

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|----------------------|-------|-------|-------------|-------|-------|
| Lane Group | WBL | WBR | NBT | SBL | SBT |
| Lane Configurations | 7 | 7 | ∱ î≽ | 7 | 44 |
| Traffic Volume (vph) | 25 | 245 | 134 | 153 | 81 |
| Future Volume (vph) | 25 | 245 | 134 | 153 | 81 |
| Turn Type | Prot | Perm | NA | pm+pt | NA |
| Protected Phases | 8 | | 2 | 1 | 6 |
| Permitted Phases | | 8 | | 6 | |
| Detector Phase | 8 | 8 | 2 | 1 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 5.0 | 15.0 |
| Minimum Split (s) | 23.5 | 23.5 | 23.5 | 10.5 | 23.5 |
| Total Split (s) | 42.0 | 42.0 | 38.0 | 20.0 | 58.0 |
| Total Split (%) | 42.0% | 42.0% | 38.0% | 20.0% | 58.0% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | | | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | |
| Recall Mode | None | None | Max | None | Max |

Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 78.5

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Sinclair Rd & Tradition Blvd



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|------------------------------|------|------|----------|----------|----------|----------|------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | ሻ | 7 | ħβ | | ሻ | ^ | |
| Traffic Volume (veh/h) | 25 | 245 | 134 | 26 | 153 | 81 | |
| Future Volume (veh/h) | 25 | 245 | 134 | 26 | 153 | 81 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | No | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1841 | 1870 | 1870 | 1841 | |
| Adj Flow Rate, veh/h | 28 | 272 | 149 | 29 | 170 | 90 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Percent Heavy Veh, % | 2 | 2 | 4 | 2 | 2 | 4 | |
| Cap, veh/h | 360 | 321 | 1532 | 292 | 810 | 2307 | |
| Arrive On Green | 0.20 | 0.20 | 0.52 | 0.52 | 0.07 | 0.66 | |
| Sat Flow, veh/h | 1781 | 1585 | 3023 | 558 | 1781 | 3589 | |
| Grp Volume(v), veh/h | 28 | 272 | 88 | 90 | 170 | 90 | |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1585 | 1749 | 1740 | 1781 | 1749 | |
| Q Serve(g_s), s | 1.0 | 13.2 | 2.0 | 2.1 | 3.2 | 0.7 | |
| Cycle Q Clear(g_c), s | 1.0 | 13.2 | 2.0 | 2.1 | 3.2 | 0.7 | |
| Prop In Lane | 1.00 | 1.00 | | 0.32 | 1.00 | | |
| Lane Grp Cap(c), veh/h | 360 | 321 | 914 | 910 | 810 | 2307 | |
| V/C Ratio(X) | 0.08 | 0.85 | 0.10 | 0.10 | 0.21 | 0.04 | |
| Avail Cap(c_a), veh/h | 817 | 727 | 914 | 910 | 1014 | 2307 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 25.7 | 30.6 | 9.5 | 9.6 | 6.6 | 4.7 | |
| Incr Delay (d2), s/veh | 0.1 | 6.2 | 0.2 | 0.2 | 0.1 | 0.0 | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(95%),veh/ln | 0.8 | 9.2 | 1.3 | 1.4 | 1.9 | 0.4 | |
| Unsig. Movement Delay, s/veh | | | | | | | |
| LnGrp Delay(d),s/veh | 25.8 | 36.8 | 9.7 | 9.8 | 6.8 | 4.8 | |
| LnGrp LOS | С | D | A | A | A | A | |
| Approach Vol, veh/h | 300 | | 178 | | | 260 | |
| Approach Delay, s/veh | 35.8 | | 9.8 | | | 6.1 | |
| Approach LOS | D | | Α | | | Α | |
| Timer - Assigned Phs | 1 | 2 | | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 10.9 | 47.1 | | | | 58.0 | 21.6 |
| Change Period (Y+Rc), s | 5.5 | 5.5 | | | | 5.5 | 5.5 |
| Max Green Setting (Gmax), s | 14.5 | 32.5 | | | | 52.5 | 36.5 |
| Max Q Clear Time (g_c+l1), s | 5.2 | 4.1 | | | | 2.7 | 15.2 |
| Green Ext Time (p_c), s | 0.3 | 1.0 | | | | 0.6 | 1.0 |
| Intersection Summary | | | | | | | |
| HCM 6th Ctrl Delay | | | 19.0 | | | | |
| HCM 6th LOS | | | В | | | | |

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|----------------------|-------|------------|-------|------------|-------|----------|-------|-------|--|
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | |
| Lane Configurations | * | ↑ ↑ | J. | ∱ } | J. | f) | 7 | f) | |
| Traffic Volume (vph) | 88 | 68 | 58 | 32 | 304 | 118 | 20 | 120 | |
| Future Volume (vph) | 88 | 68 | 58 | 32 | 304 | 118 | 20 | 120 | |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 8 | | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 15.0 | 5.0 | 15.0 | 7.0 | 15.0 | 5.0 | 10.0 | |
| Minimum Split (s) | 10.5 | 23.5 | 10.5 | 20.5 | 12.5 | 20.5 | 10.5 | 15.5 | |
| Total Split (s) | 21.0 | 46.0 | 24.0 | 49.0 | 17.0 | 45.0 | 15.0 | 43.0 | |
| Total Split (%) | 16.2% | 35.4% | 18.5% | 37.7% | 13.1% | 34.6% | 11.5% | 33.1% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | Min | None | Min | |

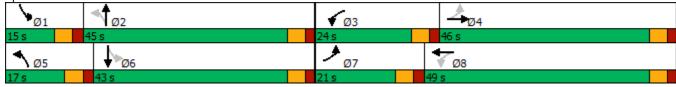
Intersection Summary

Cycle Length: 130

Actuated Cycle Length: 68.8

Natural Cycle: 70





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|------------------------------|------|------------|----------|------|------------|------|----------|----------|-------------|-------------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ∱ ∱ | | 7 | ተ ኈ | | 7 | ₽ | | ሻ | 1> | |
| Traffic Volume (veh/h) | 88 | 68 | 411 | 58 | 32 | 12 | 304 | 118 | 89 | 20 | 120 | 67 |
| Future Volume (veh/h) | 88 | 68 | 411 | 58 | 32 | 12 | 304 | 118 | 89 | 20 | 120 | 67 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1826 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 | 1841 | 1870 | 1870 | 1870 | 1811 |
| Adj Flow Rate, veh/h | 107 | 83 | 501 | 71 | 39 | 15 | 371 | 144 | 109 | 24 | 146 | 82 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Percent Heavy Veh, % | 5 | 2 | 2 | 2 | 2 | 2 | 3 | 4 | 2 | 2 | 2 | 6 |
| Cap, veh/h | 657 | 643 | 573 | 253 | 929 | 338 | 385 | 273 | 207 | 310 | 186 | 104 |
| Arrive On Green | 0.06 | 0.36 | 0.36 | 0.06 | 0.36 | 0.36 | 0.14 | 0.28 | 0.28 | 0.03 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1739 | 1777 | 1585 | 1781 | 2553 | 927 | 1767 | 972 | 736 | 1781 | 1125 | 632 |
| Grp Volume(v), veh/h | 107 | 83 | 501 | 71 | 26 | 28 | 371 | 0 | 253 | 24 | 0 | 228 |
| Grp Sat Flow(s),veh/h/ln | 1739 | 1777 | 1585 | 1781 | 1777 | 1703 | 1767 | 0 | 1708 | 1781 | 0 | 1757 |
| Q Serve(g_s), s | 3.1 | 2.5 | 24.0 | 1.9 | 8.0 | 0.9 | 11.5 | 0.0 | 10.2 | 0.9 | 0.0 | 10.1 |
| Cycle Q Clear(g_c), s | 3.1 | 2.5 | 24.0 | 1.9 | 0.8 | 0.9 | 11.5 | 0.0 | 10.2 | 0.9 | 0.0 | 10.1 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 0.54 | 1.00 | | 0.43 | 1.00 | | 0.36 |
| Lane Grp Cap(c), veh/h | 657 | 643 | 573 | 253 | 647 | 620 | 385 | 0 | 480 | 310 | 0 | 290 |
| V/C Ratio(X) | 0.16 | 0.13 | 0.87 | 0.28 | 0.04 | 0.04 | 0.96 | 0.00 | 0.53 | 0.08 | 0.00 | 0.79 |
| Avail Cap(c_a), veh/h | 886 | 885 | 790 | 549 | 951 | 911 | 385 | 0 | 830 | 472 | 0 | 810 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 14.5 | 17.4 | 24.2 | 18.0 | 16.7 | 16.7 | 26.2 | 0.0 | 24.7 | 27.0 | 0.0 | 32.6 |
| Incr Delay (d2), s/veh | 0.1 | 0.1 | 8.1 | 0.6 | 0.0 | 0.0 | 36.3 | 0.0 | 0.9 | 0.1 | 0.0 | 4.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(95%),veh/ln | 2.1 | 1.8 | 14.6 | 1.4 | 0.6 | 0.6 | 14.6 | 0.0 | 7.2 | 0.7 | 0.0 | 8.0 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 14.7 | 17.5 | 32.3 | 18.6 | 16.7 | 16.7 | 62.5 | 0.0 | 25.6 | 27.1 | 0.0 | 37.3 |
| LnGrp LOS | В | В | <u>C</u> | В | В | В | <u>E</u> | A | <u>C</u> | <u>C</u> | A | <u>D</u> |
| Approach Vol, veh/h | | 691 | | | 125 | | | 624 | | | 252 | |
| Approach Delay, s/veh | | 27.8 | | | 17.8 | | | 47.5 | | | 36.3 | |
| Approach LOS | | С | | | В | | | D | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 7.6 | 28.3 | 10.5 | 34.9 | 17.0 | 18.9 | 10.3 | 35.1 | | | | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | | | | |
| Max Green Setting (Gmax), s | 9.5 | 39.5 | 18.5 | 40.5 | 11.5 | 37.5 | 15.5 | 43.5 | | | | |
| Max Q Clear Time (g_c+l1), s | 2.9 | 12.2 | 3.9 | 26.0 | 13.5 | 12.1 | 5.1 | 2.9 | | | | |
| Green Ext Time (p_c), s | 0.0 | 1.5 | 0.1 | 3.4 | 0.0 | 1.3 | 0.2 | 0.3 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 35.6 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |
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|----------------------|-------|-------|-------------|-------|----------|
| Lane Group | WBL | WBR | NBT | SBL | SBT |
| Lane Configurations | 7 | 7 | ∱ î≽ | 7 | ^ |
| Traffic Volume (vph) | 25 | 148 | 78 | 236 | 130 |
| Future Volume (vph) | 25 | 148 | 78 | 236 | 130 |
| Turn Type | Prot | Perm | NA | pm+pt | NA |
| Protected Phases | 8 | | 2 | 1 | 6 |
| Permitted Phases | | 8 | | 6 | |
| Detector Phase | 8 | 8 | 2 | 1 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 5.0 | 15.0 |
| Minimum Split (s) | 20.5 | 20.5 | 20.5 | 10.5 | 20.5 |
| Total Split (s) | 27.0 | 27.0 | 37.0 | 36.0 | 73.0 |
| Total Split (%) | 27.0% | 27.0% | 37.0% | 36.0% | 73.0% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | | | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | |
| Recall Mode | None | None | Max | None | Max |
| | | | | | |

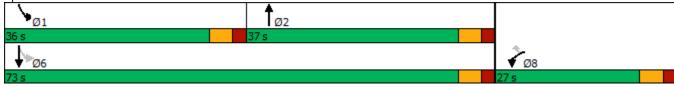
Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 93.5

Natural Cycle: 55





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|------------------------------|------|------|------------|----------|----------|----------|------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | ¥ | 7 | ∱ ⊅ | | Ţ | ^ | |
| Traffic Volume (veh/h) | 25 | 148 | 78 | 24 | 236 | 130 | |
| Future Volume (veh/h) | 25 | 148 | 78 | 24 | 236 | 130 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Work Zone On Approach | No | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1826 | 1870 | 1870 | 1870 | 1826 | |
| Adj Flow Rate, veh/h | 27 | 163 | 86 | 26 | 259 | 143 | |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | |
| Percent Heavy Veh, % | 2 | 5 | 2 | 2 | 2 | 5 | |
| Cap, veh/h | 284 | 247 | 1578 | 459 | 951 | 2507 | |
| Arrive On Green | 0.16 | 0.16 | 0.58 | 0.58 | 0.08 | 0.72 | |
| Sat Flow, veh/h | 1781 | 1547 | 2810 | 789 | 1781 | 3561 | |
| Grp Volume(v), veh/h | 27 | 163 | 55 | 57 | 259 | 143 | |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1547 | 1777 | 1728 | 1781 | 1735 | |
| 2 Serve(g_s), s | 1.2 | 9.2 | 1.3 | 1.3 | 5.0 | 1.1 | |
| Cycle Q Clear(g_c), s | 1.2 | 9.2 | 1.3 | 1.3 | 5.0 | 1.1 | |
| Prop In Lane | 1.00 | 1.00 | | 0.46 | 1.00 | | |
| ane Grp Cap(c), veh/h | 284 | 247 | 1032 | 1004 | 951 | 2507 | |
| I/C Ratio(X) | 0.10 | 0.66 | 0.05 | 0.06 | 0.27 | 0.06 | |
| Avail Cap(c_a), veh/h | 410 | 356 | 1032 | 1004 | 1385 | 2507 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 33.5 | 36.9 | 8.5 | 8.5 | 5.5 | 3.7 | |
| ncr Delay (d2), s/veh | 0.1 | 3.0 | 0.1 | 0.1 | 0.2 | 0.0 | |
| nitial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(95%),veh/ln | 1.0 | 6.6 | 0.9 | 0.9 | 2.9 | 0.6 | |
| Jnsig. Movement Delay, s/veh | | | | | | | |
| LnGrp Delay(d),s/veh | 33.6 | 39.9 | 8.6 | 8.6 | 5.6 | 3.8 | |
| nGrp LOS | С | D | Α | Α | Α | Α | |
| Approach Vol, veh/h | 190 | | 112 | | | 402 | |
| Approach Delay, s/veh | 39.0 | | 8.6 | | | 5.0 | |
| Approach LOS | D | | A | | | A | |
| Timer - Assigned Phs | 1 | 2 | | | | 6 | 8 |
| Phs Duration (G+Y+Rc), s | 13.2 | 59.8 | | | | 73.0 | 20.4 |
| Change Period (Y+Rc), s | 5.5 | 5.5 | | | | 5.5 | 5.5 |
| Max Green Setting (Gmax), s | 30.5 | 31.5 | | | | 67.5 | 21.5 |
| Max Q Clear Time (q_c+l1), s | 7.0 | 3.3 | | | | 3.1 | 11.2 |
| Green Ext Time (p_c), s | 0.7 | 0.6 | | | | 1.0 | 0.4 |
| 4 — <i>7</i> | 0.7 | 0.0 | | | | 1.0 | 0.7 |
| Intersection Summary | | | 447 | | | | |
| HCM 6th Ctrl Delay | | | 14.7 | | | | |
| HCM 6th LOS | | | В | | | | |

2: Goodman Rd & Bella Cita Blvd/Sinclair Rd

| | • | - | • | • | 1 | † | - | ţ | |
|----------------------|-------|------------|-------|------------|-------|----------|-------|-------|--|
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT | |
| Lane Configurations | 7 | ∱ } | ¥ | ∱ } | ¥ | f) | 7 | f) | |
| Traffic Volume (vph) | 45 | 41 | 76 | 53 | 232 | 42 | 18 | 157 | |
| Future Volume (vph) | 45 | 41 | 76 | 53 | 232 | 42 | 18 | 157 | |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 8 | | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 15.0 | 5.0 | 15.0 | 7.0 | 15.0 | 5.0 | 10.0 | |
| Minimum Split (s) | 10.5 | 23.5 | 23.5 | 23.5 | 12.5 | 20.5 | 10.5 | 23.5 | |
| Total Split (s) | 23.0 | 49.0 | 23.0 | 49.0 | 16.0 | 42.0 | 16.0 | 42.0 | |
| Total Split (%) | 17.7% | 37.7% | 17.7% | 37.7% | 12.3% | 32.3% | 12.3% | 32.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | Min | None | Min | |

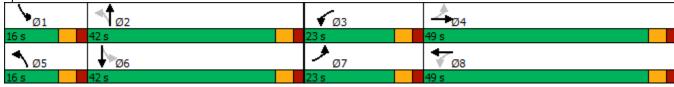
Intersection Summary

Cycle Length: 130

Actuated Cycle Length: 69.5

Natural Cycle: 85





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|------------------------------|------|------------|------|----------|------------|------|----------|------|------|-------------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | × | ∱ ∱ | | 7 | ∱ ∱ | | 7 | 4î | | 7 | f) | |
| Traffic Volume (veh/h) | 45 | 41 | 351 | 76 | 53 | 10 | 232 | 42 | 39 | 18 | 157 | 109 |
| Future Volume (veh/h) | 45 | 41 | 351 | 76 | 53 | 10 | 232 | 42 | 39 | 18 | 157 | 109 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1811 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 |
| Adj Flow Rate, veh/h | 50 | 46 | 390 | 84 | 59 | 11 | 258 | 47 | 43 | 20 | 174 | 121 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 |
| Cap, veh/h | 553 | 528 | 471 | 277 | 960 | 174 | 388 | 289 | 265 | 413 | 217 | 151 |
| Arrive On Green | 0.04 | 0.30 | 0.30 | 0.07 | 0.32 | 0.32 | 0.13 | 0.32 | 0.32 | 0.02 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1725 | 1777 | 1585 | 1781 | 3004 | 545 | 1781 | 899 | 823 | 1781 | 1027 | 714 |
| Grp Volume(v), veh/h | 50 | 46 | 390 | 84 | 34 | 36 | 258 | 0 | 90 | 20 | 0 | 295 |
| Grp Sat Flow(s), veh/h/ln | 1725 | 1777 | 1585 | 1781 | 1777 | 1772 | 1781 | 0 | 1722 | 1781 | 0 | 1742 |
| Q Serve(g_s), s | 1.5 | 1.4 | 17.2 | 2.4 | 1.0 | 1.1 | 8.0 | 0.0 | 2.8 | 0.7 | 0.0 | 12.1 |
| Cycle Q Clear(g_c), s | 1.5 | 1.4 | 17.2 | 2.4 | 1.0 | 1.1 | 8.0 | 0.0 | 2.8 | 0.7 | 0.0 | 12.1 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 0.31 | 1.00 | | 0.48 | 1.00 | | 0.41 |
| Lane Grp Cap(c), veh/h | 553 | 528 | 471 | 277 | 568 | 566 | 388 | 0 | 554 | 413 | 0 | 368 |
| V/C Ratio(X) | 0.09 | 0.09 | 0.83 | 0.30 | 0.06 | 0.06 | 0.67 | 0.00 | 0.16 | 0.05 | 0.00 | 0.80 |
| Avail Cap(c_a), veh/h | 880 | 1029 | 918 | 575 | 1029 | 1026 | 400 | 0 | 837 | 621 | 0 | 846 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 16.8 | 19.1 | 24.6 | 18.2 | 17.7 | 17.8 | 19.1 | 0.0 | 18.2 | 22.3 | 0.0 | 28.1 |
| Incr Delay (d2), s/veh | 0.1 | 0.1 | 3.8 | 0.6 | 0.0 | 0.0 | 4.0 | 0.0 | 0.1 | 0.0 | 0.0 | 4.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(95%),veh/ln | 1.0 | 1.0 | 10.8 | 1.7 | 0.7 | 0.8 | 6.3 | 0.0 | 2.0 | 0.5 | 0.0 | 9.0 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | 22.0 |
| LnGrp Delay(d),s/veh | 16.9 | 19.1 | 28.4 | 18.8 | 17.8 | 17.8 | 23.1 | 0.0 | 18.4 | 22.3 | 0.0 | 32.2 |
| LnGrp LOS | В | В | С | В | В | В | <u>C</u> | A | В | С | A | <u>C</u> |
| Approach Vol, veh/h | | 486 | | | 154 | | | 348 | | | 315 | |
| Approach Delay, s/veh | | 26.4 | | | 18.3 | | | 21.9 | | | 31.6 | |
| Approach LOS | | С | | | В | | | С | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 7.2 | 29.7 | 10.4 | 27.8 | 15.5 | 21.4 | 8.7 | 29.5 | | | | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | | | | |
| Max Green Setting (Gmax), s | 10.5 | 36.5 | 17.5 | 43.5 | 10.5 | 36.5 | 17.5 | 43.5 | | | | |
| Max Q Clear Time (g_c+l1), s | 2.7 | 4.8 | 4.4 | 19.2 | 10.0 | 14.1 | 3.5 | 3.1 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.5 | 0.1 | 3.1 | 0.0 | 1.8 | 0.1 | 0.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 25.5 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|----------------------|-------|-------|-------------|-------|-------|
| Lane Group | WBL | WBR | NBT | SBL | SBT |
| Lane Configurations | ሻ | 7 | ∱ î≽ | 7 | 44 |
| Traffic Volume (vph) | 158 | 501 | 809 | 295 | 495 |
| Future Volume (vph) | 158 | 501 | 809 | 295 | 495 |
| Turn Type | Prot | Perm | NA | pm+pt | NA |
| Protected Phases | 8 | | 2 | 1 | 6 |
| Permitted Phases | | 8 | | 6 | |
| Detector Phase | 8 | 8 | 2 | 1 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 5.0 | 15.0 |
| Minimum Split (s) | 23.5 | 23.5 | 23.5 | 10.5 | 23.5 |
| Total Split (s) | 42.0 | 42.0 | 38.0 | 20.0 | 58.0 |
| Total Split (%) | 42.0% | 42.0% | 38.0% | 20.0% | 58.0% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | | | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | |
| Recall Mode | None | None | Max | None | Max |

Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 85.8

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Sinclair Rd & Tradition Blvd



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|------------------------------|------|----------|------------|----------|----------|----------|------|--|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | | |
| Lane Configurations | ች | 7 | † % | | * | ^ | | |
| Traffic Volume (veh/h) | 158 | 501 | 809 | 152 | 295 | 495 | | |
| Future Volume (veh/h) | 158 | 501 | 809 | 152 | 295 | 495 | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Work Zone On Approach | No | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1841 | 1870 | 1870 | 1841 | | |
| Adj Flow Rate, veh/h | 176 | 557 | 899 | 169 | 328 | 550 | | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | | |
| Percent Heavy Veh, % | 2 | 2 | 4 | 2 | 2 | 4 | | |
| Cap, veh/h | 649 | 578 | 955 | 180 | 345 | 1837 | | |
| Arrive On Green | 0.36 | 0.36 | 0.33 | 0.33 | 0.15 | 0.53 | | |
| Sat Flow, veh/h | 1781 | 1585 | 3030 | 552 | 1781 | 3589 | | |
| Grp Volume(v), veh/h | 176 | 557 | 535 | 533 | 328 | 550 | | |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1585 | 1749 | 1741 | 1781 | 1749 | | |
| Q Serve(g_s), s | 7.0 | 34.4 | 29.7 | 29.7 | 13.3 | 8.9 | | |
| Cycle Q Clear(g_c), s | 7.0 | 34.4 | 29.7 | 29.7 | 13.3 | 8.9 | | |
| Prop In Lane | 1.00 | 1.00 | | 0.32 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 649 | 578 | 569 | 566 | 345 | 1837 | | |
| V/C Ratio(X) | 0.27 | 0.96 | 0.94 | 0.94 | 0.95 | 0.30 | | |
| Avail Cap(c_a), veh/h | 651 | 579 | 569 | 566 | 345 | 1837 | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Uniform Delay (d), s/veh | 22.4 | 31.1 | 32.8 | 32.8 | 27.0 | 13.4 | | |
| Incr Delay (d2), s/veh | 0.2 | 28.4 | 25.6 | 25.8 | 35.6 | 0.4 | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| %ile BackOfQ(95%),veh/ln | 5.3 | 24.0 | 22.7 | 22.6 | 12.4 | 6.1 | | |
| Unsig. Movement Delay, s/veh | | F6 - | F.C. 1 | F.C. (| 16.1 | 46.5 | | |
| LnGrp Delay(d),s/veh | 22.6 | 59.5 | 58.4 | 58.6 | 62.6 | 13.8 | | |
| LnGrp LOS | С | <u>E</u> | <u>E</u> | E | E | В | | |
| Approach Vol, veh/h | 733 | | 1068 | | | 878 | | |
| Approach Delay, s/veh | 50.7 | | 58.5 | | | 32.0 | | |
| Approach LOS | D | | Е | | | С | | |
| Timer - Assigned Phs | 1 | 2 | | | | 6 | 8 | |
| Phs Duration (G+Y+Rc), s | 20.0 | 38.0 | | | | 58.0 | 41.9 | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | | | | 5.5 | 5.5 | |
| Max Green Setting (Gmax), s | 14.5 | 32.5 | | | | 52.5 | 36.5 | |
| Max Q Clear Time (g_c+l1), s | 15.3 | 31.7 | | | | 10.9 | 36.4 | |
| Green Ext Time (p_c), s | 0.0 | 0.5 | | | | 4.0 | 0.0 | |
| Intersection Summary | | | | | | | | |
| HCM 6th Ctrl Delay | | | 47.7 | | | | | |
| HCM 6th LOS | | | 47.7 D | | | | | |
| HOW UIT LOS | | | U | | | | | |

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|----------------------|-------|---------------|-------|-------------|-------|----------|-------|-------|
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Configurations | 7 | ∱ î≽ | 7 | ∱ î≽ | ሻ | f) | ሻ | f) |
| Traffic Volume (vph) | 89 | 511 | 263 | 281 | 240 | 59 | 98 | 63 |
| Future Volume (vph) | 89 | 511 | 263 | 281 | 240 | 59 | 98 | 63 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 8 | | 2 | | 6 | |
| Detector Phase | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 15.0 | 5.0 | 15.0 | 7.0 | 15.0 | 5.0 | 10.0 |
| Minimum Split (s) | 10.5 | 23.5 | 10.5 | 20.5 | 12.5 | 20.5 | 10.5 | 15.5 |
| Total Split (s) | 24.0 | 48.0 | 27.0 | 51.0 | 17.0 | 48.0 | 12.0 | 43.0 |
| Total Split (%) | 17.8% | 35.6% | 20.0% | 37.8% | 12.6% | 35.6% | 8.9% | 31.9% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min |

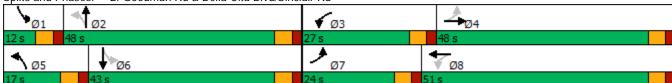
Intersection Summary

Cycle Length: 135

Actuated Cycle Length: 115.6

Natural Cycle: 75





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|------------------------------|------|------------|----------|----------|------------|------|------|----------|----------|----------|--------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ተ ኈ | | 7 | ∱ ∱ | | 7 | ₽ | | ሻ | ₽ | |
| Traffic Volume (veh/h) | 89 | 511 | 333 | 263 | 281 | 70 | 240 | 59 | 340 | 98 | 63 | 69 |
| Future Volume (veh/h) | 89 | 511 | 333 | 263 | 281 | 70 | 240 | 59 | 340 | 98 | 63 | 69 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1826 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 | 1841 | 1870 | 1870 | 1870 | 1811 |
| Adj Flow Rate, veh/h | 109 | 623 | 406 | 321 | 343 | 85 | 293 | 72 | 415 | 120 | 77 | 84 |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Percent Heavy Veh, % | 5 | 2 | 2 | 2 | 2 | 2 | 3 | 4 | 2 | 2 | 2 | 6 |
| Cap, veh/h | 448 | 649 | 423 | 343 | 1174 | 287 | 452 | 75 | 429 | 154 | 228 | 248 |
| Arrive On Green | 0.06 | 0.31 | 0.31 | 0.16 | 0.41 | 0.41 | 0.09 | 0.32 | 0.32 | 0.05 | 0.28 | 0.28 |
| Sat Flow, veh/h | 1739 | 2062 | 1343 | 1781 | 2830 | 692 | 1767 | 236 | 1360 | 1781 | 818 | 892 |
| Grp Volume(v), veh/h | 109 | 537 | 492 | 321 | 214 | 214 | 293 | 0 | 487 | 120 | 0 | 161 |
| Grp Sat Flow(s), veh/h/ln | 1739 | 1777 | 1629 | 1781 | 1777 | 1746 | 1767 | 0 | 1596 | 1781 | 0 | 1710 |
| Q Serve(g_s), s | 5.6 | 39.8 | 39.8 | 19.0 | 10.7 | 11.0 | 11.5 | 0.0 | 40.3 | 6.5 | 0.0 | 10.1 |
| Cycle Q Clear(g_c), s | 5.6 | 39.8 | 39.8 | 19.0 | 10.7 | 11.0 | 11.5 | 0.0 | 40.3 | 6.5 | 0.0 | 10.1 |
| Prop In Lane | 1.00 | | 0.82 | 1.00 | | 0.40 | 1.00 | _ | 0.85 | 1.00 | _ | 0.52 |
| Lane Grp Cap(c), veh/h | 448 | 559 | 513 | 343 | 737 | 724 | 452 | 0 | 504 | 154 | 0 | 476 |
| V/C Ratio(X) | 0.24 | 0.96 | 0.96 | 0.93 | 0.29 | 0.30 | 0.65 | 0.00 | 0.97 | 0.78 | 0.00 | 0.34 |
| Avail Cap(c_a), veh/h | 588 | 562 | 516 | 349 | 737 | 724 | 452 | 0 | 505 | 154 | 0 | 478 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 28.2 | 45.2 | 45.2 | 40.2 | 26.1 | 26.2 | 35.3 | 0.0 | 45.2 | 37.8 | 0.0 | 38.6 |
| Incr Delay (d2), s/veh | 0.3 | 27.9 | 29.6 | 31.7 | 0.2 | 0.2 | 3.2 | 0.0 | 31.4 | 22.2 | 0.0 | 0.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(95%),veh/ln | 4.3 | 29.2 | 27.4 | 19.6 | 8.1 | 8.1 | 5.8 | 0.0 | 27.5 | 6.8 | 0.0 | 7.7 |
| Unsig. Movement Delay, s/veh | | 70.1 | 747 | 71.0 | 2/2 | 27.4 | 20.5 | 0.0 | 7/7 | (0.0 | 0.0 | 20.0 |
| LnGrp Delay(d),s/veh | 28.5 | 73.1 | 74.7 | 71.8 | 26.3 | 26.4 | 38.5 | 0.0 | 76.7 | 60.0 | 0.0 | 39.0 |
| LnGrp LOS | С | 1120 | <u>E</u> | <u>E</u> | C | С | D | A | <u>E</u> | <u>E</u> | A 201 | D |
| Approach Vol, veh/h | | 1138 | | | 749 | | | 780 | | | 281 | |
| Approach Delay, s/veh | | 69.5 | | | 45.9 | | | 62.3 | | | 48.0 | |
| Approach LOS | | Ł | | | D | | | Ł | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.0 | 47.9 | 26.6 | 47.8 | 17.0 | 42.9 | 13.2 | 61.2 | | | | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | | | | |
| Max Green Setting (Gmax), s | 6.5 | 42.5 | 21.5 | 42.5 | 11.5 | 37.5 | 18.5 | 45.5 | | | | |
| Max Q Clear Time (g_c+l1), s | 8.5 | 42.3 | 21.0 | 41.8 | 13.5 | 12.1 | 7.6 | 13.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.1 | 0.1 | 0.4 | 0.0 | 0.9 | 0.2 | 2.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 59.6 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |

| | • | • | † | - | ţ |
|----------------------|-------|-------|------------|-------|----------|
| Lane Group | WBL | WBR | NBT | SBL | SBT |
| Lane Configurations | 7 | 7 | ∱ } | J. | ^ |
| Traffic Volume (vph) | 173 | 248 | 440 | 446 | 789 |
| Future Volume (vph) | 173 | 248 | 440 | 446 | 789 |
| Turn Type | Prot | Perm | NA | pm+pt | NA |
| Protected Phases | 8 | | 2 | 1 | 6 |
| Permitted Phases | | 8 | | 6 | |
| Detector Phase | 8 | 8 | 2 | 1 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 15.0 | 5.0 | 15.0 |
| Minimum Split (s) | 20.5 | 20.5 | 20.5 | 10.5 | 20.5 |
| Total Split (s) | 27.0 | 27.0 | 37.0 | 36.0 | 73.0 |
| Total Split (%) | 27.0% | 27.0% | 37.0% | 36.0% | 73.0% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | | | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | |
| Recall Mode | None | None | Max | None | Max |
| | | | | | |

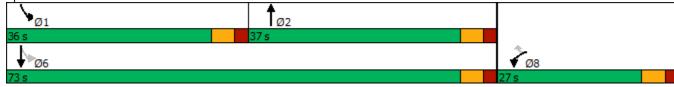
Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 95.4

Natural Cycle: 65





| | • | 4 | † | / | / | ļ | | |
|------------------------------|------|------|------------|----------|----------|----------|----------|--|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | | |
| Lane Configurations | ች | 7 | ∱ } | | ሻ | ^ | | |
| Traffic Volume (veh/h) | 173 | 248 | 440 | 174 | 446 | 789 | | |
| Future Volume (veh/h) | 173 | 248 | 440 | 174 | 446 | 789 | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | | 1.00 | 1.00 | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Work Zone On Approach | No | | No | | | No | | |
| Adj Sat Flow, veh/h/ln | 1870 | 1826 | 1870 | 1870 | 1870 | 1826 | | |
| Adj Flow Rate, veh/h | 190 | 273 | 484 | 191 | 490 | 867 | | |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | | |
| Percent Heavy Veh, % | 2 | 5 | 2 | 2 | 2 | 5 | | |
| Cap, veh/h | 351 | 305 | 1166 | 457 | 629 | 2395 | | |
| Arrive On Green | 0.20 | 0.20 | 0.47 | 0.47 | 0.17 | 0.69 | | |
| Sat Flow, veh/h | 1781 | 1547 | 2587 | 978 | 1781 | 3561 | | |
| Grp Volume(v), veh/h | 190 | 273 | 344 | 331 | 490 | 867 | <u> </u> | |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1547 | 1777 | 1694 | 1781 | 1735 | | |
| Q Serve(g_s), s | 9.4 | 16.8 | 12.5 | 12.6 | 12.8 | 10.1 | | |
| Cycle Q Clear(g_c), s | 9.4 | 16.8 | 12.5 | 12.6 | 12.8 | 10.1 | | |
| Prop In Lane | 1.00 | 1.00 | | 0.58 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 351 | 305 | 831 | 792 | 629 | 2395 | | |
| V/C Ratio(X) | 0.54 | 0.89 | 0.41 | 0.42 | 0.78 | 0.36 | | |
| Avail Cap(c_a), veh/h | 392 | 340 | 831 | 792 | 888 | 2395 | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Uniform Delay (d), s/veh | 35.3 | 38.3 | 17.2 | 17.2 | 11.1 | 6.3 | | |
| Incr Delay (d2), s/veh | 1.3 | 23.2 | 1.5 | 1.6 | 2.9 | 0.4 | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| %ile BackOfQ(95%),veh/ln | 7.5 | 12.9 | 9.1 | 8.8 | 8.5 | 6.0 | | |
| Unsig. Movement Delay, s/veh | | | | | | | | |
| LnGrp Delay(d),s/veh | 36.6 | 61.5 | 18.7 | 18.8 | 14.0 | 6.7 | | |
| LnGrp LOS | D | Е | В | В | В | Α | | |
| Approach Vol, veh/h | 463 | | 675 | | | 1357 | | |
| Approach Delay, s/veh | 51.2 | | 18.8 | | | 9.3 | | |
| Approach LOS | D | | В | | | А | | |
| Timer - Assigned Phs | 1 | 2 | | | | 6 | 8 | |
| Phs Duration (G+Y+Rc), s | 21.8 | 51.2 | | | | 73.0 | 24.8 | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | | | | 5.5 | 5.5 | |
| Max Green Setting (Gmax), s | 30.5 | 31.5 | | | | 67.5 | 21.5 | |
| Max Q Clear Time (q_c+l1), s | 14.8 | 14.6 | | | | 12.1 | 18.8 | |
| Green Ext Time (p_c), s | 1.5 | 4.0 | | | | 7.8 | 0.5 | |
| V = 7: | 1.0 | 7.0 | | | | 7.0 | 0.0 | |
| Intersection Summary | | | 46.7 | | | | | |
| HCM 6th Ctrl Delay | | | 19.7 | | | | | |
| HCM 6th LOS | | | В | | | | | |

2: Goodman Rd & Bella Cita Blvd/Sinclair Rd

| | • | - | • | • | 1 | † | - | Ţ |
|----------------------|-------|-------------|-------|------------|-------|----------|-------|-------|
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Configurations | ሻ | ∱ î≽ | 7 | ∱ ∱ | 7 | f) | ሻ | f) |
| Traffic Volume (vph) | 43 | 341 | 386 | 399 | 186 | 23 | 105 | 103 |
| Future Volume (vph) | 43 | 341 | 386 | 399 | 186 | 23 | 105 | 103 |
| Turn Type | pm+pt | NA | pm+pt | NA | pm+pt | NA | pm+pt | NA |
| Protected Phases | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 8 | | 2 | | 6 | |
| Detector Phase | 7 | 4 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | |
| Minimum Initial (s) | 5.0 | 15.0 | 5.0 | 15.0 | 7.0 | 15.0 | 5.0 | 10.0 |
| Minimum Split (s) | 10.5 | 23.5 | 23.5 | 23.5 | 12.5 | 20.5 | 10.5 | 23.5 |
| Total Split (s) | 23.0 | 49.0 | 23.0 | 49.0 | 16.0 | 42.0 | 16.0 | 42.0 |
| Total Split (%) | 17.7% | 37.7% | 17.7% | 37.7% | 12.3% | 32.3% | 12.3% | 32.3% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lead | Lag | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | Min | None | Min |

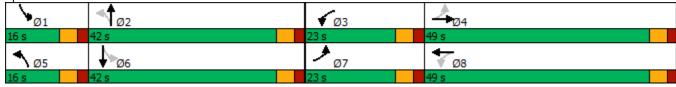
Intersection Summary

Cycle Length: 130

Actuated Cycle Length: 90.5

Natural Cycle: 85





| | ۶ | → | • | • | — | • | • | † | ~ | > | + | ✓ |
|------------------------------|------|------------|------|------|------------|------|------|------|------|-------------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ∱ ⊅ | | ሻ | ∱ ∱ | | 7 | ₽ | | ሻ | ₽ | |
| Traffic Volume (veh/h) | 43 | 341 | 335 | 386 | 399 | 50 | 186 | 23 | 183 | 105 | 103 | 107 |
| Future Volume (veh/h) | 43 | 341 | 335 | 386 | 399 | 50 | 186 | 23 | 183 | 105 | 103 | 107 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1811 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1856 |
| Adj Flow Rate, veh/h | 48 | 379 | 372 | 429 | 443 | 56 | 207 | 26 | 203 | 117 | 114 | 119 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, % | 6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 |
| Cap, veh/h | 401 | 522 | 466 | 461 | 1395 | 175 | 325 | 38 | 300 | 299 | 141 | 147 |
| Arrive On Green | 0.04 | 0.29 | 0.29 | 0.18 | 0.44 | 0.44 | 0.11 | 0.21 | 0.21 | 0.07 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1725 | 1777 | 1585 | 1781 | 3176 | 399 | 1781 | 183 | 1430 | 1781 | 838 | 875 |
| Grp Volume(v), veh/h | 48 | 379 | 372 | 429 | 247 | 252 | 207 | 0 | 229 | 117 | 0 | 233 |
| Grp Sat Flow(s), veh/h/ln | 1725 | 1777 | 1585 | 1781 | 1777 | 1798 | 1781 | 0 | 1613 | 1781 | 0 | 1713 |
| Q Serve(g_s), s | 1.8 | 17.5 | 19.8 | 14.7 | 8.3 | 8.4 | 8.6 | 0.0 | 12.0 | 4.9 | 0.0 | 12.0 |
| Cycle Q Clear(g_c), s | 1.8 | 17.5 | 19.8 | 14.7 | 8.3 | 8.4 | 8.6 | 0.0 | 12.0 | 4.9 | 0.0 | 12.0 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 0.22 | 1.00 | | 0.89 | 1.00 | | 0.51 |
| Lane Grp Cap(c), veh/h | 401 | 522 | 466 | 461 | 780 | 790 | 325 | 0 | 339 | 299 | 0 | 288 |
| V/C Ratio(X) | 0.12 | 0.73 | 0.80 | 0.93 | 0.32 | 0.32 | 0.64 | 0.00 | 0.68 | 0.39 | 0.00 | 0.81 |
| Avail Cap(c_a), veh/h | 664 | 843 | 752 | 474 | 843 | 854 | 325 | 0 | 642 | 374 | 0 | 682 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.0 | 29.0 | 29.8 | 19.5 | 16.7 | 16.8 | 27.4 | 0.0 | 33.3 | 28.7 | 0.0 | 36.7 |
| Incr Delay (d2), s/veh | 0.1 | 1.9 | 3.2 | 25.0 | 0.2 | 0.2 | 4.1 | 0.0 | 2.4 | 0.8 | 0.0 | 5.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(95%),veh/ln | 1.3 | 12.1 | 12.3 | 13.7 | 6.0 | 6.1 | 7.1 | 0.0 | 8.4 | 3.8 | 0.0 | 9.2 |
| Unsig. Movement Delay, s/veh | | 21.0 | 22.0 | 44.5 | 17.0 | 17.0 | 24 5 | 0.0 | 25.7 | 20.7 | 0.0 | 40.0 |
| LnGrp Delay(d),s/veh | 21.1 | 31.0 | 33.0 | 44.5 | 17.0 | 17.0 | 31.5 | 0.0 | 35.7 | 29.6 | 0.0 | 42.2 |
| LnGrp LOS | С | C | С | D | В | В | С | A | D | С | A | <u>D</u> |
| Approach Vol, veh/h | | 799 | | | 928 | | | 436 | | | 350 | |
| Approach Delay, s/veh | | 31.3 | | | 29.7 | | | 33.7 | | | 38.0 | |
| Approach LOS | | С | | | С | | | С | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.1 | 24.8 | 22.3 | 32.5 | 16.0 | 20.9 | 9.0 | 45.7 | | | | |
| Change Period (Y+Rc), s | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | | | | |
| Max Green Setting (Gmax), s | 10.5 | 36.5 | 17.5 | 43.5 | 10.5 | 36.5 | 17.5 | 43.5 | | | | |
| Max Q Clear Time (g_c+I1), s | 6.9 | 14.0 | 16.7 | 21.8 | 10.6 | 14.0 | 3.8 | 10.4 | | | | |
| Green Ext Time (p_c), s | 0.1 | 1.4 | 0.1 | 5.1 | 0.0 | 1.4 | 0.1 | 3.3 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 32.1 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

Arterial Level of Service 2025 Build
AM Peak Hour

Arterial Level of Service: NB Sinclair Rd

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 160.6 | 9.7 | 170.3 | 1.36 | 28.7 | В |
| Total | III | | 160.6 | 9.7 | 170.3 | 1.36 | 28.7 | В |

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 35 | 43.5 | 4.5 | 48.0 | 0.36 | 27.2 | В |
| Goodman Rd | III | 32 | 154.3 | 19.7 | 174.0 | 1.36 | 28.0 | В |
| Total | III | | 197.8 | 24.2 | 222.0 | 1.72 | 27.9 | В |

Arterial Level of Service 2025 Build
PM Peak Hour

Arterial Level of Service: NB Sinclair Rd

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 162.6 | 7.8 | 170.4 | 1.36 | 28.6 | В |
| Total | III | | 162.6 | 7.8 | 170.4 | 1.36 | 28.6 | В |

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 46.0 | 3.8 | 49.8 | 0.36 | 26.2 | В |
| Goodman Rd | III | 30 | 162.6 | 21.0 | 183.6 | 1.36 | 26.6 | В |
| Total | III | | 208.6 | 24.8 | 233.4 | 1.72 | 26.5 | В |

Arterial Level of Service 2045 Build
AM Peak Hour

Arterial Level of Service: NB Sinclair Rd

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 160.6 | 31.0 | 191.6 | 1.36 | 25.5 | В |
| Total | III | | 160.6 | 31.0 | 191.6 | 1.36 | 25.5 | В |

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 35 | 43.5 | 9.1 | 52.6 | 0.36 | 24.8 | В |
| Goodman Rd | III | 32 | 154.3 | 22.3 | 176.6 | 1.36 | 27.6 | В |
| Total | III | | 197.8 | 31.4 | 229.2 | 1.72 | 27.0 | В |

Arterial Level of Service 2045 Build
PM Peak Hour

Arterial Level of Service: NB Sinclair Rd

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 162.6 | 19.6 | 182.2 | 1.36 | 26.8 | В |
| Total | III | | 162.6 | 19.6 | 182.2 | 1.36 | 26.8 | В |

| | Arterial | Flow | Running | Signal | Travel | Dist | Arterial | Arterial |
|----------------|----------|-------|---------|--------|----------|------|----------|----------|
| Cross Street | Class | Speed | Time | Delay | Time (s) | (mi) | Speed | LOS |
| Tradition Blvd | III | 30 | 46.0 | 6.1 | 52.1 | 0.36 | 25.0 | В |
| Goodman Rd | III | 30 | 162.6 | 19.2 | 181.8 | 1.36 | 26.8 | В |
| Total | III | | 208.6 | 25.3 | 233.9 | 1.72 | 26.4 | В |

APPENDIX G

Crash Data

| 2017 | | | | | |
|------|------|---------------|-----------|---------|---------------------------------------|
| 2016 | 2017 | 2018 | 2019 | 2020 | Total |
| | 1 | | | 1 | 2 |
| | | | 1 | | 1 |
| 1 | | 2 | | 2 | 5 |
| | | | | 1 | 1 |
| 1 | 1 | 2 | 1 | 4 | 9 |
| | 1 | 1 1 1 1 | 1 1 2 1 2 | 1 1 2 1 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |

| Light Condition | olumn Labels | | | | | | | | |
|--------------------|--------------|------|------|------|------|-------|--|--|--|
| Row Labels | 2016 | 2017 | 2018 | 2019 | 2020 | Total | | | |
| Dark - Lighted | | | 2 | | 2 | 4 | | | |
| Dark - Not Lighted | | 1 | | | | 1 | | | |
| Daylight | 1 | | | 1 | 2 | 4 | | | |
| Total | 1 | 1 | 2 | 1 | 4 | 9 | | | |

| Crash Severity per Intersection | olumn Labels | : | |
|---------------------------------|--------------|---|-------|
| Row Labels | 1 | 2 | Total |
| 1 | 4 | | 4 |
| Injury | 1 | | 1 |
| No Injury | 3 | | 3 |
| 2 | | 5 | 5 |
| No Injury | | 5 | 5 |
| Total | 4 | 5 | 9 |

| Crash Type | olumn Labe | ls | | | | |
|------------|------------|------|------|------|------|-------|
| | 2016 | 2017 | 2018 | 2019 | 2020 | Total |
| | | | | | | |
| Row Labels | | | | | | |
| 1 | | | 2 | | 2 | 4 |
| Off Road | | | 2 | | 2 | 4 |
| 2 | 1 | 1 | | 1 | 2 | 5 |
| Left Turn | | 1 | | | 1 | 2 |
| Off Road | 1 | | | | | 1 |
| Rear End | | | | 1 | | 1 |
| Sideswipe | | | | | 1 | 1 |
| Total | 1 | 1 | 2 | 1 | 4 | 9 |

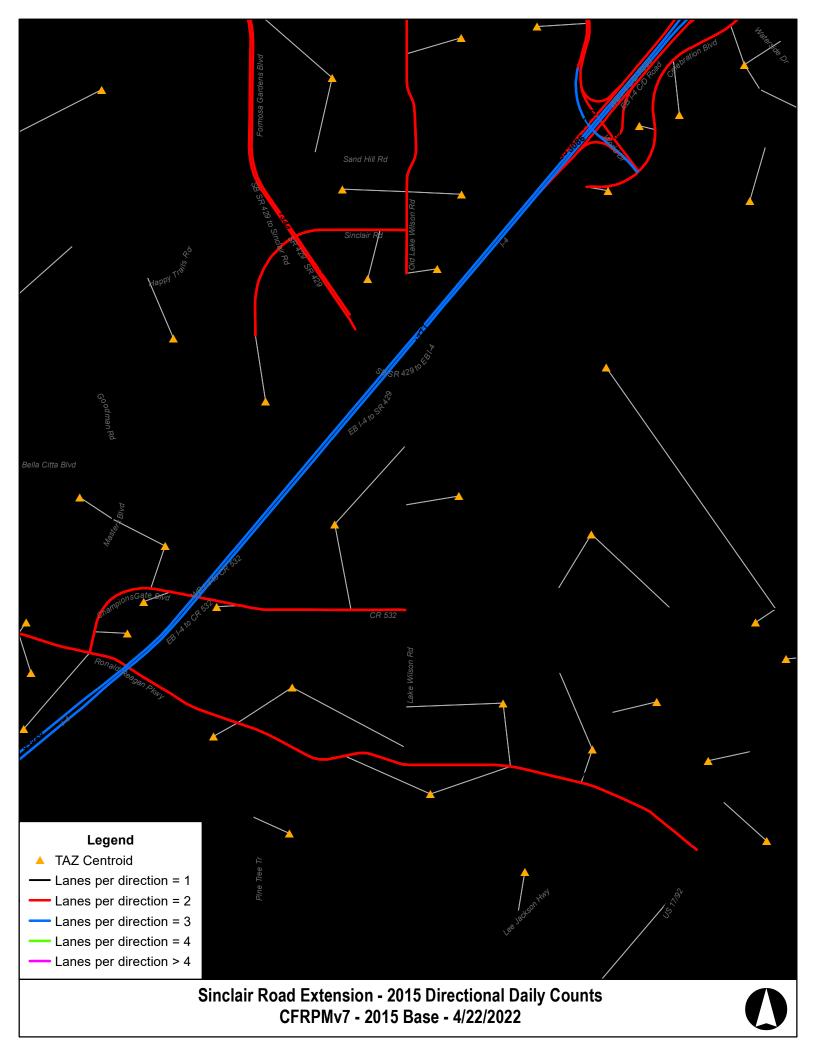
| Crash Type per Time of Day | olumn Labe | ls | | | | | | | |
|----------------------------|------------|------|------|------|-------|------|-------|-------|--------------------|
| | 12 AM | 3 AM | 6 AM | 8 AM | 12 PM | 4 PM | 10 PM | 11 PM | Grand Total |
| Row Labels | | | | | | | | | |
| Left Turn | 1 | | | | 1 | | | | 2 |
| Off Road | | 1 | 1 | 1 | | | 1 | 1 | 5 |
| Rear End | | | | | | 1 | | | 1 |
| Sideswipe | | | | 1 | | | | | 1 |
| Grand Total | 1 | 1 | 1 | 2 | 1 | 1 | 1 | 1 | 9 |

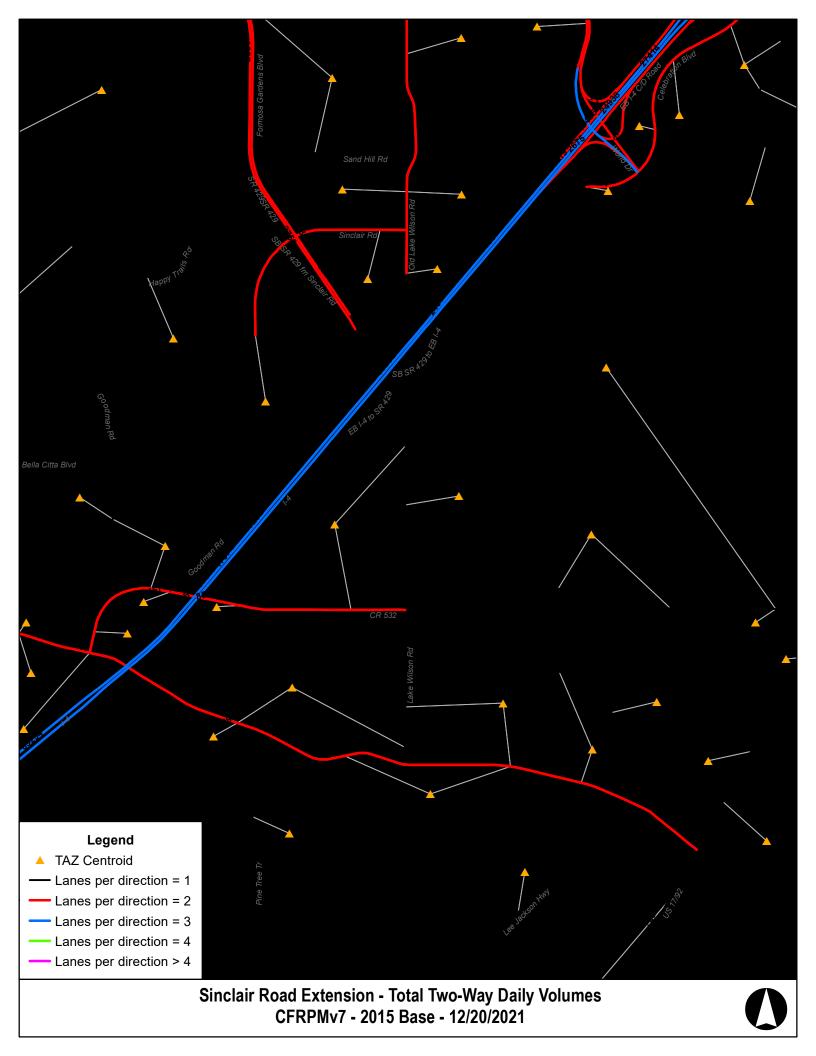
| Harmful Event | olumn Labe | els | | | | |
|----------------------------|------------|------|------|------|------|-------|
| Row Labels | 2016 | 2017 | 2018 | 2019 | 2020 | Total |
| Guardrail Face | | | | | 2 | 2 |
| Motor Vehicle in Transport | | 1 | | 1 | 2 | 4 |
| Traffic Sign Support | | | 1 | | | 1 |
| Tree (standing) | 1 | | | | | 1 |
| Utility Pole/Light Support | | | 1 | | | 1 |
| Total | 1 | 1 | 2 | 1 | 4 | 9 |

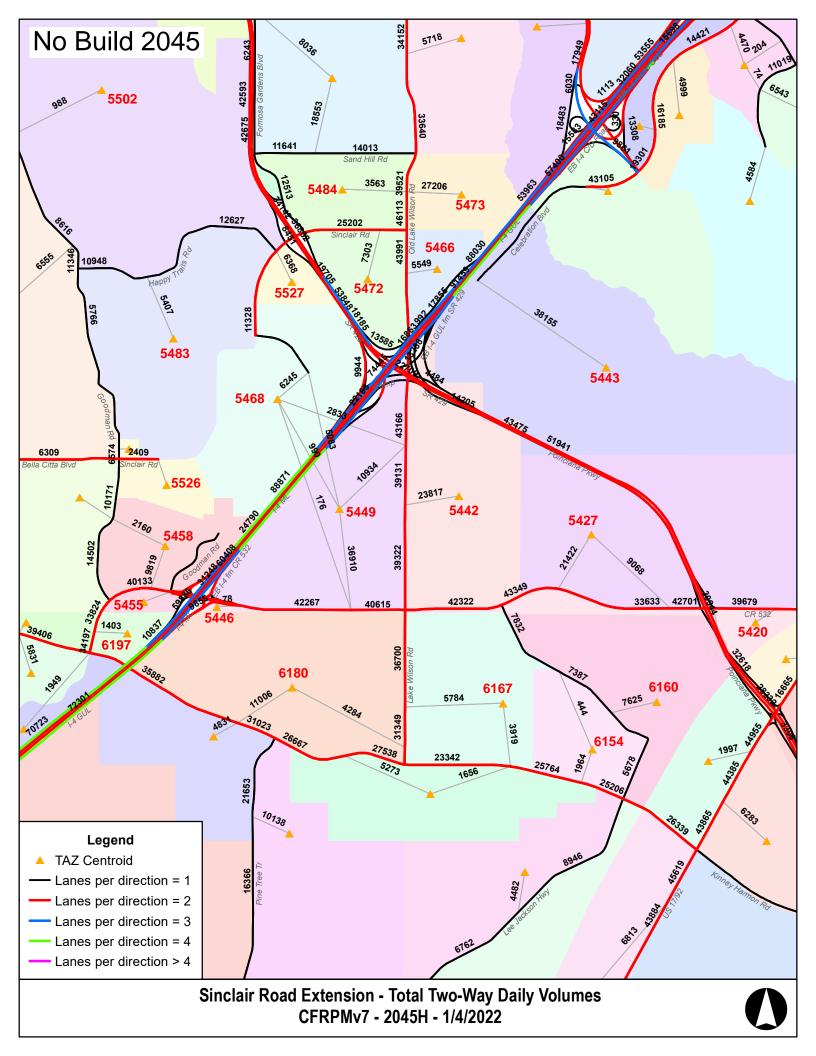
| Crash Severity | olumn Labels | | | | | | | |
|----------------|--------------|------|------|------|------|--------------------|--|--|
| Row Labels | 2016 | 2017 | 2018 | 2019 | 2020 | Grand Total | | |
| Injury | | | 1 | | | 1 | | |
| No Injury | 1 | 1 | 1 | 1 | 4 | 8 | | |
| Grand Total | 1 | 1 | 2 | 1 | 4 | 9 | | |

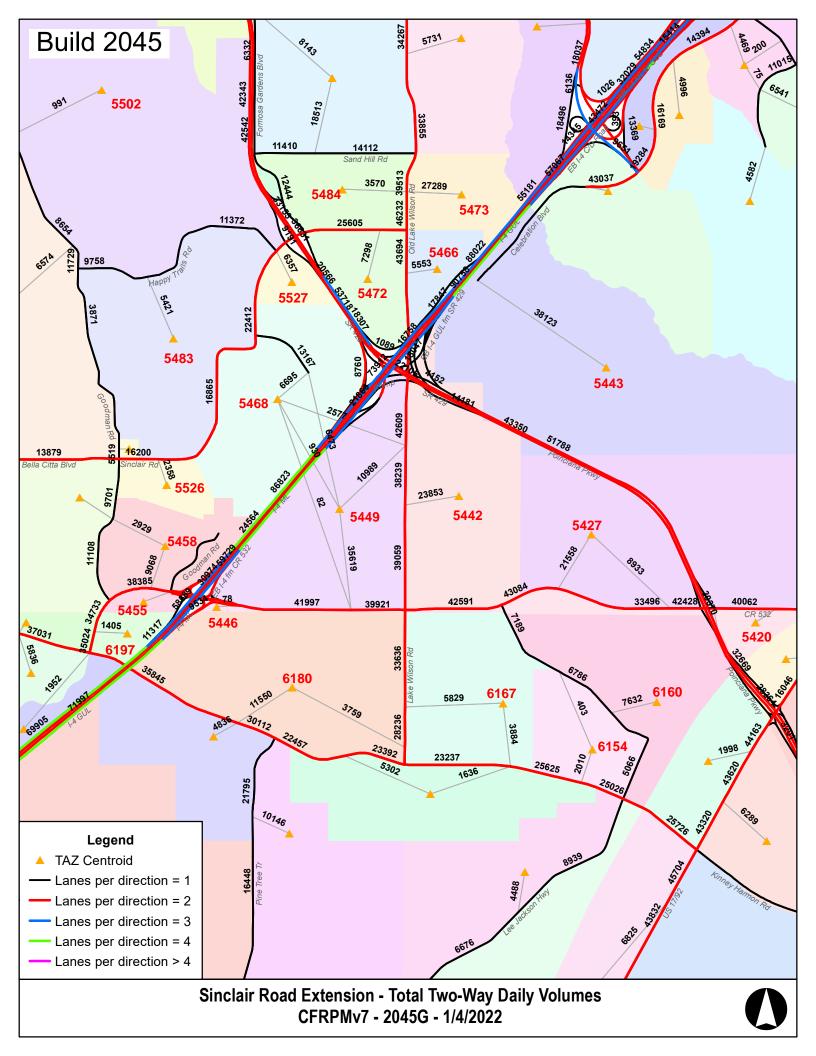
APPENDIX H

CFRPMv7 Model Outputs









APPENDIX I

Sinclair Road Extension – CFRPM7 Representation of Reunion Development Technical Memorandum



MEMORANDUM

To: Robert Denney, PE

Transportation & Transit Department

Osceola County

From: James M. Taylor, P.E.

Kimley-Horn and Associates, Inc.

Date: May 11, 2022

Subject: Sinclair Road Extension | CFRPM v7 Representation of Reunion Development

Introduction

Kimley-Horn and Associates, Inc. is preparing a Project Traffic Analysis Report (PTAR) to provide design traffic volumes and traffic analyses in support of the Alternatives Evaluation Study for Sinclair Road Extension, from Tradition Boulevard to Bella Citta Boulevard. During the development of the PTAR, Osceola County requested clarification of the travel demand model's representation of the Reunion Development of Regional Impact (DRI). This memorandum documents the latest adopted Central Florida Regional Planning Model (CFRPM v7) socioeconomic data in and around the Reunion development and compares this information with the approved development levels in the Reunion DRI.

Reunion DRI

Figure 1 illustrates the "Map H" for the Reunion DRI (Map H is the concept plan for the development). The total development plan approved for the Reunion DRI is summarized in **Table 1**. Because the travel demand model uses employment instead of square footage to account for office and retail space, the square footage from the Reunion DRI Map H has been converted to number of service and commercial employees.

Table 1: Reunion DRI Development Plan

| Type of Development | Development Intensity | Employees |
|--------------------------------------------------|--------------------------|------------------|
| Residential Resort (Single-Family & Multifamily) | 6,233 DU | - |
| Hotel Rooms | 1,574 DU | - |
| Office | 140,000 SF | 560 Service |
| Retail | 484,000 SF | 1,210 Commercial |
| Golf | 54 Holes | 60 Commercial |

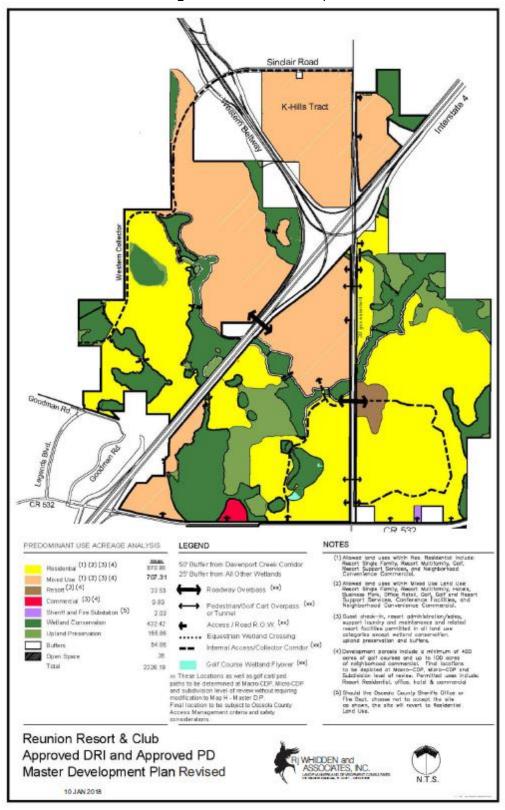


Figure 1: Reunion DRI Map H



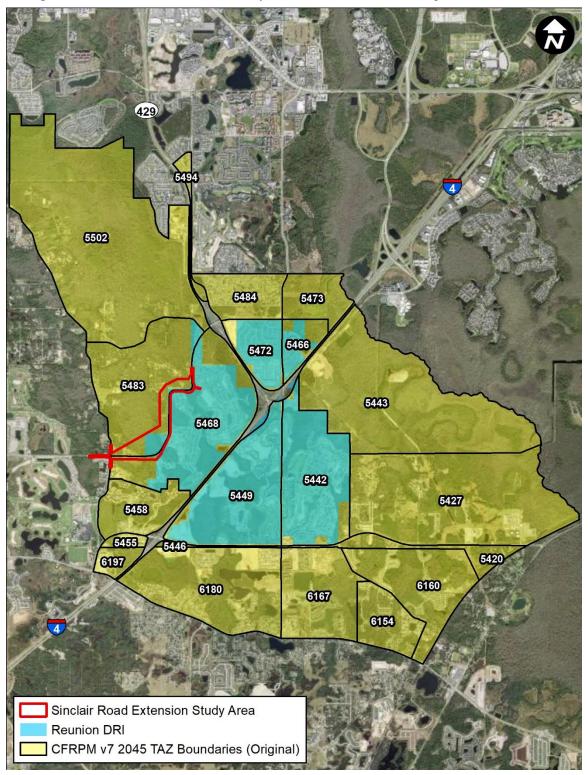
Travel Demand Model Socioeconomic Data

Results from the CFRPM v7 were considered in the development of forecasted design year 2045 traffic for the PTAR. The socioeconomic data (dwelling units, employment, etc.) in the 2045 model are approved by the metropolitan planning organizations (MPOs) and local governments. Thus, it is understood that Osceola County approved the socioeconomic data (at the traffic analysis zone (TAZ) level) that is included in the 2045 model. The socioeconomic data forecasts utilize the population forecasts developed by the Bureau of Economic and Business Research (BEBR) at the county level. These forecasts are spread across each county's TAZs based on assumptions by the local governments. With Osceola County's historic and projected high level of growth, some areas within the County are anticipated to have higher intensity and density of development in the future than what currently exists today. While it is recognized that not all the actual 2045 development will be located in the specific TAZs assumed, these forecasts are as accurate as possible given the available information at the time they are developed.

Figure 2 illustrates the Sinclair Road Extension study area, the area covered by the Reunion DRI, and the adjacent TAZ boundaries in the original unedited CFRPM v7.

As part of the review of the socioeconomic data in the CFRPM v7 2045 model set, TAZs 5468 and 5483 (which border the Sinclair Road Extension study area) were modified to separate out planned development in the area. **Figure 3** illustrates the original boundaries of TAZs 5468 and 5483. **Figure 4** illustrates the revised boundaries of TAZs 5468 and 5483 and the addition of TAZs 5525, 5526 and 5527. TAZ 5525 was separated from TAZ 5483 to represent the planned Goodman Road Charter School in the northeast quadrant of Bella Citta Boulevard and Goodman Road. TAZ 5526 was separated from TAZ 5468 to represent the development of the Dewan/Elevation parcel. TAZ 5527 was separated from TAZ 5468 to represent the development of the Sinclair Road Property project.

Figure 2: Sinclair Road Extension Study Area, Reunion DRI, and Original TAZ Boundaries



5483 5468 Sinclair Road Extension Study Area CFRPM v7 2045 TAZ Boundaries (Original)

Figure 3: Original Boundaries of TAZs 5468 and 5483

Figure 4: Revised Boundaries of TAZs 5468 and 5483 and Addition of TAZs 5525, 5526 and 5527

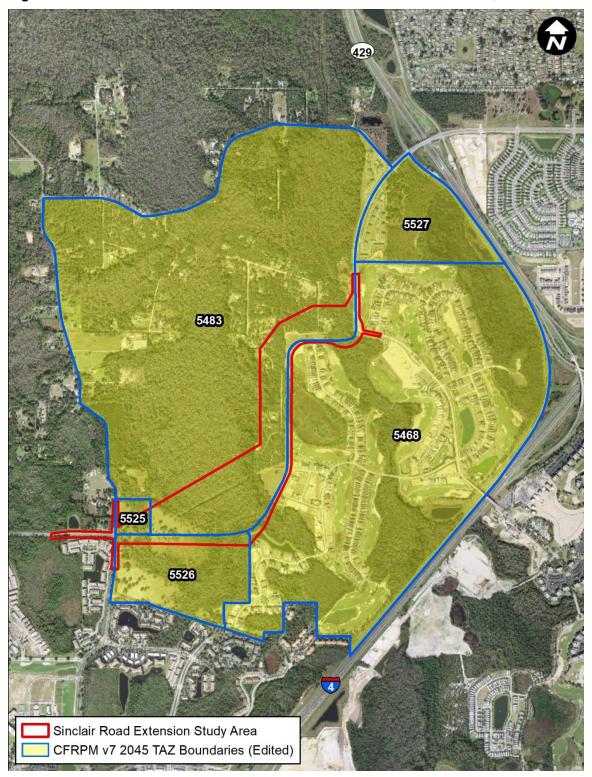


Table 2 summarizes the adjustments to the 2045 multifamily dwelling units, commercial employment, service employment, and school enrollment for these TAZs. There were no changes to the single-family dwelling units, hotel/motel rooms, or industrial employment. In total, the number of multifamily dwelling units increased by 1,026 (from 1,546 to 2,572); commercial employment increased by 13 (from 487 to 500); service employment increased by 29 (from 1,144 to 1,173); and school enrollment increased by 2,550 (from 0 to 2,550). While the school enrollment is 850 students, this was increased by a factor of 3.0 to get the model to align with the Institute of Transportation Engineer's (ITE) trip generation for an 850-student school.

Dwelling Units Employees Students TAZ Multifamily Commercial Service K-12 Initial Revised Initial Revised Initial Revised Initial Revised 1,206 334 5468 316 328 495 481 0 0 5483 340 340 153 153 649 649 0 0 5525 ¹ 0 0 0 0 0 0 0 2,550 5526² 0 533 0 0 0 0 0 0 5527² 0 1,383 0 19 0 43 0 0 Total 1,546 2,572 487 500 1,144 1,173 0 2,550

Table 2: TAZ Splits and Socioeconomic Data Revisions

Notes:

Table 3 summarizes the socioeconomic data in the TAZs illustrated on **Figure 2**, including the splits and revisions identified on **Figure 4** and in **Table 2**. The TAZs which include portions of the Reunion DRI are highlighted in blue. **Figure 5** illustrates the Reunion DRI and the adjacent and associated TAZs. All TAZs except 5447 and 5468 include some non-Reunion development. As identified in **Table 3**, the TAZs which include portions of the Reunion DRI represent a development level higher than what is in the Reunion DRI Map H.

^{1.} New TAZ, split from 5483 for the planned Goodman Road Charter School (850 students) (includes a factor of 3.0 to align with ITE trip generation)

^{2.} New TAZ, split from 5468 for Dewan/Elevation (444 Multifamily DU) and Sinclair Road Property (446 Multifamily DU, 3.5 KSF restaurant, and 10 pump gas station) (includes a factor of 1.2 for TAZ 5526 and 3.1 for TAZ 5527 to better reflect ITE estimated daily trips).

Sinclair Road Extension Study Area Reunion DRI CFRPM v7 2045 TAZ Boundaries (Original) CFRPM v7 2045 TAZ Boundaries (Edited)

Figure 5: Reunion DRI and the Adjacent and Associated TAZs

Table 3: Summary of 2045 Socioeconomic Data by TAZ

| TAZ | Single Family Dwelling Units | Multifamily Dwelling Units | Hotel/Motel Dwelling Units | Commercial Employees | Service Employees | Industrial Employees | Students |
|-----------------|---------------------------------------|----------------------------------|----------------------------------|-------------------------|----------------------|-------------------------|----------|
| 5420 | 15 | 17 | 0 | 165 | 977 | 0 | 0 |
| 5427 | 171 | 14 | 0 | 2,145 | 3,958 | 15 | 0 |
| 5442 | 711 | 1,656 | 1,320 | 579 | 2,444 | 4 | 0 |
| 5443 | 4,147 | 1,265 | 1,067 | 345 | 1,277 | 178 | 0 |
| 5446 | 0 | 0 | 0 | 8 | 5 | 0 | 0 |
| 5449 | 401 | 2,978 | 3,276 | 2,620 | 4,022 | 2 | 1,986 |
| 5455 | 0 | 308 | 74 | 98 | 186 | 2 | 0 |
| 5458 | 512 | 1,052 | 616 | 218 | 563 | 11 | 0 |
| 5466 | 197 | 241 | 36 | 161 | 224 | 0 | 0 |
| 5468 | 509 | 316 | 834 | 328 | 481 | 25 | 0 |
| 5472 | 427 | 474 | 711 | 0 | 482 | 0 | 0 |
| 5473 | 0 | 0 | 0 | 2,133 | 3,281 | 0 | 0 |
| 5483 | 154 | 340 | 33 | 153 | 649 | 4 | 0 |
| 5484 | 500 | 0 | 97 | 52 | 240 | 12 | 0 |
| 5494 | 60 | 0 | 59 | 0 | 6 | 1 | 0 |
| 5502 | 197 | 0 | 0 | 0 | 9 | 0 | 0 |
| 5525 | 0 | 0 | 0 | 0 | 0 | 0 | 2,550 |
| 5526 | 0 | 533 | 0 | 0 | 0 | 0 | 0 |
| 5527 | 0 | 1,383 | 0 | 19 | 43 | 0 | 0 |
| 6154 | 432 | 62 | 0 | 0 | 52 | 12 | 0 |
| 6160 | 772 | 84 | 853 | 8 | 486 | 0 | 0 |
| 6167 | 438 | 1,054 | 751 | 0 | 376 | 10 | 0 |
| 6180 | 884 | 587 | 192 | 465 | 716 | 7 | 0 |
| 6197 | 0 | 0 | 0 | 43 | 175 | 250 | 10 |
| Total | 10,527 | 12,364 | 9,919 | 9,540 | 20,652 | 533 | 4,546 |
| Reunion TAZs | 9,7 | 787 | 6,210 | 3,860 | 8,345 | 35 | 1,986 |
| Reunion DRI | 6,2 | 233 | 1,574 | 1,270 | 560 | 0 | 0 |



Conclusion

The socioeconomic data used in the CFRPM v7 model for 2045 is reasonable, consistent with projected growth in Osceola County, and appropriate for developing projected traffic demands on the roadway network, including for Sinclair Road Extension.

It is important to recognize that the Reunion DRI is represented by seven TAZs (the blue highlighted TAZs in **Table 3**) and most of these TAZs also include non-Reunion development, and/or higher levels of development than currently approved in the Reunion DRI. Thus, the identification of Reunion traffic in the model will need to include a more detailed analysis than summarizing the trips from the TAZs that include the Reunion DRI.

APPENDIX J

BEBR Population Projections

Projections of Florida Population by County, 2025–2045, with Estimates for 2020 (continued)

| County | Estimates | | | | | |
|-------------------------------------|---------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|
| and State | April 1, 2020 | 2025 | 2030 | 2035 | 2040 | 2045 |
| MIAMI-DADE Low Medium High | 2,832,794 | 2,791,500 2,992,700 3,186,900 | 2,844,300 3,128,300 3,423,300 | 2,871,900 3,234,600 3,621,000 | 2,880,900 3,322,200 3,799,900 | 2,876,900 3,398,200 3,964,600 |
| MONROE Low Medium High | 77,823 | 73,600 78,800 84,300 | 72,200 79,400 87,500 | 70,500 79,800 90,100 | 68,700 80,000 92,200 | 66,700 80,200 94,200 |
| NASSAU Low Medium High | 89,258 | 89,500 99,200 108,200 | 93,600 107,500 121,600 | 96,800 114,600 134,900 | 99,300 121,100 148,200 | 100,800 126,900 161,400 |
| OKALOOSA Low Medium High | 203,951 | 200,200 214,600 228,500 | 202,800 223,200 244,000 | 204,000 230,000 257,200 | 204,500 236,000 269,700 | 203,800 241,100 280,900 |
| OKEECHOBEE Low Medium High | 42,112 | 40,600 43,400 46,500 | 40,500 44,500 49,100 | 40,300 45,300 51,500 | 39,900 46,000 53,700 | 39,500 46,700 55,900 |
| ORANGE Low Medium High | 1,415,260 | 1,429,800 1,558,700 1,674,800 | 1,494,500 1,678,400 1,857,100 | 1,542,300 1,777,900 2,021,600 | 1,577,800 1,864,300 2,179,700 | 1,602,500 1,941,800 2,331,800 |
| OSCEOLA Low Medium High | 387,055 | 409,200 453,600 491,900 | 447,500 512,500 574,500 | 476,000 560,700 649,300 | 499,500 603,600 723,900 | 518,300 643,100 798,500 |
| PALM BEACH Low Medium High | 1,466,494 | 1,440,900 1,544,900 1,645,000 | 1,465,500 1,612,200 1,763,800 | 1,482,000 1,668,600 1,868,600 | 1,491,200 1,717,000 1,966,800 | 1,491,500 1,758,500 2,055,400 |
| PASCO Low Medium High | 542,638 | 543,900 593,000 637,100 | 565,700 635,700 703,000 | 578,700 668,800 758,500 | 586,200 696,400 809,700 | 589,400 720,500 857,600 |
| PINELLAS Low Medium High | 984,054 | 960,600 1,011,800 1,067,900 | 959,500 1,031,400 1,116,700 | 953,100 1,045,200 1,153,300 | 943,000 1,055,500 1,184,100 | 930,500 1,063,800 1,210,200 |
| POLK Low Medium High | 715,090 | 718,300 783,100 841,400 | 747,800 840,200 929,200 | 770,200 888,400 1,009,500 | 785,000 929,300 1,084,500 | 794,600 965,800 1,156,200 |
| PUTNAM Low Medium High | 73,723 | 69,300 74,200 79,400 | 67,900 74,700 82,200 | 66,400 75,100 84,900 | 64,800 75,500 87,100 | 63,300 75,800 89,400 |
| ST. JOHNS Low Medium High | 261,900 | 274,700 304,600 330,200 | 297,000 340,500 381,300 | 314,400 370,900 428,800 | 328,600 398,000 476,200 | 339,400 422,800 522,900 |
| ST. LUCIE Low Medium High | 322,265 | 326,300 355,800 382,300 | 342,800 384,800 426,000 | 353,400 407,500 463,200 | 360,300 426,400 497,800 | 364,400 443,100 530,300 |

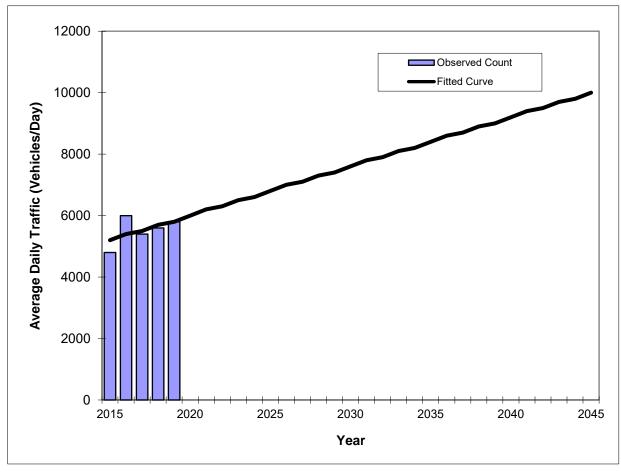
APPENDIX K

Growth Trend Analysis

Traffic Trends - V03.a BELLA CITTA BLVD -- WEST OF GOODMAND RD

FIN# 0 Location 1

| County: | Osceola (92) |
|------------|------------------|
| Station #: | 0 |
| Highway: | BELLA CITTA BLVD |



| | Traffic (AD | T/AADT) |
|------|----------------|-----------|
| Year | Count* | Trend** |
| 2015 | 4800 | 5200 |
| 2016 | 6000 | 5400 |
| 2017 | 5400 | 5500 |
| 2018 | 5600 | 5700 |
| 2019 | 5800 | 5800 |
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| | 5 Opening Yea | |
| 2025 | N/A | 6800 |
| _ | 035 Mid-Year T | |
| 2035 | N/A | 8400 |
| | 15 Design Year | |
| 2045 | N/A | 10000 |
| IRAN | PLAN Forecas | ts/Trends |
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** Annual Trend Increase: 160

Trend R-squared: 30.19%

Trend Annual Historic Growth Rate: 2.88%

Trend Growth Rate (2019 to Design Year): 2.79%

Printed: 17-May-22

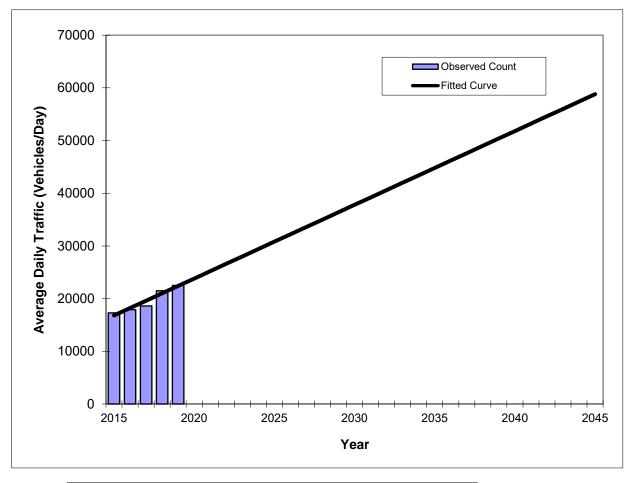
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a CHAMPIONS GATE BLVD -- EAST OF MASTERS BLVD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| County: | Osceola (92) |
|------------|---------------------|
| Station #: | 0 |
| Highway: | CHAMPIONS GATE BLVD |



| i oai | Oddine | Hona |
|-------|----------------|---------|
| 2015 | 17300 | 16800 |
| 2016 | 17900 | 18200 |
| | | |
| 2017 | 18600 | 19600 |
| 2018 | 21500 | 21000 |
| 2019 | 22500 | 22400 |
| 2013 | 22300 | 22400 |
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| 202 | 5 Opening Yea | r Trend |
| 2025 | N/A | 30800 |
| 2 | 035 Mid-Year T | rend |
| 2035 | N/A | 44800 |
| 204 | 15 Design Year | Trend |
| 2045 | N/A | 58800 |
| TRAN | PLAN Forecas | |
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Traffic (ADT/AADT)

Count* Trend**

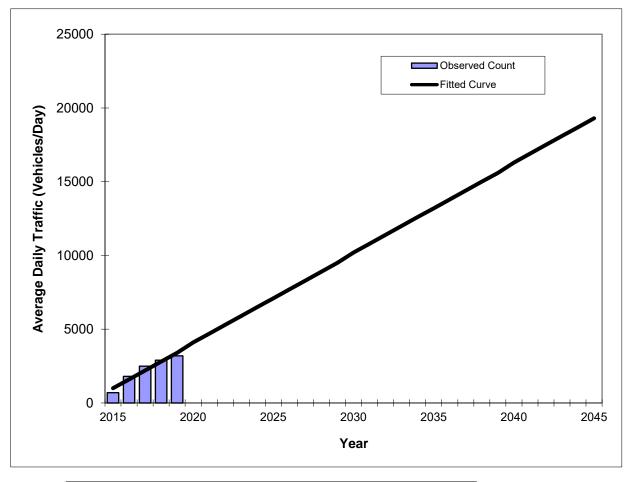
** Annual Trend Increase: 1,400
Trend R-squared: 92.49%
Trend Annual Historic Growth Rate: 8.33%
Trend Growth Rate (2019 to Design Year): 6.25%
Printed: 17-May-22
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a GOODMAN ROAD -- NORTH OF BELLA CITTA BLVD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| County: | Osceola (92) |
|------------|--------------|
| Station #: | 0 |
| Highway: | GOODMAN ROAD |



| | Traffic (ADT/AADT) | | |
|------|--------------------|-----------|--|
| Year | Count* | Trend** | |
| 2015 | 700 | 1000 | |
| 2016 | 1800 | 1600 | |
| 2017 | 2500 | 2200 | |
| 2018 | 2900 | 2800 | |
| 2019 | 3200 | 3400 | |
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| 202 | 5 Opening Yea | r Trend | |
| 2025 | N/A | 7100 | |
| | 035 Mid-Year T | | |
| 2035 | N/A | 13200 | |
| | 15 Design Year | | |
| 2045 | N/A | 19300 | |
| IRAN | PLAN Forecas | ts/Trends | |
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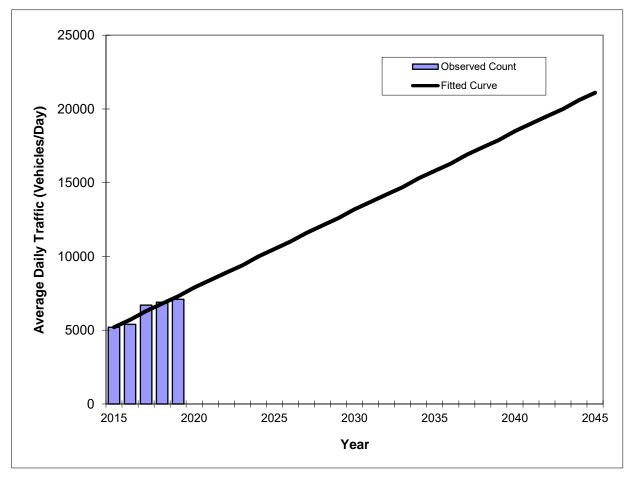
** Annual Trend Increase: 610
Trend R-squared: 93.30%
Trend Annual Historic Growth Rate: 60.00%
Trend Growth Rate (2019 to Design Year): 17.99%
Printed: 17-May-22
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a GOODMAN ROAD -- SOUTH OF BELLA CITTA BLVD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| Station #: 0 Highway: GOODMAN BOAD | County: | Osceola (92) |
|------------------------------------|------------|--------------|
| Highway: COODMAN ROAD | Station #: | 0 |
| riigiway: GOODMAN NOAD | Highway: | GOODMAN ROAD |



| | Traffic (AD | |
|------|----------------|-----------|
| Year | Count* | Trend** |
| 2015 | 5200 | 5200 |
| 2016 | 5400 | 5700 |
| 2017 | 6700 | 6300 |
| 2018 | 6900 | 6800 |
| 2019 | 7100 | 7300 |
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| 202 | 5 Opening Yea | r Trend |
| 2025 | N/A | 10500 |
| 2 | 035 Mid-Year 1 | rend |
| 2035 | N/A | 15800 |
| 204 | 15 Design Year | Trend |
| 2045 | N/A | 21100 |
| TRAN | PLAN Forecas | ts/Trends |
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** Annual Trend Increase: 530

Trend R-squared: 88.56%

Trend Annual Historic Growth Rate: 10.10%

Trend Growth Rate (2019 to Design Year): 7.27%

Printed: 17-May-22

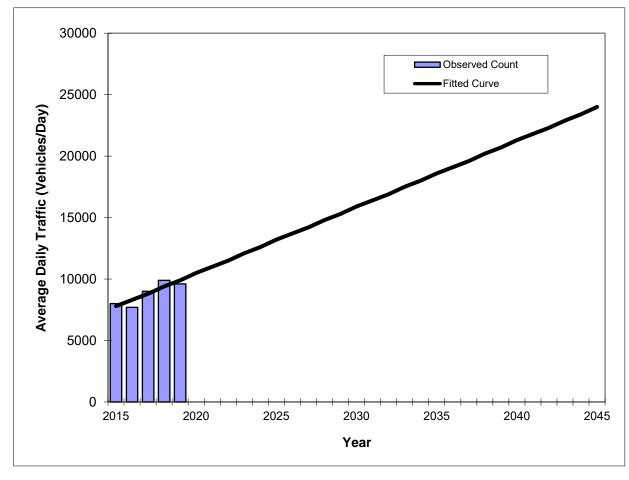
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a MASTERS BLVD -- NORTH OF CHAMPIONS GATE BLVD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| County: | Osceola (92) | |
|------------|--------------|--|
| Station #: | 0 | |
| Highway: | MASTERS BLVD | |



| | Traffic (ADT/AADT) | |
|------|--------------------|-----------|
| Year | Count* | Trend** |
| 2015 | 8000 | 7800 |
| 2016 | 7700 | 8300 |
| 2017 | 9000 | 8800 |
| 2018 | 9900 | 9400 |
| 2019 | 9600 | 9900 |
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| 202 | 5 Opening Yea | r Trend |
| 2025 | N/A | 13200 |
| | 035 Mid-Year T | |
| 2035 | N/A | 18600 |
| 204 | 15 Design Year | Trend |
| 2045 | N/A | 24000 |
| TRAN | PLAN Forecas | ts/Trends |
| | | |
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** Annual Trend Increase: 540

Trend R-squared: 78.14%

Trend Annual Historic Growth Rate: 6.73%

Trend Growth Rate (2019 to Design Year): 5.48%

Printed: 17-May-22

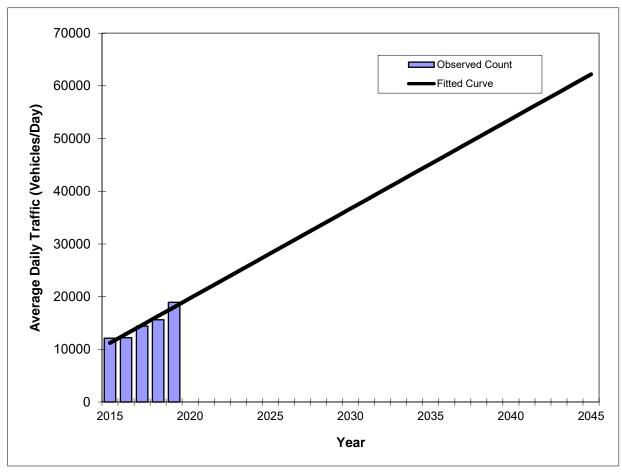
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a S OLD LAKE WILSON -- NORTH OF SINCLAIR ROAD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| County: | Osceola (92) | |
|------------|-------------------|--|
| Station #: | 0 | |
| Highway: | S OLD LAKE WILSON | |



| | Traffic (ADT/AADT) | |
|------|----------------------|----------|
| Year | Count* | Trend** |
| 2015 | 12100 | 11200 |
| 2016 | 12200 | 12900 |
| 2017 | 14400 | 14600 |
| 2018 | 15600 | 16300 |
| 2019 | 18900 | 18000 |
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| 202 | E Opening Vec | r Trond |
| 2025 | 5 Opening Yea N/A | 28200 |
| | 035 Mid-Year T | |
| 2035 | N/A | 45200 |
| | 15 Design Year | |
| 2045 | N/A | 62200 |
| | PLAN Forecas | |
| | LANT OFCCAS | to/Honds |
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| | | 1 |

** Annual Trend Increase: 1,700

Trend R-squared: 91.65%

Trend Annual Historic Growth Rate: 15.18%

Trend Growth Rate (2019 to Design Year): 9.44%

Printed: 17-May-22

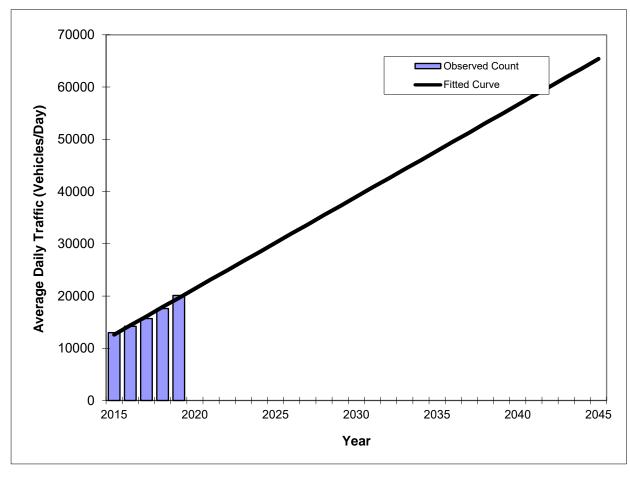
Straight Line Growth Option

*Axle-Adjusted

Traffic Trends - V03.a S OLD LAKE WILSON -- SOUTH OF SINCLAIR RD

| FIN# | 0 |
|----------|---|
| Location | 1 |

| County: | Osceola (92) | |
|------------|-------------------|--|
| Station #: | 0 | |
| Highway: | S OLD LAKE WILSON | |



| | Traffic (ADT/AADT) | |
|------|--------------------|-----------|
| Year | Count* | Trend** |
| 2015 | 13000 | 12600 |
| 2016 | 14200 | 14400 |
| 2017 | 15700 | 16100 |
| 2018 | 17600 | 17900 |
| 2019 | 20100 | 19600 |
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| 202 | 5 Opening Yea | r Trend |
| 2025 | N/A | 30200 |
| | 035 Mid-Year T | |
| 2035 | N/A | 47800 |
| | 15 Design Year | |
| 2045 | N/A | 65400 |
| TRAN | PLAN Forecas | ts/Trends |
| | | |
| | | |

** Annual Trend Increase: 1,760

Trend R-squared: 97.94%

Trend Annual Historic Growth Rate: 13.89%

Trend Growth Rate (2019 to Design Year): 8.99%

Printed: 17-May-22

Straight Line Growth Option

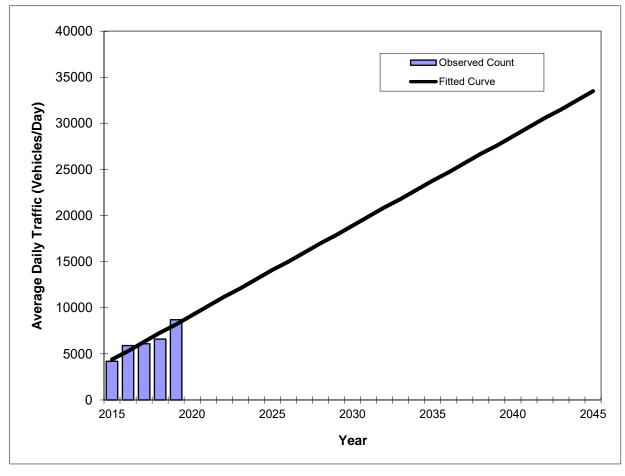
*Axle-Adjusted

Traffic Trends - V03.a SINCLAIR ROAD -- EAST OF SR 429

FIN# 0 Location 1

| | County: | Osceola (92) | |
|------------------------|------------|---------------|--|
| Station #: 0 | Station #: | 0 | |
| Highway: SINCLAIR ROAD | Highway: | SINCLAIR ROAD | |

Traffic (ADT/AADT)



| Year | Count* | Trend** |
|------|----------------|-----------|
| 2015 | 4200 | 4400 |
| 2016 | 5900 | 5300 |
| 2017 | 6100 | 6300 |
| 2018 | 6600 | 7300 |
| 2019 | 8700 | 8200 |
| | | |
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| | | |
| | 5 Opening Yea | |
| 2025 | N/A | 14100 |
| | 035 Mid-Year T | |
| 2035 | N/A | 23800 |
| | 15 Design Year | |
| 2045 | N/A | 33500 |
| TRAN | PLAN Forecas | ts/Trends |
| | | |
| | | |
| | | |

** Annual Trend Increase: 970

Trend R-squared: 89.95%

Trend Annual Historic Growth Rate: 21.59%

Trend Growth Rate (2019 to Design Year): 11.87%

Printed: 17-May-22

Straight Line Growth Option

*Axle-Adjusted

APPENDIX L

TURNS5 Outputs

TURNS5 ANALYSIS SHEET - INPUT

| Analyst: | | | | | — la thia a | 4 way intersection? |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------|-------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Highway: Sinclair Road If not, which 3 approaches exist in the intersection: Tradition Boulevard Enter Yes or No Sinclair Road PD&E EB, WB, and NB EB, SB, and NB EB, WB, AB, Proach NB, Approach NB, | • | | | | _ | • |
| Intersection: Project: Sinclair Road PD&E County: Osceola Is the Mainline iented North/South? K Factors Mainline 9.00% Side street Westbound (NB) Eastbound (EB) Was yes Westbound (EB) Is ther Yes or No If "Yes" go to cell C47 Enter Yes or No If "No" go to cell C3 Enter Year and Growth Rates from Base Year: Year Popening Mid Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From West: From East: From North: From South: From West: From West: From East: From North: From South: Sinclair Road PD&E D East Base Opening Side Street Wainline Mainline Side Street Opening Side Street Opening Side Street Opening Carry Side Street Opening Side Street Decaying Side Street Decaying From West: From East: From North: From South: EB Approach WB Approach NB Approach NB Approach NB Approach TOTAL | Date: | 20-May-22 | <u> </u> | | Yes, m | ny intersection has four approaches |
| Intersection: Project: Sinclair Road PD&E County: Osceola Sinclair Road PD&E Enter Yes or No Sy Yes Northbound (NB) Side street 9.00% Side street Southbound (SB) Southbound (SB) Side Street Westbound (WB) Eastbound (EB) O.00% Side street Southbound (SB) Side street Westbound (WB) Eastbound (EB) O.00% Side street Westbound (EB) O.00% If "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening Opening Mid Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach NB Approach TOTAL Decaying TOTAL EB BB, WB, and NB EB, WB, and NB BB, WB, BB, BB BB, WB, BB, BB, BB BB, BB, WB, BB, BB, BB, BB, BB, BB, BB, | Highway: | | Sinclair Road | | | |
| Sinclair Road PD&E County: Osceola Is the Mainline itented North/South? K Factors Mainline 9.00% Side street 9.00% Side street Westbound (NB) Eastbound (EB) O.0% Side street Westbound (WB) Eastbound (EB) O.0% Fir "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening 2025 Mid 2035 Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: From South: From West: From East: From North: From South: From West: From East: From North: From South: From South: From South: From South From West: From East: From North: From South: From South: From South: From TOTAL From TOTAL From Total EB, WB, and NB EB, SB, and NB E | Intersection: | Tra | adition Boulevard | d | intersectio | _ |
| County: Sthe Mainline Picture Yes or No Picture Yes or No Picture North/South? No No | Project: | Sin | clair Road PD&I | E | | EB, WB, and SB |
| Is the Mainline riented North/South? K Factors Mainline 9.00% Side street 9.00% Side street Westbound (NB) 61.0% Side street Westbound (WB) 61.0% Eastbound (EB) 0.0% U have FTSUTMS Model Year traffic from which you would like to interpolate/extrapolate for project years? (Y/N) If "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening Mid 2035 Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach Opening WB, SB, and NB | | | | _ | | EB, WB, and NB |
| Is the Mainline riented North/South? K Factors Mainline 9.00% Side street 9.00% Side street Westbound (NB) 61.0% Side street Westbound (WB) 61.0% Eastbound (EB) 0.0% Finter Year and Growth Rates from Wich you would like to interpolate/extrapolate for project years? (Y/N) Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening 2025 Opening 2025 Mid 2035 Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | County: | | | | | Ī. |
| No No No No No No No No | Is the Mainline | | | | | WB, SB, and NB |
| K Factors Mainline 9.00% Side street 9.00% Southbound (NB) Southbound (NB) Side street Westbound (WB) Eastbound (EB) 0.0% Westbound (EB) 0.0% If "Yes" go to cell C47 Enter Yes or No If "No" go to cell C3 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening Opening Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach WB Approach WB Approach WB Approach FOTAL From South: TOTAL Time Side Street Adinline Northbound (NB) Side Street Northbound (NB) Side Street Northbound (NB) Side Street Northbound (NB) Side Street Now If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Exponential Decaying TOTAL | | 9 .03 | | | | |
| Side street Southbound (NB) 39.0% 39.0% Side street | nonioa noringodani. | O NO | | | | |
| Side street 9.00% Side street Westbound (WB) Eastbound (EB) O.0% Enter Yes or No interpolate/extrapolate for project years? (Y/N) If "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening Opening Design Design Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach Westbound (SB) 39.0% Side street Westbound (WB) 61.0% Find Yes or No If "No" go to cell C3 Mainline Growth Function Enter Growth Function Exponential Decaying Side Street Growth Function Exponential Decaying Side Street Growth Function Exponential Decaying TOTAL | K Factors | Mainline | ı | D Factors | Main | line |
| ## Side street Westbound (WB) 61.0% 61.0% | | 9.00% | | | 61.0 | 0% |
| Westbound (WB) Eastbound (EB) Ou have FTSUTMS Model Year traffic from which you would like to interpolate/extrapolate for project years? (Y/N) If "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening 2025 Opening Mid 2035 Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | | | Sou | ıthbound (SB) | 39.0 | 0% |
| Enter Yes or No If "Yes" go to cell C47 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base Opening Mid 2035 Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: Enter Yes or No Yes No Mainline Growth Function Enter Side Street Opening Side Street Opening County Function Exponential Decaying Side Street Growth Function Exponential Decaying Side Street Growth Function Exponential Decaying TOTAL | | 9.00% | | _ | | |
| Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base 2021 Mainline Side Street Opening 2025 Mid 2035 0.00% 0.00% Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: Enter Yes or No All Yes No Mainline Growth Function Linear Exponential Decaying Side Street Cyening 2025 Exponential Decaying Side Street Growth Function Exponential Decaying Total | | | | | | |
| Du have FTSUTMS Model Year traffic from which you would like to interpolate/extrapolate for project years? (Y/N) If "Yes" go to cell C47 If "No" go to cell C3 Enter Year and Growth Rates from Base Year: Year Rate (1.0% = 0.01) Base 2021 Mainline Side Street Opening 2025 Mid 2035 0.00% 0.00% Design 2045 Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | | | | | | |
| Base Opening 2025 Mainline Side Street Exponential Decaying Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | | | from which you roject years? (\ | u would like to Y/N) | | Enter Yes or No Yes No |
| Base Opening Mid 2035 0.00% 0.00% Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach Exponential Decaying Side Street Growth Function Exponential Decaying Carbon Decaying Decaying | | | from which you roject years? (\ | u would like to Y/N) | | Enter Yes or No Yes No |
| Opening Mid Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach Decaying Side Street Growth Function — Exponential Decaying TOTAL | interpolate/e | xtrapolate for p | from which you roject years? (\ | u would like to Y/N) If "Yes" go to cell C4 | | Enter Yes or No Yes No If "No" go to cell Ca |
| Mid Design 2045 0.00% 0.00% Side Street Growth Function → Side St | interpolate/e Enter Year a | xtrapolate for p nd Growth Rate Year | from which you roject years? (\ s from Base Ye | u would like to Y/N) If "Yes" go to cell C4 Pear: (1.0% = 0.01) | | Enter Yes or No Yes No If "No" go to cell C3 |
| Design Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach SIde Street Growth Function © Linear Decaying TOTAL | interpolate/e Enter Year al Base | nd Growth Rate Year 2021 | from which you roject years? (\ s from Base Ye | u would like to Y/N) If "Yes" go to cell C4 Pear: (1.0% = 0.01) | | Enter Yes or No Yes No If "No" go to cell C3 |
| Enter Base Year AADTs for Volume Comparison: (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | Enter Year an Base Opening | nd Growth Rate Year 2021 2025 | from which you roject years? (\footnote{\text{N}} s from Base Ye Rate (Mainline | u would like to Y/N) If "Yes" go to cell C4 par: (1.0% = 0.01) Side Street | | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential |
| (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | Enter Year and Base Opening Mid | nd Growth Rate Year 2021 2025 2035 | from which you roject years? (\footnote{\text{N}} s from Base Ye Rate (Mainline | u would like to Y/N) If "Yes" go to cell C4 par: (1.0% = 0.01) Side Street | | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying |
| (growth rates are used to calculate other project years) From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | Enter Year and Base Opening Mid | nd Growth Rate Year 2021 2025 2035 | from which you roject years? (\footnote{\text{N}} s from Base Ye Rate (Mainline | u would like to Y/N) If "Yes" go to cell C4 par: (1.0% = 0.01) Side Street | | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function |
| From West: From East: From North: From South: EB Approach WB Approach SB Approach NB Approach TOTAL | Enter Year at Base Opening Mid Design | nd Growth Rate Year 2021 2025 2035 2045 | from which you roject years? (\) s from Base Ye Rate (Mainline | u would like to Y/N) If "Yes" go to cell C4 Par: (1.0% = 0.01) Side Street 0.00% | | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Linear |
| EB Approach WB Approach SB Approach NB Approach TOTAL | Enter Year at Base Opening Mid Design | nd Growth Rate Year 2021 2025 2035 2045 ear AADTs for N | from which you roject years? (\footnote{\sigma} s from Base Ye Rate (\footnote{\sigma} Mainline 0.00% | u would like to Y/N) If "Yes" go to cell C4 Par: (1.0% = 0.01) Side Street 0.00% | 7 | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Linear Exponential Exponential |
| | Enter Year at Base Opening Mid Design | nd Growth Rate Year 2021 2025 2035 2045 ear AADTs for N | from which you roject years? (\footnote{\sigma} s from Base Ye Rate (\footnote{\sigma} Mainline 0.00% | u would like to Y/N) If "Yes" go to cell C4 Par: (1.0% = 0.01) Side Street 0.00% | 7 | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Linear Exponential Exponential |
| 0 0 0 0 | Enter Year an Base Opening Mid Design Enter Base Y | nd Growth Rate Year 2021 2025 2035 2045 ear AADTs for V | from which you roject years? (\text{\text{N}} & \text{s from Base Ye} & Rate (\text{\text{Mainline}} & 0.00\text{\text{M}} & \text{Volume Compa} & re used to calculate the control of the control | u would like to Y/N) If "Yes" go to cell C4 Par: (1.0% = 0.01) Side Street 0.00% Urison: late other project | 7 | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Linear Exponential Exponential |
| | Enter Year and Base Opening Mid Design Enter Base Y | nd Growth Rate Year 2021 2025 2035 2045 ear AADTs for V (growth rates a | from which you roject years? (\) s from Base Ye Rate (\) Mainline 0.00% Volume Compa re used to calculate the control of the compa | u would like to Y/N) If "Yes" go to cell C4 ear: (1.0% = 0.01) Side Street 0.00% Irison: Idate other project | rt years) | Enter Yes or No Yes No If "No" go to cell C3 Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Exponential Exponential Decaying |
| | Enter Year an Base Opening Mid Design Enter Base Y | nd Growth Rate Year 2021 2025 2035 2045 ear AADTs for V | from which you roject years? (\text{\text{N}} & \text{s from Base Ye} & Rate (\text{\text{Mainline}} & 0.00\text{\text{M}} & \text{Volume Compa} & re used to calculate the control of the control | u would like to Y/N) If "Yes" go to cell C4 Par: (1.0% = 0.01) Side Street 0.00% Urison: late other project | 7 | Enter Yes or No Yes No If "No" go to cell C Mainline Growth Function Linear Exponential Decaying Side Street Growth Function Linear Exponential Exponential |

| | Year |
|---------|------|
| Base | 2021 |
| Opening | 2025 |
| Mid | 2035 |
| Design | 2045 |
| Model | 2045 |

Enter Base and Model Year AADTs for Volume Comparison: (volumes for other project years are calculated by interpolation)

| | From West: | From East: | From North: | From South: | |
|------|-------------|-------------|-------------|-------------|-------|
| | EB Approach | WB Approach | SB Approach | NB Approach | TOTAL |
| 2021 | 0 | 3500 | 3500 | 0 | 7000 |
| 2045 | 0 | 12000 | 22500 | 17500 | 52000 |

| | | 1st Guess urning %'s for ADT Balancing | Actual/Count Traffic for 2021 | red | First Guess Turning % Option Used FSUTMS Model Year AADTs |
|--------------------------------------------------------------------|-------------------------------------------------------------------------------------|--------------------------------------------------|-------------------------------------|----------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------|
| (EB LT) (EB THRU) (EB RT) | West-to-North West-to-East West-to-South | 0.0% 0.0% 0.0% | 0 0 0 | Existing Year AADTs | Only the existing year total departure volumes [AADT*K*(1-D)] will be used to calculate the |
| (WB LT) (WB THRU) (WB RT) (SB LT) (SB THRU) (SB RT) | East-to-South East-to-West East-to-North North-to-East North-to-South North-to-West | 33.2% 0.0% 66.8% 40.7% 59.3% 0.0% | 0 0 0 | Existing Turning Movement Counts | The turning percentages first guess is the same as the <u>actual</u> <u>distribution of turning volumes</u> <u>entered</u> . No balancing technique is used. |
| (NB LT) (NB THRU) (NB RT) Desired Clos | South-to-West South-to-North South-to-East ure: | 0.0% 74.6% 25.4% | 0 0 0 | FSUTMS Model Year AADTs | Only the FSUTMS model year departure volumes [AADT*K*(1-D)] will be used to calculate the turning percentages first guess. |

TURNS5 INITIAL TURNING VOLUME SUMMARY

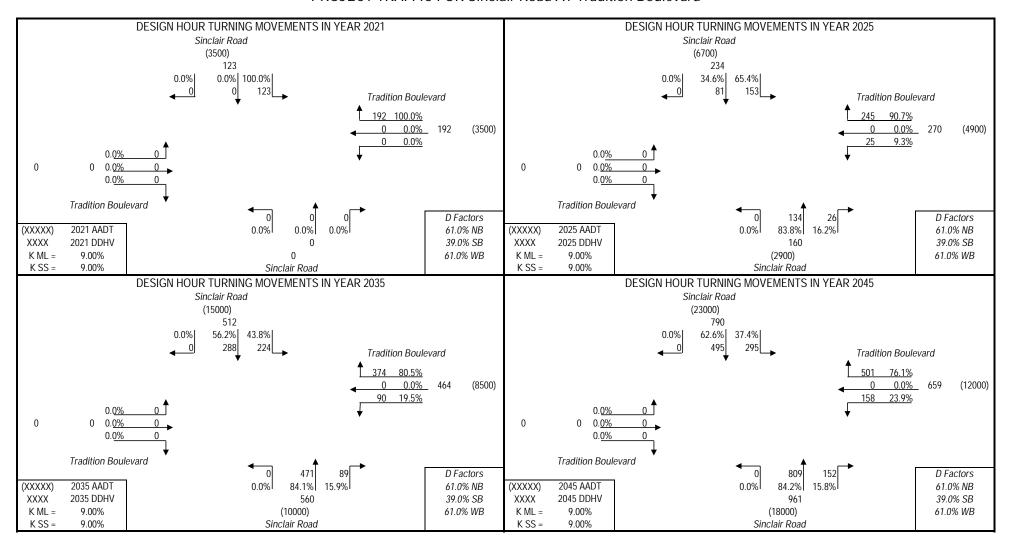
Highway: Sinclair Road County: Osceola

Intersection: Tradition Boulevard
Project: Sinclair Road PD&E Analyst: KHA

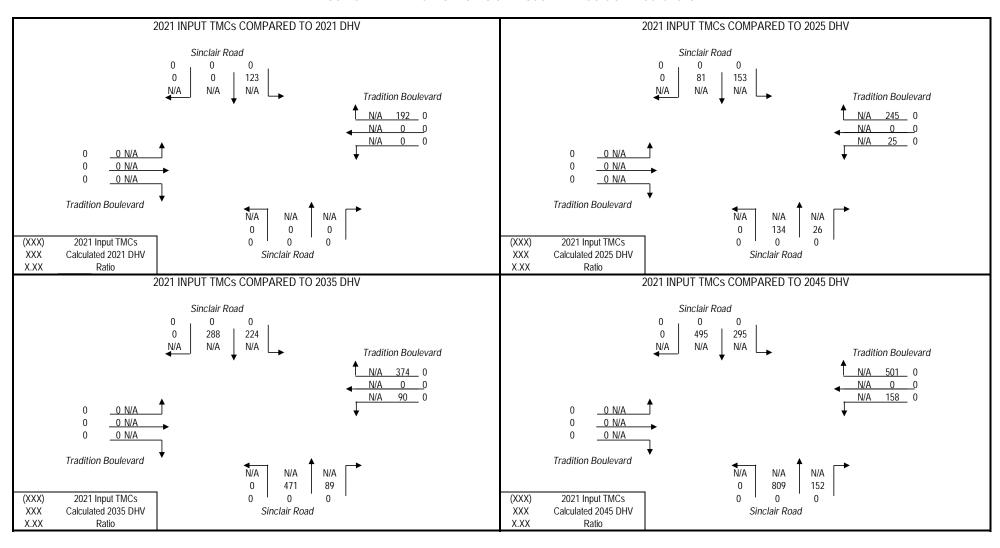
Date: 20-May-22

| | 2021 | 2 | 2021 | 2 | 025 | 2 | 2035 | 20 |)45 |
|--------------------------|---------------------|-------------------|----------------------|-------------------|-------------------|-------------------|----------------------|-------------------|----------------------|
| Approach-To- Approach | Initial Estimate | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume |
| | | | | | | | _ | | |
| West-To-North (LT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| West-To-East (Thru) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| West-To-South (RT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| Total Flow From W | est: | | 0 | | 0 | | 0 | | 0 |
| | | | | | | | | ì | |
| East-To-South (LT) | 0.332 | 0.000 | 0 | 0.093 | 25 | 0.195 | 90 | 0.239 | 158 |
| East-To-West (Thru) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| East-To-North (RT) | 0.668 | 1.000 | 192 | 0.907 | 245 | 0.805 | 374 | 0.761 | 501 |
| Total Flow From Ea | ıst: | | 192 | | 270 | | 464 | | 659 |
| 1010111011120 | | | | | | | | | |
| North-To-East (LT) | 0.407 | 1.000 | 123 | 0.654 | 153 | 0.438 | 224 | 0.374 | 295 |
| North-To-South (Thru) | 0.593 | 0.000 | 0 | 0.346 | 81 | 0.562 | 288 | 0.626 | 495 |
| North-To-West (RT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| Total Flow From No | orth: | | 123 | | 234 | | 512 | | 790 |
| | | | | | | | * | | |
| South-To-West (LT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| South-To-North (Thru) | 0.746 | 0.000 | 0 | 0.838 | 134 | 0.841 | 471 | 0.842 | 809 |
| South-To-East (RT) | 0.254 | 0.000 | 0 | 0.162 | 26 | 0.159 | 89 | 0.158 | 152 |
| Total Flow From So | vuth: | | 0 | | 160 | | 560 | | 961 |
| Total Flow Floil Sc | Julii. | | U | | 100 | | 300 | | 301 |

PROJECT TRAFFIC FOR Sinclair Road AT Tradition Boulevard



PROJECT TRAFFIC FOR Sinclair Road AT Tradition Boulevard



TURNS5 ANALYSIS SHEET - INPUT

| | 10.1.100 | , , ., , , <u>, , , , , , , , , , , , , , </u> | <u></u> |
|-----------------------|-----------------|------------------------------------------------------------------------------|---------------------------------------------------|
| | | | |
| Analyst: | | KHA | Is this a 4 way intersection? |
| Date: | 20-May-22 | | Yes, my intersection has four approaches |
| Highway: | Ş | Sinclair Road | If not, which 3 approaches exist in the |
| Intersection: | Trac | dition Boulevard | intersection? |
| Project: | Sinc | lair Road PD&E | EB, WB, and SB |
| | Sinc | iali Road PD&E | EB, WB, and NB |
| County: | | Osceola | ○ EB, SB, and NB |
| | Enter Yes or No | | WB, SB, and NB |
| Is the Mainline | Yes | | |
| Oriented North/South? | ○ No | | |
| K Factors | Mainline | D Factors | Mainline |
| K Factors | 9.00% | Northbound (NB) | 39.0% |
| | Side street | Southbound (SB) | 61.0% |
| | 9.00% | 004111004114 (02) | Side street |
| | | Westbound (WB) | 39.0% |
| | | Eastbound (EB) | 0.0% |
| • | | rom which you would like to oject years? (Y/N) If "Yes" go to cell C47 | Enter Yes or No Yes No If "No" go to cell C31 |
| Base | Year 2021 | from Base Year: Rate (1.0% = 0.01) Mainline Side Street | Mainline Growth Function © Linear C Exponential |
| Opening | 2025 | | O Decaving |

| Enter Year ar | nd Growth Rates | Mainline Growth Function | | | |
|---------------|------------------|--------------------------|---------------|---------------|-----------------------------|
| | Year | Rate | (1.0% = 0.01) | | Linear |
| Base | 2021 | Mainline | Side Street | _ | ○ Exponential |
| Opening | 2025 | | | | Decaying |
| Mid | 2035 | 0.00% | 0.00% | | 0 , 0 |
| Design | 2045 | | | | Side Street Growth Function |
| | • | | - | | Linear |
| Enter Base Y | ear AADTs for \ | /olume Comp | arison: | ○ Exponential | |
| | (growth rates ar | re used to calc | O Decaying | | |
| | | | | | |
| From West: | From East: | From North: | From South: | | |
| EB Approach | WB Approach | SB Approach | NB Approach | тот | AL |
| 0 | 0 | 0 | 0 | 0 | |

Enter Project and Model Years

| | Year |
|---------|------|
| Base | 2021 |
| Opening | 2025 |
| Mid | 2035 |
| Design | 2045 |
| Model | 2045 |

Enter Base and Model Year AADTs for Volume Comparison: (volumes for other project years are calculated by interpolation)

| | From West: | From East: | From North: | From South: | |
|------|-------------|-------------|-------------|-------------|-------|
| | EB Approach | WB Approach | SB Approach | NB Approach | TOTAL |
| 2021 | 0 | 3500 | 3500 | 0 | 7000 |
| 2045 | 0 | 12000 | 22500 | 17500 | 52000 |
| | | | | | |

| | 1st Guess Turning %'s for AADT Balancing | Actual/Count Traffic for 2021 | ted | First Guess Turning % Option Used FSUTMS Model Year AADTs |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------|-------------------------------------|----------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------|
| (EB LT) West-to-North (EB THRU) West-to-East (EB RT) West-to-South | 0.0% 0.0% | 0 0 0 | Existing Year AADTs | Only the existing year total departure volumes [AADT*K*(1-D)] will be used to calculate the |
| (WB LT) East-to-South (WB THRU) East-to-West (WB RT) East-to-North (SB LT) North-to-East (SB THRU) North-to-South (SB RT) North-to-West | | 0 0 0 | Existing Turning Movement Counts | The turning percentages first guess is the same as the <u>actual</u> <u>distribution of turning volumes</u> <u>entered</u> . No balancing technique is used. |
| (NB LT) South-to-Wes (NB THRU) South-to-Norti (NB RT) South-to-East Desired Closure: | | 0 0 | FSUTMS Model Year AADTs | Only the FSUTMS model year departure volumes [AADT*K*(1-D)] will be used to calculate the turning percentages first guess. |

TURNS5 INITIAL TURNING VOLUME SUMMARY

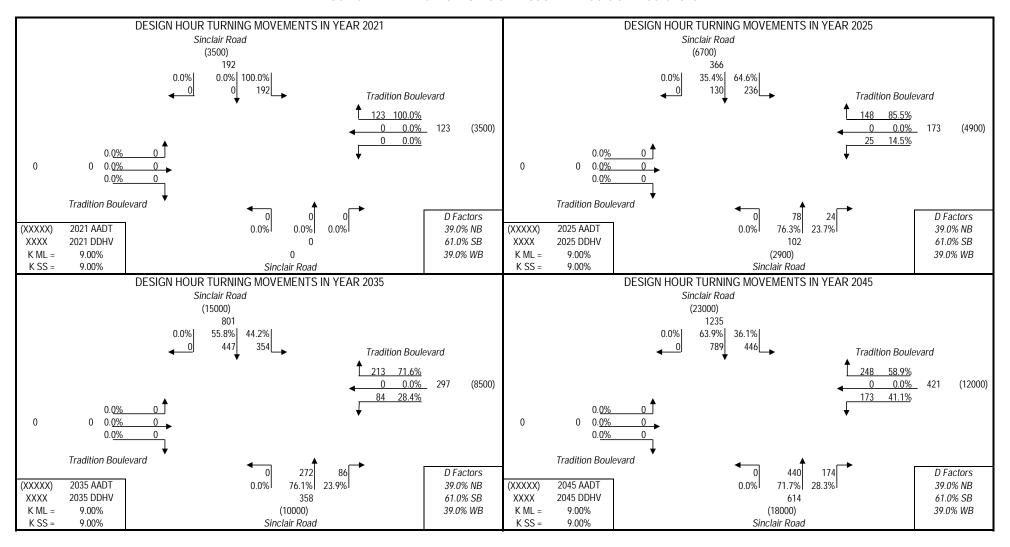
Highway: Sinclair Road County: Osceola

Intersection: Tradition Boulevard
Project: Sinclair Road PD&E Analyst: KHA

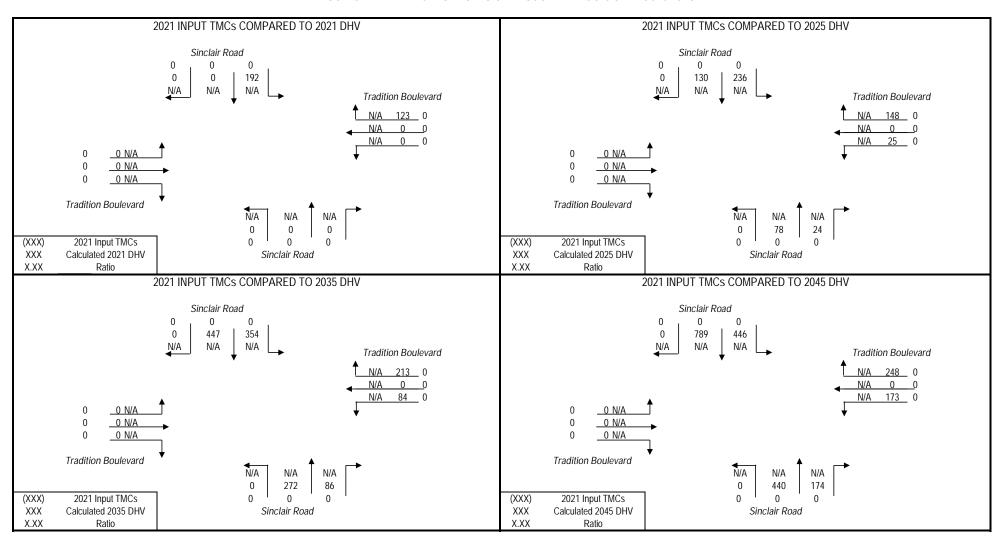
Date: 20-May-22

| | 2021 | 2 | 2021 | 2 | 025 | 2 | 2035 | 20 |)45 |
|----------------------------------------|---------------------|-------------------|----------------------|-------------------|-------------------|-------------------|----------------------|-------------------|----------------------|
| Approach-To- Approach | Initial Estimate | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume |
| Most To North (LT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| West-To-North (LT) West-To-East (Thru) | 0.000 | 0.000 | 0 | 0.000 0.000 | 0 0 | 0.000 | 0 | 0.000 | 0 0 |
| West-To-South (RT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| | | | - | | _ | | - | | _ |
| Total Flow From W | est: | | 0 | | 0 | | 0 | | 0 |
| | | | | | | | | | |
| East-To-South (LT) | 0.549 | 0.000 | 0 | 0.145 | 25 | 0.284 | 84 | 0.411 | 173 |
| East-To-West (Thru) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| East-To-North (RT) | 0.451 | 1.000 | 123 | 0.855 | 148 | 0.716 | 213 | 0.589 | 248 |
| Total Flow From Ea | ıst: | | 123 | | 173 | | 297 | | 421 |
| | | | | | | | | | |
| North-To-East (LT) | 0.407 | 1.000 | 192 | 0.646 | 236 | 0.442 | 354 | 0.361 | 446 |
| North-To-South (Thru) | 0.593 | 0.000 | 0 | 0.354 | 130 | 0.558 | 447 | 0.639 | 789 |
| North-To-West (RT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| Total Flow From No | orth: | | 192 | | 366 | | 801 | | 1235 |
| | | | | | | | | | |
| South-To-West (LT) | 0.000 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 | 0.000 | 0 |
| South-To-North (Thru) | 0.545 | 0.000 | 0 | 0.763 | 78 | 0.761 | 272 | 0.717 | 440 |
| South-To-East (RT) | 0.455 | 0.000 | 0 | 0.237 | 24 | 0.239 | 86 | 0.283 | 174 |
| Total Flow From South: | | | 0 | | 102 | | 358 | | 614 |

PROJECT TRAFFIC FOR Sinclair Road AT Tradition Boulevard



PROJECT TRAFFIC FOR Sinclair Road AT Tradition Boulevard



TURNS5 ANALYSIS SHEET - INPUT

| Analyst: | KHA | | Is this a 4 way intersection? |
|-----------------------|-------------------|-----------------|------------------------------------------|
| Date: | 20-May-22 | | Yes, my intersection has four approaches |
| Highway: | Sinclair Rd/Bella | Citta Blvd | If not, which 3 approaches exist in the |
| Intersection: | Goodman | ı Rd | intersection? |
| Project: | Sinclair Road | IDD8E | EB, WB, and SB |
| | Siliciali Ruad | IFDAE | EB, WB, and NB |
| County: | Osceol | a | ○ EB, SB, and NB |
| | Enter Yes or No | 7 | ○ WB, SB, and NB |
| Is the Mainline | ○ Yes | | |
| Oriented North/South? | ● No | | |
| W.F | Maria Para | D.F t | A 4 - to Bar |
| K Factors | Mainline | D Factors | Mainline |
| | 9.00% | Westbound (WB) | 39.0% |
| | Side street | Eastbound (EB) | 61.0% |
| | 9.00% | | Side street |
| | | Northbound (NB) | 49.0% |
| | | Southbound (SB) | 51.0% |
| | | | |
| | | | |
| | | | |

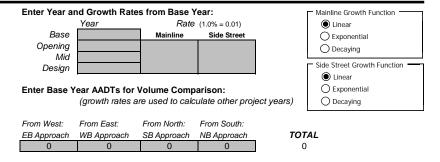
Do you have FTSUTMS Model Year traffic from which you would like to interpolate/extrapolate for project years? (Y/N)

Enter Yes or No

Yes
No

If "Yes" go to cell C47

If "No" go to cell C31



Enter Project and Model Years

| Year | | | | | | |
|---------|------|--|--|--|--|--|
| Base | 2021 | | | | | |
| Opening | 2025 | | | | | |
| Mid | 2035 | | | | | |
| Design | 2045 | | | | | |
| Model | 2045 | | | | | |

Enter Base and Model Year AADTs for Volume Comparison:

(volumes for other project years are calculated by interpolation)

| | From West: | From East: | From North: | From South: | |
|------|-------------|-------------|-------------|-------------|-------|
| | EB Approach | WB Approach | SB Approach | NB Approach | TOTAL |
| 2021 | 9000 | 0 | 4400 | 11000 | 24400 |
| 2045 | 17000 | 17500 | 5000 | 14500 | 54000 |

| | | 1st Guess urning %'s for ADT Balancing | Actual/Counted Traffic for 2021 | d | First Guess Turning % Option Used FSUTMS Model Year AADTs |
|-----------------------------------------|--------------------------------------------------|----------------------------------------------|---------------------------------------|----------------------------|----------------------------------------------------------------------------------------------------------------------------|
| (EB LT) (EB THRU) (EB RT) | West-to-North West-to-East West-to-South | 11.9% 52.1% 36.0% | 61 0 303 | Existing Year AADTs | Only the existing year total departure volumes [AADT*K*(1-D)] will be used to calculate the |
| (WB LT) (WB THRU) (WB RT) | East-to-South East-to-West East-to-North | 44.9% 40.2% 14.9% | 0 0 | Existing Turning Movement | turning percentages first guess. The turning percentages first guess is the same as the <u>actual</u> |
| (SB LT) (SB THRU) (SB RT) | North-to-East North-to-South North-to-West | 43.2% 30.0% 26.8% | 0 63 33 | Counts | distribution of turning volumes entered. No balancing technique is used. |
| (NB LT) (NB THRU) (NB RT) Desired Clos | South-to-West South-to-North South-to-East | 33.6% 12.4% 54.0% | 201 123 0 | FSUTMS Model Year AADTs | Only the FSUTMS model year departure volumes [AADT*K*(1-D)] will be used to calculate the turning percentages first guess. |

TURNS5 INITIAL TURNING VOLUME SUMMARY

Highway: Sinclair Rd/Bella Citta Blvd

Intersection: Goodman Rd

Project: Sinclair Road PD&E Analyst: KHA

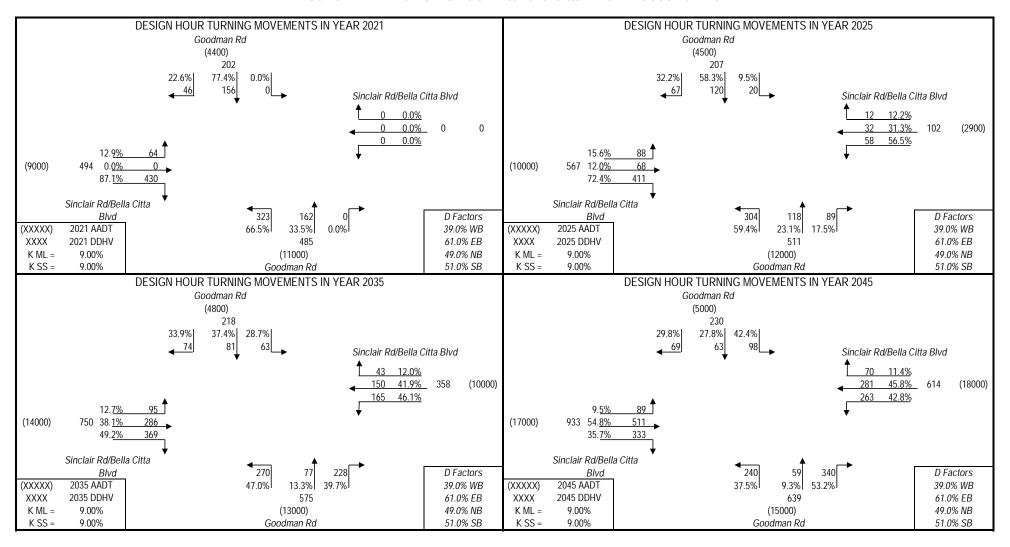
Date: 20-May-22

Osceola

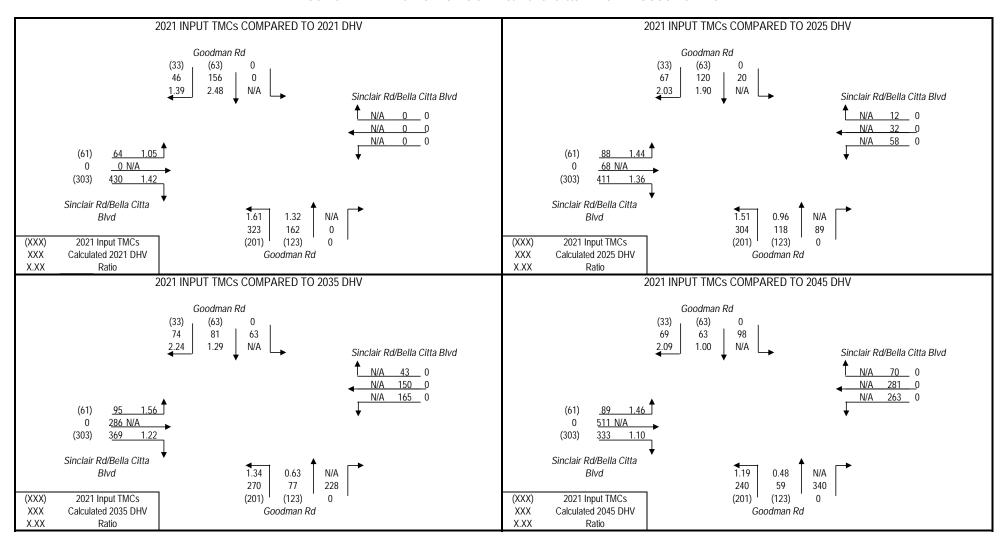
County:

| | 2021 | 2021 | | 2 | 025 | 4 | 2035 | 20 |)45 |
|------------------------------------------|---------------------|-------------------|----------------------|-------------------|-------------------|-------------------|----------------------|-------------------|----------------------|
| Approach-To- Approach | Initial Estimate | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume |
| West-To-North (LT) | 0.119 | 0.129 | 64 | 0.156 | 88 | 0.127 | 95 | 0.095 | 89 |
| West-To-East (Thru) | 0.521 | 0.000 | 0 | 0.120 | 68 | 0.381 | 286 | 0.548 | 511 |
| West-To-South (RT) | 0.360 | 0.871 | 430 | 0.724 | 411 | 0.492 | 369 | 0.357 | 333 |
| Total Flow From We | est: | | 494 | | 567 | | 750 | | 933 |
| E . T . O ! . (1. T) | 0.440 | | • | | | 2 121 | 105 | 2.422 | |
| East-To-South (LT) | 0.449 | 0.000 | 0 | 0.565 | 58 | 0.461 | 165 | 0.428 | 263 |
| East-To-West (Thru) | 0.402 | 0.000 | 0 | 0.313 | 32 | 0.419 | 150 | 0.458 | 281 |
| East-To-North (RT) | 0.149 | 0.000 | 0 | 0.122 | 12 | 0.120 | 43 | 0.114 | 70 |
| Total Flow From Ea | ıst: | | 0 | | 102 | | 358 | | 614 |
| North To Foot (LT) | 0.432 | 0.000 | 0 | 0.095 | 20 | 0.287 | 63 | 0.424 | 98 |
| North-To-East (LT) North-To-South (Thru) | 0.432 | 0.000 | 0 156 | 0.095 | 120 | 0.267 | 81 | 0.424 | 98 63 |
| North-To-West (RT) | 0.300 | 0.774 | 46 | 0.363 | 67 | 0.374 | 74 | 0.278 | 69 |
| Notth-10-West (K1) | 0.200 | 0.220 | 40 | 0.322 | 07 | 0.339 | 74 | 0.290 | 09 |
| Total Flow From No | orth: | | 202 | | 207 | | 218 | | 230 |
| South-To-West (LT) | 0.336 | 0.665 | 323 | 0.594 | 304 | 0.470 | 270 | 0.375 | 240 |
| South-To-West (E1) | 0.330 | 0.003 | 162 | 0.394 | 118 | 0.470 | 270 77 | 0.093 | 59 |
| South-To-East (RT) | 0.124 | 0.000 | 0 | 0.231 | 89 | 0.133 | 228 | 0.532 | 340 |
| Coddi To Edot (ICT) | 0.040 | 0.000 | U | 0.170 | 00 | 0.007 | 220 | 0.002 | 070 |
| Total Flow From So | outh: | | 485 | | 511 | | 575 | | 639 |

PROJECT TRAFFIC FOR Sinclair Rd/Bella Citta Blvd AT Goodman Rd



PROJECT TRAFFIC FOR Sinclair Rd/Bella Citta Blvd AT Goodman Rd



TURNS5 ANALYSIS SHEET - INPUT

| Analyst: | KHA | | Is this a 4 way intersection? |
|-----------------------|-------------------|-----------------|------------------------------------------|
| Date: | 20-May-22 | | Yes, my intersection has four approaches |
| Highway: | Sinclair Rd/Bella | Citta Blvd | If not, which 3 approaches exist in the |
| Intersection: | Goodman | Rd | intersection? |
| Project: | Sinclair Road | I PD&F | EB, WB, and SB |
| | | | EB, WB, and NB |
| County: | Osceol | a | ○ EB, SB, and NB |
| Is the Mainline | Enter Yes or No | | ○ WB, SB, and NB |
| Oriented North/South? | O 163 | | |
| Oriented North/South? | ● No | | |
| K Factors | Mainline | D Factors | Mainline |
| | 9.00% | Westbound (WB) | 53.0% |
| | Side street | Eastbound (EB) | 47.0% |
| | 9.00% | _ | Side street |
| | | Northbound (NB) | 30.0% |
| | | Southbound (SB) | 70.0% |
| | | | |
| | | | |

Do you have FTSUTMS Model Year traffic from which you would like to interpolate/extrapolate for project years? (Y/N)

Enter Yes or No

Yes
No

If "Yes" go to cell C47

If "No" go to cell C31

Enter Year and Growth Rates from Base Year: Mainline Growth Function Linear Rate (1.0% = 0.01) Mainline Base Side Street O Exponential Opening Oecaying Mid Side Street Growth Function Design Linear Enter Base Year AADTs for Volume Comparison: O Exponential (growth rates are used to calculate other project years) O Decaying From West: From North: From South: WB Approach TOTAL EB Approach SB Approach NB Approach 0

Enter Project and Model Years

| Year | | | | | | | |
|---------|------|--|--|--|--|--|--|
| Base | 2021 | | | | | | |
| Opening | 2025 | | | | | | |
| Mid | 2035 | | | | | | |
| Design | 2045 | | | | | | |
| Model | 2045 | | | | | | |

Enter Base and Model Year AADTs for Volume Comparison:

(volumes for other project years are calculated by interpolation)

| | From West: | From East: | From North: | From South: | |
|------|-------------|-------------|-------------|-------------|-------|
| | EB Approach | WB Approach | SB Approach | NB Approach | TOTAL |
| 2021 | 9000 | 0 | 4400 | 11000 | 24400 |
| 2045 | 17000 | 17500 | 5000 | 14500 | 54000 |

| | | 1st Guess urning %'s for ADT Balancing | Actual/Counter Traffic for 2021 | d | First Guess Turning % Option Used FSUTMS Model Year AADTs |
|---------------------------------|--------------------------------------------------|----------------------------------------------|---------------------------------------|----------------------------|------------------------------------------------------------------------------------------------------------------------------|
| (EB LT) (EB THRU) (EB RT) | West-to-North West-to-East West-to-South | 7.5% 41.4% 51.1% | 17 0 273 | Existing Year AADTs | Only the existing year total departure volumes [AADT*K*(1-D)] will be used to calculate the turning percentages first quess. |
| (WB LT) (WB THRU) (WB RT) | East-to-South East-to-West East-to-North | 49.1% 43.6% 7.3% | 0 0 0 | Existing Turning | The turning percentages first guess is the same as the <u>actual</u> |
| (SB LT) (SB THRU) (SB RT) | North-to-East North-to-South North-to-West | 30.0% 37.1% 32.9% | 0 340 114 | Movement Counts | <u>distribution of turning volumes</u> <u>entered</u> . No balancing technique is used. |
| (NB LT) (NB THRU) (NB RT) | South-to-West South-to-North South-to-East | 48.1% 8.0% 43.9% | 210 92 0 | FSUTMS Model Year AADTs | Only the FSUTMS model year departure volumes [AADT*K*(1-D)] will be used to calculate the turning percentages first guess. |

TURNS5 INITIAL TURNING VOLUME SUMMARY

Highway: Sinclair Rd/Bella Citta Blvd

Intersection: Goodman Rd

Project: Sinclair Road PD&E Analyst:

Date: 20-May-22

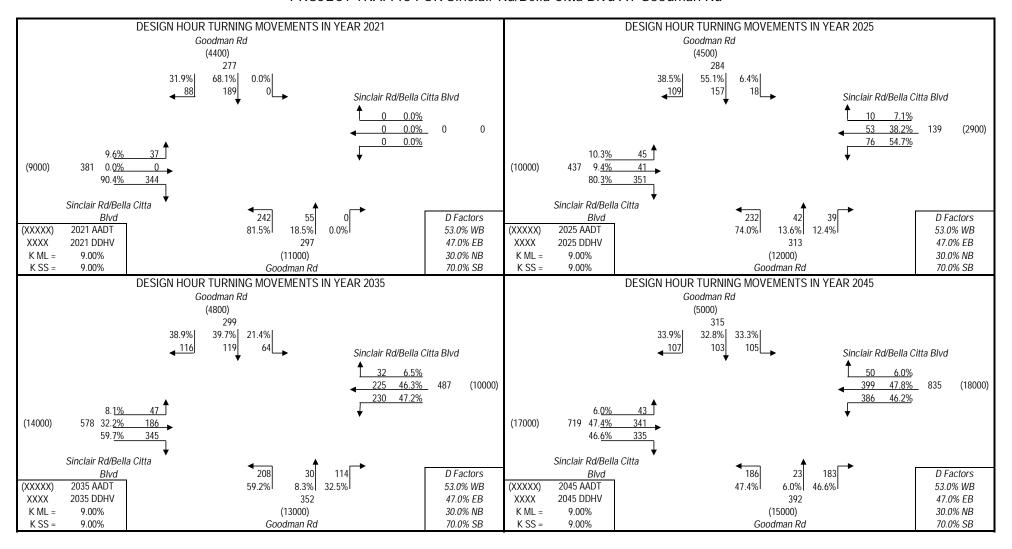
Osceola

KHA

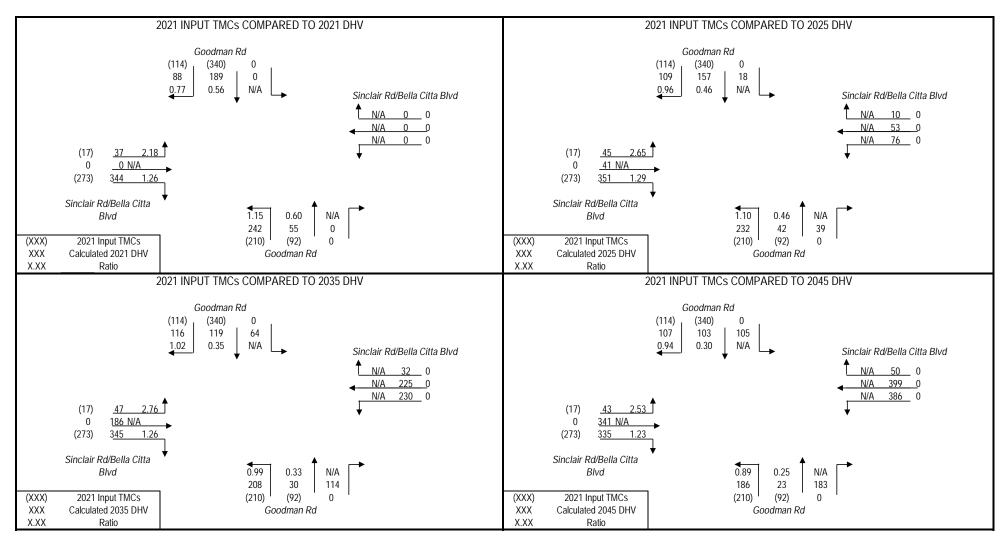
County:

| | 2021 | 2 | 2021 | 2 | 025 | | 2035 | 20 |)45 |
|--------------------------|---------------------|-------------------|----------------------|-------------------|-------------------|-------------------|----------------------|-------------------|----------------------|
| Approach-To- Approach | Initial Estimate | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume | Final Estimate | Calculated Volume |
| West-To-North (LT) | 0.075 | 0.096 | 37 | 0.103 | 45 | 0.081 | 47 | 0.060 | 43 |
| West-To-East (Thru) | 0.414 | 0.000 | 0 | 0.103 | 41 | 0.322 | 186 | 0.474 | 341 |
| West-To-South (RT) | 0.511 | 0.904 | 344 | 0.803 | 351 | 0.597 | 345 | 0.466 | 335 |
| Total Flow From W | est: | | 381 | | 437 | | 578 | | 719 |
| | | | | | - | | | | - |
| East-To-South (LT) | 0.491 | 0.000 | 0 | 0.547 | 76 | 0.472 | 230 | 0.462 | 386 |
| East-To-West (Thru) | 0.436 | 0.000 | 0 | 0.382 | 53 | 0.463 | 225 | 0.478 | 399 |
| East-To-North (RT) | 0.073 | 0.000 | 0 | 0.071 | 10 | 0.065 | 32 | 0.060 | 50 |
| Total Flow From Ea | ıst: | | 0 | | 139 | | 487 | | 835 |
| | | | | | | | | | |
| North-To-East (LT) | 0.300 | 0.000 | 0 | 0.064 | 18 | 0.214 | 64 | 0.333 | 105 |
| North-To-South (Thru) | 0.371 | 0.681 | 189 | 0.551 | 157 | 0.397 | 119 | 0.328 | 103 |
| North-To-West (RT) | 0.329 | 0.319 | 88 | 0.385 | 109 | 0.389 | 116 | 0.339 | 107 |
| Total Flow From No | orth: | | 277 | | 284 | | 299 | | 315 |
| O . (I. T. W (I.T.) | 0.404 | 0.045 | 0.10 | 0.740 | 000 | 0.500 | | 0.474 | 400 |
| South-To-West (LT) | 0.481 | 0.815 | 242 | 0.740 | 232 | 0.592 | 208 | 0.474 | 186 |
| South-To-North (Thru) | 0.080 | 0.185 | 55 | 0.136 | 42 | 0.083 | 30 | 0.060 | 23 |
| South-To-East (RT) | 0.439 | 0.000 | 0 | 0.124 | 39 | 0.325 | 114 | 0.466 | 183 |
| Total Flow From Sc | outh: | | 297 | | 313 | | 352 | | 392 |

PROJECT TRAFFIC FOR Sinclair Rd/Bella Citta Blvd AT Goodman Rd



PROJECT TRAFFIC FOR Sinclair Rd/Bella Citta Blvd AT Goodman Rd



| APPENDIX M | |
|-----------------------------------------------------------------|--|
| Sinclair Road Preliminary Traffic Analysis Technical Memorandum | |
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MEMORANDUM

To: Conroy Jacobs, AICP, MPA

Transportation & Transit Department

Osceola County

From: James M. Taylor, P.E.

Kimley-Horn and Associates, Inc.

Date: May 23, 2022

Subject: Sinclair Road Extension Preliminary Traffic Evaluation

Introduction

This memorandum summarizes the development of 2045 average annual daily traffic (AADT) volumes and peak hour turning movement volumes (TMVs) at the intersections of Sinclair Road Extension with Goodman Road and Tradition Boulevard. These TMVs were used to develop lane requirements at these two intersections. This information will be incorporated into the more detailed Project Traffic Analysis Report (PTAR). This analysis was performed consistent with the approved PTAR Methodology.

Existing (2021) Traffic Volumes

Daily roadway volumes were collected at the study roadway segments during three (3) consecutive days from Tuesday, November 16, 2021, to Thursday, November 18, 2021. The average volume during the three days was calculated and adjusted by applying the seasonal factor (SF) published in the Florida Department of Transportation (FDOT) Florida Traffic Online (FTO) database for the volumes were collected. **Table 1** shows a summary of the adjusted Average Annual Daily Traffic (AADT) for each segment. **Figure 1** depicts the existing AADT.

Table 1: Existing Average Annual Daily Traffic (AADT)

| Roadway Segment | Į. | Average Daily | / Traffic (ADT |) | SF ¹ | Adjusted | Adjusted AADT |
|--------------------------------|--------|---------------|----------------|---------|-----------------|----------|------------------|
| Roadway Segment | Day 1 | Day 2 | Day 3 | Average | 3 F | AADT | (Rounded |
| Happy Trails | | | | | | | |
| west of Sinclair Road | 820 | 794 | 869 | 828 | | 795 | 800 |
| Sinclair Road | | | | | | | |
| north of Tradition Boulevard | 3,480 | 3,484 | 4,062 | 3,675 | | 3,528 | 3,500 |
| Bella Citta Boulevard | | | | | 0.96 | | |
| west of S Goodman Road | 9,129 | 9,005 | 10,077 | 9,404 | | 9,028 | 9,000 |
| S Goodman Rd | | | | | | | |
| north of Bella Citta Boulevard | 4,524 | 4,308 | 4,849 | 4,560 | | 4,378 | 4,400 |
| south of Bella Citta Boulevard | 11,115 | 11,091 | 12,071 | 11,426 | | 10,969 | 11,000 |

Notes:

1. Per FDOT's Florida Traffic Online for Osceola County



The eight (8) highest hours during the day were determined and used to collect turning movement counts (TMC) at the study intersections. The eight highest hours occur from 7:00 AM to 11:00 AM and from 2:00 PM to 6:00 PM. Existing volumes were adjusted by applying the seasonal factor (SF) published in the Florida Traffic Online (FTO) database for the week turning movement counts were collected. Raw existing traffic volumes are provided in the **Attachments**. Adjusted existing (2021) AM and PM peak hour turning movement volumes are shown in **Figure 2**.

Model Calibration

The latest adopted Central Florida Regional Planning Model (CFRPM v7) was used to forecast unadjusted horizon year (2045) daily traffic volumes at the future intersection approaches. The base year 2015 model was reviewed by comparing the model volumes to the historic counts on nearby roadway segments within the study area. The model showed to underrepresent the volumes along Goodman Road south of Bella Citta Boulevard and Bella Citta Boulevard west of Goodman Road. This observation was taken into account when developing year 2045 volumes as described in the subsequent section. No modifications were made in the model to roadway segment attributes (speed, area type, facility type, etc.). **Figure 3** shows a comparison of the base year 2015 model volumes and 2015 historical volumes.

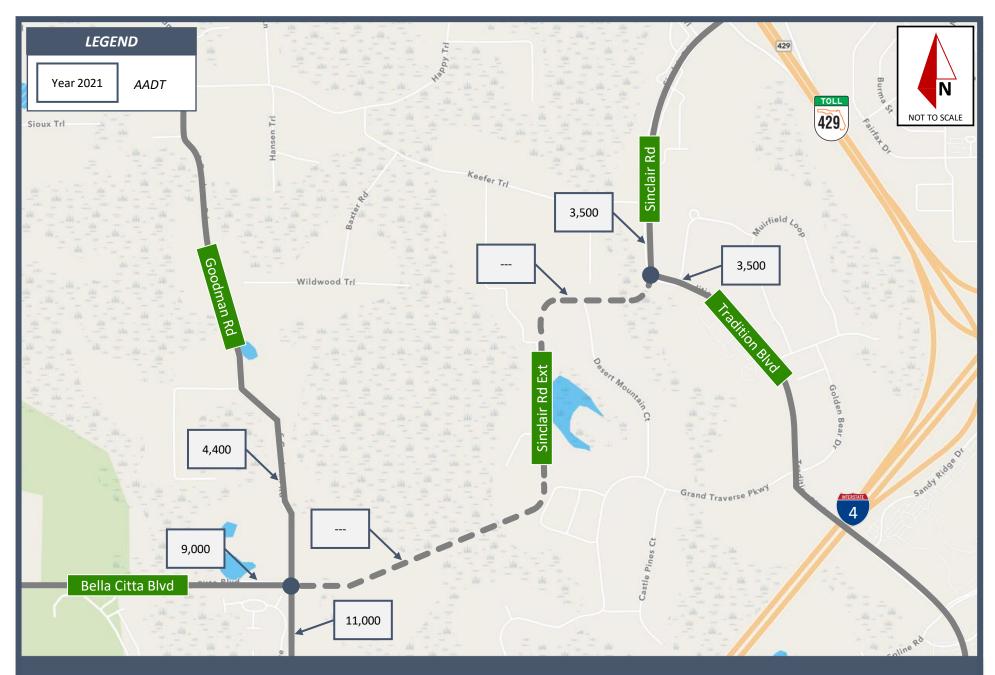


Figure 1: Existing (2021) Average Daily Traffic (ADT)
Sinclair Road Extension | Preliminary Traffic Evaluation

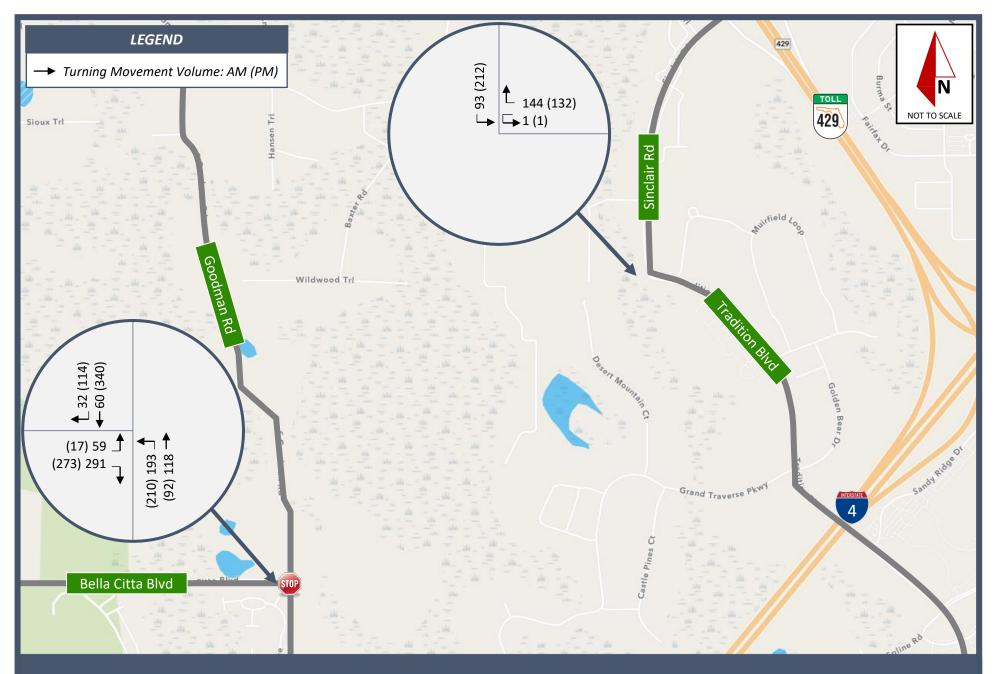


Figure 2: Existing (2021) Intersection Turning Movement Volumes
Sinclair Road Extension | Preliminary Traffic Evaluation



Figure 3: Base (2015) Model Volumes vs. Year 2015 Historical Volumes Sinclair Road Extension | Preliminary Traffic Evaluation



Project 2045 AADT's

The Cost Feasible (CF) 2045 roadway network and socioeconomic data (ZDATA) were reviewed to determine if all known roadway projects and existing/future developments (Reunion, Goodman Road Charter School, Elevation/Dewan Property, Sinclair Road Property, and Illuminate Church) were accounted for. The resulting revisions made to the CF 2045 roadway network and ZDATA are listed below. A summary of the TAZ and ZDATA edits is included in **Table 2**.

- The 2045 CF roadway network did not include the Poinciana Parkway Extension north of CR 532 (Osceola Polk Line Road) to the Interstate 4 (I-4)/SR 429 interchange; therefore, the connection from CR 532 and I-4/SR 429 was coded into the network. The connection at the I-4/SR 429 interchange was assumed to be full access.
- Sinclair Road Extension was coded into the model as a 4-lane road with similar attributes to the existing portion of Sinclair Road north of Tradition Boulevard.
- A segment of Tradition Boulevard was added into the model to represent the existing/future T-intersection at Sinclair Road.
- Westside Boulevard is planned to be fully connected to the north and south by the year 2045, and it was coded in the model as a 4-lane road connecting from and to Bella Citta Boulevard and Sand Mine Road.
- The 2045 ZDATA sufficiently accounted for all planned developments in the area except for the Goodman Road Charter School. A separate TAZ (5525) was coded into the network with a connection to Goodman Road north of Sinclair Road to represent the school's access.
- The TAZ located south of Sinclair Road and north of I-4 was divided into three (3) separate TAZs (5468, 5526, and 5527) to better represent future developments' access points along Sinclair Road.
- Tradition Boulevard currently provides access between the northern and southern
 portions of Reunion via an overpass on I-4 and allows for vehicles on either side of I-4 to
 access Sinclair Road, S Old Lake Wilson Road, and CR 532. Centroid connectors were
 added to the model to represent the connections between Reunion TAZs as well as
 access to the roadway network.

Dwelling Units Students **Employees** Single-Family TAZ Multifamily Hotel/Motel Commercial Industrial K-12 Service Initial Initial Initial Revised Initial Revised Initial Revised Initial Revised Initial Revised Revised Revised 834 509 509 1206 316 834 334 328 495 481 25 5468 25 0 0 340 649 5483 154 154 340 33 33 153 153 649 4 4 0 0 5484 ¹ 500 500 0 0 97 97 52 52 240 240 12 12 0 0 5525 ² 0 0 0 0 2550 0 0 5526 ³ 0 533 0 0 0 0 0 5527³ 0 1383 19 43 0 0

Table 2: CF 2045 TAZ and ZDATA Revisions

Notes:

^{1.} Planned Illuminate Church is accounted for within the initial 2045 ZDATA.

^{2.} New TAZ, split from 5483 for the planned Goodman Road Charter School (850 students) (includes a factor of 3.0 to align with ITE trip generation)

^{3.} New TAZ, split from 5468 for Dewan/Elevation (444 Multifamily DU) and Sinclair Road Property (446 Multifamily DU, 3.5 KSF restaurant, and 10 pump gas station) (includes a factor of 1.2 for TAZ 5526 and 3.1 for TAZ 5527 to better reflect ITE estimated daily trips).



Two (2) main CF 2045 models were run to determine the impacts of Sinclair Road Extension: No-Build Scenario (without Sinclair Road extension) and Build Scenario (with the Sinclair Road extension). Raw model volumes are shown in **Figure 4**. Model volumes were adjusted using the Osceola County Model Output Conversion Factor (MOCF). The MOCF is identified in the FDOT FTO seasonal factor sheet, included in the **Attachments**. The Sinclair Road Extension is shown to serve as a major connection between Polk County to the west of Reunion and the major freeway interchange of Interstate 4 (I-4) & SR 429. The proposed Sinclair Road extension is shown to reduce traffic along most parallel routes from/to I-4/SR429 and Bella Citta Boulevard & US 27.

Build 2045 volumes were adjusted to account for base year 2015 model underrepresentation of volumes along portions of Goodman Road and Bella Citta Boulevard. Two sets of adjustments were performed:

- Adjustment #1: Historical 2015 AADTs were compared to the adjusted 2015 daily model volume. The model showed to underrepresent the volumes along Goodman Road south of Bella Citta Boulevard and Bella Citta Boulevard west of Goodman Road. The difference in volume (historical 2015 AADT 2015 model vol.) was added to the Build 2045 model daily volume.
- Adjustment #2: The major corridor volumes (Sinclair Road and Bella Citta Boulevard)
 were increased by ±10% of the highest volume along the segment (2,000 daily trips) to
 be conservative.

Table 3 shows a summary of the build 2045 volume development.

2045 AADT Model Volume **Build 2045 AADT Volume Determination** Adi. Historical 2015 Raw 2015 Adi. 2015 Existing County olume Diff Build Adj. #1 Build Adj. #2 Build Roadway Model Model No-Build 2021 2015 (AADT -Model Build 2045 Vol.² Vol. Model 2045 Model 2045 Model Model AADT Model Vol.) Vol. Diff. Model AADT AADT1 Vol. Vol.2 AADT³ AADT⁴ Sinclair Rd North of Tradition Blvd 2,300 2,100 10,500 20.500 10,000 20.500 20.500 22.500 3,500 South of Tradition Blvd 0 15.500 15,500 15,500 15,500 17.500 Tradition Blvd East of Sinclair Rd 3,500 2,300 2,100 10,500 12,000 1,500 12,000 12,000 12,000 Goodman Rd South of Bella Citta Blvd 11.000 2.800 2.500 8.039 5.539 9.300 8.800 -500 8.800 14.339 14.339 North of Bella Citta Blvd 4,400 3,200 2,900 698 -2,202 6,000 5,000 -1,000 5,000 5,000 5,000 Bella Citta Blvd 12.500 6.800 West of Goodman Rd 9.000 2,600 2,400 4.800 2,400 5,700 12,500 14,900 16,900

Table 3: Build 2045 Volume Development

Notes:

Projected Turning Movement Volumes

Future intersection design hour volumes (DHV) for the horizon year 2045 were developed at the study intersections using TURNS5. A K-factor of 0.09 was used, and the D-factors for each intersection were calculated based on existing traffic counts. Adjusted model volumes, shown in **Table 3** above, were used as seed volumes in TURNS5 to generate build 2045 turning movement volumes. TURNS5 outputs are provided in the **Attachments**. **Figure 5** shows the Build 2045 design hourly turning movement volumes.

Adjusted by applying the seasonal factor (SF) for Osceola County 0.96, based on FDOT FTO.

Row model volumes adjusted per MOCF = 0.91
 Ruild 2045 model AADT volumes adjusted where model volumes were underestimated.

^{4.} Build 2045 model AADT volumes adjusted by adding 10% of the highest volume (2,000) along the Sinclair Rd mainline

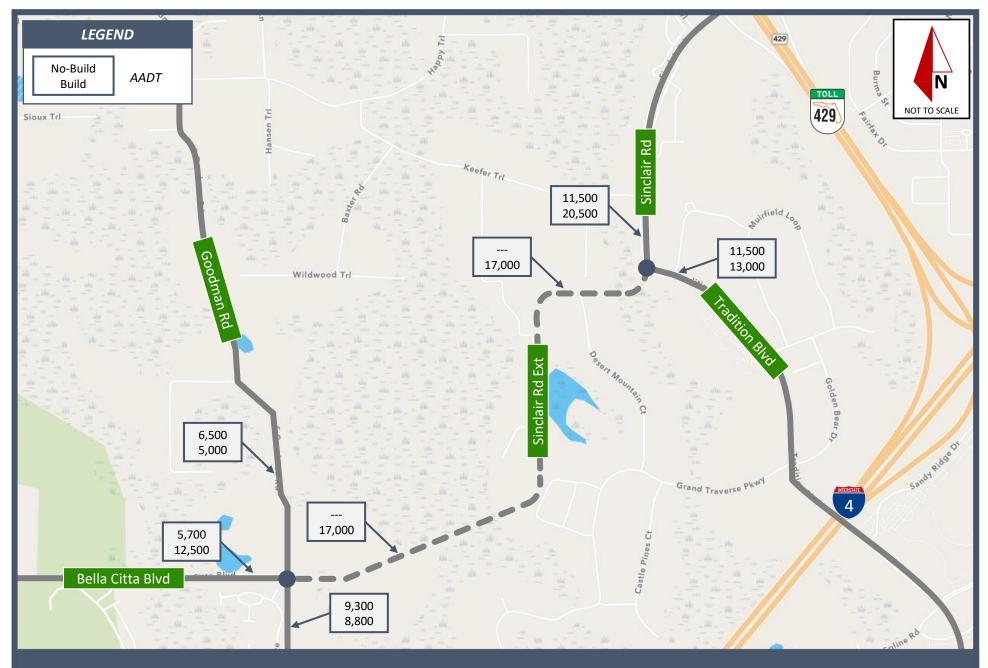


Figure 4: Horizon Year (2045) No-Build and Build Raw Average Daily Traffic (AADT) Sinclair Road Extension | Preliminary Traffic Evaluation

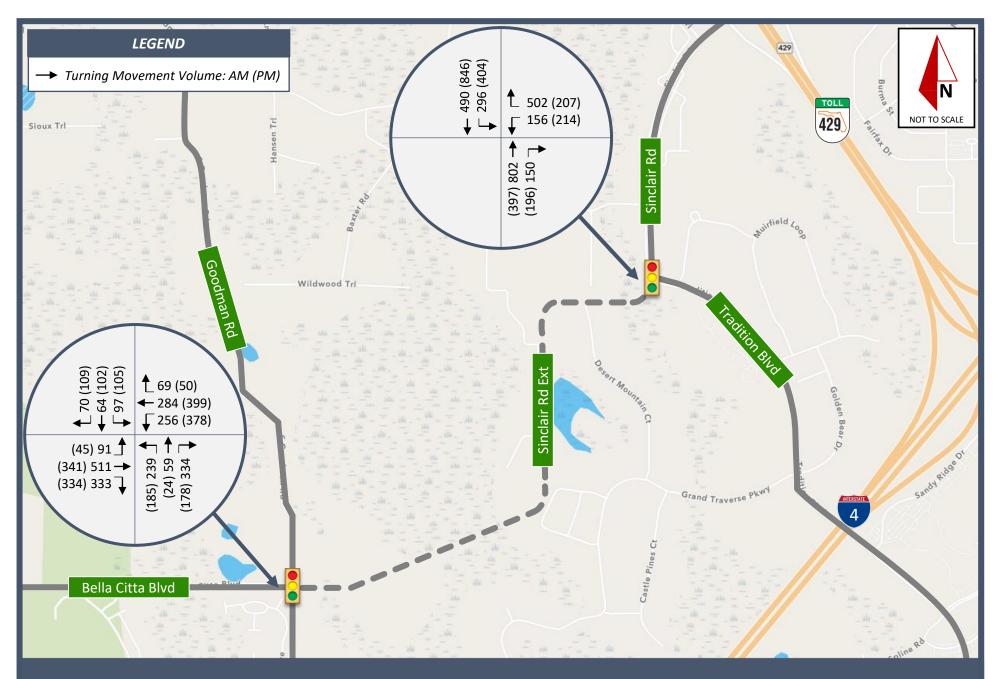


Exhibit 10: Horizon Year (2045) Intersection Turning Movement VolumesSinclair Road Extension | Preliminary Traffic Evaluation



Operational Analysis and Lane Requirements

Synchro v11 was used to evaluate the Build 2045 conditions potential intersection configurations. The intersections were evaluated with multiple control types (unsignalized, signalized, and roundabout) and lane configurations to determine the appropriate intersection configuration needed during the horizon year (2045).

Additionally, an FDOT Intersection Control Evaluation (ICE) Stage 1 was performed using the Capacity Analysis for Planning of Junctions (CAP-X) for the intersection of Sinclair Road & Tradition Boulevard during the AM and PM peak hour conditions. The evaluation concluded the Continuous Green T-intersection to operate with the best volume-to-capacity (v/c) ratio of 0.56 and a traffic signal as the second-best alternative with a maximum v/c ratio of 0.63. Two-lane roundabouts were ranked 3^{rd} (v/c = 0.94) and 4^{th} (v/c = 0.98). CAP-X outputs are provided in the **Attachments**.

The signalized intersection control was selected to evaluate both intersections. As shown in **Table 4** below, all study intersection movements are shown to operate with acceptable LOS and v/c ratio less than one (1.0) during the peak hours with the following lane configuration:

Sinclair Road (N/S) & Tradition Boulevard (E/W)

- Northbound: 1 through lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 2 through lanes
- Westbound: 1 left-turn lane and 1 right-turn lane

Sinclair Road/Bella Citta Boulevard & S Goodman Road

- Northbound: 1 left-turn lane and 1 shared through/right lane
- Southbound: 1 left-turn lane and 1 shared through/right lane
- Westbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane
- Eastbound: 1 left-turn lane, 1 through lane, and 1 shared through/right lane

Synchro outputs and supporting documentation are included in the **Attachments**.

Turn lane length needs were evaluated for all approaches of the study intersections. One (1) vehicle was assumed to be 25 feet. **Table 5** shows a summary of the recommended queue storage lengths for the turn lanes.



Table 4: 2045 Operational Results

| | Build 2045 Conditions | LOS | Delay (sec/veh) | v/c | 95th % Queue (veh) | LOS | Delay (sec/veh) | V/C | 95th % Queue (veh) |
|-------------------------|-----------------------|-----|--------------------|--------|-----------------------|-----|--------------------|---------|-----------------------|
| | Approach | | AM Pea | k Hour | • | | PM Pea | k Hour | |
| | Northbound | Е | 58.5 | - | - | В | 18.8 | = | - |
| _ | L | - | - | _ | - | - | - | - | - |
| <u>%</u> | T | Ε | 58.4 | 0.94 | 23 | В | 18.7 | 0.41 | 8 |
| Tradition Blvd | R* | E | 58.6 | 0.94 | 23 | В | 18.8 | 0.42 | 8 |
| ij | Southbound | С | 32.0 | - | - | Α | 9.3 | - | - |
| Ľ | L | Ε | 62.6 | 0.95 | 12 | В | 14.0 | 0.78 | 6 |
| જ | Т | В | 13.8 | 0.30 | 6 | Α | 6.7 | 0.36 | 6 |
| Sinclair Rd | R | - | - | _ | - | - | - | - | - |
| <u>a</u> : | Westbound | D | 50.7 | - | - | D | 51.2 | - | - |
| ši | L | С | 22.6 | 0.27 | 5 | D | 36.6 | 0.54 | 10 |
| ٠, | Т | - | - | - | - | - | - | - | - |
| | R | Ε | 59.5 | 0.96 | 24 | D | 61.5 | 0.89 | 10 |
| | Overall | D | 47.7 | - | - | В | 19.7 | - | - |
| | Approach | | AM Pea | k Hour | | | PM Pea | ık Hour | |
| | Northbound | E | 62.3 | - | - | С | 33.7 | - | - |
| | L | D | 38.5 | 0.63 | 6 | С | 31.5 | 0.64 | 7 |
| 8 | T | Α | 0.0 | 0.00 | 0 | Α | 0.0 | 0.00 | 0 |
| Goodman Rd | R* | Ε | <i>76.7</i> | 0.97 | 28 | D | 35.7 | 0.68 | 8 |
| 臣 | Southbound | D | 48.00 | - | - | D | 38 | - | - |
| 90 | L | Ε | 60.0 | 0.78 | 7 | С | 29.6 | 0.39 | 4 |
| Ø | T | Α | 0.0 | 0.00 | 0 | Α | 0.0 | 0.00 | 0 |
| 쮼 | R* | D | 39.0 | 0.34 | 8 | D | 42.2 | 0.81 | 9 |
| itta | Eastbound | E | 69.5 | - | - | С | 31.3 | - | - |
| aCi | L | С | 28.5 | 0.24 | 4 | С | 21.1 | 0.12 | 1 |
| Sell sell | Т | Ε | 73.1 | 0.96 | 29 | С | 31.00 | 0.73 | 12 |
| , g | R* | Ε | 74.7 | 0.93 | 27 | С | 33.00 | 0.80 | 12 |
| i R | Westbound | D | 45.9 | - | - | С | 29.7 | - | - |
| Sinclair Rd/Bella Citta | L | Ε | 71.8 | 0.93 | 20 | D | 44.5 | 0.93 | 14 |
| Si | T | С | 26.3 | 0.29 | 8 | В | 17.0 | 0.32 | 6 |
| | R* | С | 26.4 | 0.30 | 8 | В | 17.0 | 0.32 | 6 |
| | Overall | E | 59.6 | _ | _ | С | 32.1 | _ | _ |

Table 5: Recommended Queue Storage Lengths for Turn Lanes

| Intersection | Turn Lane Queue Length (feet) | | | | | | |
|-------------------------------------------|-------------------------------|-----|-----|-----|--|--|--|
| intersection | EBL | WBL | NBL | SBL | | | |
| Sinclair Rd & Tradition Bvld | - | 250 | - | 300 | | | |
| Sinclair Rd/Bella Citta Blvd & Goodman Rd | 100 | 500 | 175 | 175 | | | |

 $Note: 1.95 th-percentile \ queue\ as reported\ in the\ Synchro\ outputs. Turn lane\ queue\ length\ rounded\ to\ the\ nearest\ 25 ft.$

^{*} Shared movements.

APPENDIX N Highway Safety Manual (HS) Crash Prediction Outputs

WORKSHEET 1A -- GENERAL INFORMATION AND INPUT DATA FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| General Information | | | Location Information | | |
|---------------------------------------------------|-----------------------------------------------------------------------|------------------|-------------------------------------|-----------------------------------|-----------------|
| Analyst | EDRM | | Roadway | Sinclair Rd | |
| Agency or Company K | Kimley-Horn | | Roadway Section | from Tradition Blvd to Goodman Rd | |
| Date Performed 0 | 05/19/22 | | Jurisdiction | Osceola County | |
| Segment for Analysis S | Segment 1 | | Analysis Year | 2045 | |
| Input Data | | | | Site Conditions | Base Conditions |
| Roadway type (2U, 3T, 4U, 4D, 5T) | | | | 4D | |
| Length of segment, L (mi) | Length of segment, L (mi) | | | 1.5 | - |
| AADT (veh/day) is within range | AADT (veh/day) is within range AADT _{MAX} = 66,000 (veh/day) | | | 17,500 | |
| Type of on-street parking (none/parallel/angl | of on-street parking (none/parallel/angle) | | | None | None |
| Proportion of curb length with on-street park | king | | | 0 | |
| Median width (ft) - for divided only | * * * * * * * * * * * * * * * * * * * * | | | 15 | 15 |
| Lighting (present / not present) | | | | Present | Not Present |
| Auto speed enforcement (present / not present | ent) | | | Not Present | Not Present |
| Major commercial driveways (number) | | | | 0 | |
| Minor commercial driveways (number) | | | | 0 | - |
| Major industrial / institutional driveways (nur | mber) | | | 0 | |
| Minor industrial / institutional driveways (nu | mber) | | | 0 | - |
| Major residential driveways (number) | | | | 1 | |
| Minor residential driveways (number) | | | | 1 | - |
| Other driveways (number) | | | | 0 | |
| Speed Category | | | Posted | Speed Greater than 30 mph | |
| Roadside fixed object density (fixed objects / | mi) | | | 0 | 0 |
| Offset to roadside fixed objects (ft) [If greater | r than 30 or Not Present, input 30] | | | 30 | 30 |
| Calibration Factor, Cr | | | | 1.00 | 1.00 |
| Average Annual Crash History (3 or 5-yr aver | rage) | | | | |
| Multiple vehicle driveway crashes | | KABC | Fatal and Injury Only | 0.0 | |
| Multiple vehicle univeway crashes | | PDO | Property Damage Only | 0.0 | |
| Multiple vehicle nondriveway crashes | | KABC | Fatal and Injury Only | 0.0 | |
| | | PDO | Property Damage Only | 0.0 | |
| Single-vehicle crashes | | KABC | Fatal and Injury Only | 0.0 | |
| Jingle-verlice crasiles | | PDO | Property Damage Only | 0.0 | |
| NOTES: * AADT: It is important to remember | that the AADT(major) = AADT(major | approach1) + AAI | DT(minor approach2) (refer to p.12- | 8 in Part C of the HSM) | |

WORKSHEET 1B -- CRASH MODIFICATION FACTORS FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) |
|---------------------------|--------------------------------|----------------------|---------------------|-------------------------------------|---------------------|
| CMF for On-Street Parking | CMF for Roadside Fixed Objects | CMF for Median Width | CMF for Lighting | CMF for Automated Speed Enforcement | Combined CMF |
| CMF 1r | CMF 2r | CMF 3r | CMF 4r | CMF 5r | CMF comb |
| from Equation 12-32 | from Equation 12-33 | from Table 12-22 | from Equation 12-34 | from Section 12.7.1 | (1)*(2)*(3)*(4)*(5) |
| 1.00 | 1.00 | 1.00 | 0.91 | 1.00 | 0.91 |

WORKSHEET 1C -- MULTIPLE-VEHICLE NONDRIVEWAY COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | () | 2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|------------------------------|-------------|---------------------------------|-----------------------------|---------------------------|-----------------------------------------|----------------------------|---------------|-------------|--------------------------------|
| Crash Severity Level | SPF Coe | efficients | Overdispersion Parameter, k | Initial N _{brmv} | Proportion of Total Crashes | Adjusted N _{brmv} | Combined CMFs | Calibration | Predicted N _{brmv} |
| Crash Severity Level | from Ta | from Table 12-3 from Table 12-3 | | from Equation 12-10 | Proportion of Total Clashes | (4) _{TOTAL} *(5) | (6) from | Factor, Cr | (6)*(7)*(8) |
| | a | b | Holli Table 12 5 | Trom Equation 12 To | | (')TOTAL (O) | Worksheet 1B | | (0) (1) (0) |
| Total | -12.34 | 1.36 | 1.32 | 3.867 | 1.000 | 3.867 | 0.91 | 1.00 | 3.534 |
| Fatal and Injury (FI) | -12.76 1.28 | | 1.31 | 1.163 | $(4)_{FI}/((4)_{FI}+(4)_{PDO})$ | 1.097 | 0.91 | 1.00 | 1.002 |
| - atai and injury (i i) | -12.70 | 1.20 | | 1.103 | 0.284 | 1.077 | 0.71 | 1.00 | 1.002 |
| Property Damage Only (PDO) | -12.81 | 1.38 | 1.34 | 2.939 | (5) _{TOTAL} -(5) _{FI} | 2.771 | 0.91 | 1.00 | 2.532 |
| Troperty barriage only (FBO) | -12.01 | 1.30 | 1.54 | 2.737 | 0.716 |] 2.//1 | 0.71 | 1.00 | 2.332 |

WORKSHEET 1D -- MULTIPLE-VEHICLE NONDRIVEWAY COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) |
|----------------------------------|----------------------------------------------|--------------------------------------|------------------------------------|---------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type _(FI) | Predicted N brmv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N brmv (PDO) (crashes/year) | Predicted N _{brmv (TOTAL)} (crashes/year) |
| | from Table 12-4 | (9)FI from Worksheet 1C | from Table 12-4 | (9)PDO from Worksheet 1C | (9)TOTAL from Worksheet 1C |
| Total | 1.000 | 1.002 | 1.000 | 2.532 | 3.534 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Rear-end collision | 0.832 | 0.834 | 0.662 | 1.676 | 2.510 |
| Head-on collision | 0.020 | 0.020 | 0.007 | 0.018 | 0.038 |
| Angle collision | 0.040 | 0.040 | 0.036 | 0.091 | 0.131 |
| Sideswipe, same direction | 0.050 | 0.050 | 0.223 | 0.565 | 0.615 |
| Sideswipe, opposite direction | 0.010 | 0.010 | 0.001 | 0.003 | 0.013 |
| Other multiple-vehicle collision | 0.048 | 0.048 | 0.071 | 0.180 | 0.228 |

WORKSHEET 1E -- SINGLE-VEHICLE COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | () | 2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|----------------------------|---------|------------------------------|-----------------------------|---------------------------|----------------------------------------------------------------------|----------------------------|------------------------------------|------|--------------------------------|
| Crash Severity Level | | | Overdispersion Parameter, k | Initial N _{brsv} | Proportion of Total Crashes | Adjusted N _{brsv} | Combined CMFs Calibration | | Predicted N _{brsv} |
| | from Ta | m Table 12-5 from Table 12-5 | | from Equation 12-13 | · | | (4) _{TOTAL} *(5) (6) from | | (6)*(7)*(8) |
| Total | -5.05 | 0.47 | 0.86 | 0.949 | 1.000 | 0.949 | Worksheet 1B 0.91 | 1.00 | 0.867 |
| Fatal and Injury (FI) | -8.71 | 0.66 | 0.28 | 0.156 | (4) _{FI} /((4) _{FI} +(4) _{PDO}) 0.165 | 0.157 | 0.91 | 1.00 | 0.143 |
| Property Damage Only (PDO) | -5.04 | 0.45 | 1.06 | 0.788 | (5) _{TOTAL} -(5) _{FI} 0.835 | 0.792 | 0.91 | 1.00 | 0.724 |

WORKSHEET 1F -- SINGLE-VEHICLE COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) |
|--------------------------------|----------------------------------------------|-------------------------------------------------|------------------------------------|--------------------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type _(FI) | Predicted N _{brsv} (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N _{brsv} (PDO) (crashes/year) | Predicted N _{brsv} (TOTAL) (crashes/year) |
| | from Table 12-6 | (9)FI from Worksheet 1E | from Table 12-6 | (9)PDO from Worksheet 1E | (9)TOTAL from Worksheet 1E |
| Total | 1.000 | 0.143 | 1.000 | 0.724 | 0.867 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Collision with animal | 0.001 | 0.000 | 0.063 | 0.046 | 0.046 |
| Collision with fixed object | 0.500 | 0.072 | 0.813 | 0.588 | 0.660 |
| Collision with other object | 0.028 | 0.004 | 0.016 | 0.012 | 0.016 |
| Other single-vehicle collision | 0.471 | 0.068 | 0.108 | 0.078 | 0.146 |

WORKSHEET 1G -- MULTIPLE-VEHICLE DRIVEWAY-RELATED COLLISIONS BY DRIVEWAY TYPE FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) |
|--------------------------------|-------------------------------------|-----------------------------------------------|---------------------------------------|--------------------------------------------------------------|-----------------------------|
| Driveway Type | Number of driveways, n _i | Crashes per driveway per year, N _j | Coefficient for traffic adjustment, t | Initial N _{brdwy} | Overdispersion parameter, k |
| Driveway Type | Number of unveways, 11j | from Table 12-7 | form Table 12.7 | Equation 12-16 | from Table 12-7 |
| | | from Table 12-7 from Table 12-7 | | n _i * N _i * (AADT/15,000) ^t | from Table 12-7 |
| Major commercial | 0 | 0.033 | 1.106 | 0.000 | |
| Minor commercial | 0 | 0.011 | 1.106 | 0.000 | |
| Major industrial/institutional | 0 | 0.036 | 1.106 | 0.000 | |
| Minor industrial/institutional | 0 | 0.005 | 1.106 | 0.000 | |
| Major residential | 1 | 0.018 | 1.106 | 0.021 | |
| Minor residential | 1 | 0.003 | 1.106 | 0.004 | |
| Other | 0 | 0.005 | 1.106 | 0.000 | |
| Total | | | | 0.025 | 1.39 |

WORKSHEET 1H -- MULTIPLE-VEHICLE DRIVEWAY-RELATED COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|----------------------------|----------------------------------------|-------------------------------------------------|-----------------------------|-----------------------|------------------------------------|------------------------------|
| Creak Councilial and | Initial N _{brdwy} | Proportion of total crashes (f _{dwy}) | Adjusted N _{brdwy} | Combined CMFs | Calibration factor C | Predicted N _{brdwy} |
| Crash Severity Level | (5) _{TOTAL} from Worksheet 1G | from Table 12-7 | (2) _{TOTAL} * (3) | (6) from Worksheet 1B | Calibration factor, C _r | (4)*(5)*(6) |
| Total | 0.025 | 1.000 | 0.025 | 0.91 | 1.00 | 0.023 |
| Fatal and injury (FI) | | 0.284 | 0.007 | 0.91 | 1.00 | 0.006 |
| Property damage only (PDO) | | 0.716 | 0.018 | 0.91 | 1.00 | 0.016 |

WORKSHEET 11 -- VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|-----------------------|---------------------------------------------------------|-----------------------|------------------------------|---------------------------------------------|-----------------|------------------------|-----------------------------|
| Crash Severity Level | Predicted N _{brmv} Predicted N _{brsv} | | Predicted N _{brdwy} | Predicted N _{br} f _{pedr} | | Calibration | Predicted N _{pedr} |
| | (9) from Worksheet 1C | (9) from Worksheet 1E | (7) from Worksheet 1H | (2)+(3)+(4) | from Table 12-8 | factor, C _r | (5)*(6)*(7) |
| Total | 3.534 | 0.867 | 0.023 | 4.424 | 0.019 | 1.00 | 0.084 |
| Fatal and injury (FI) | | | | | | 1.00 | 0.084 |

WORKSHEET 1J -- VEHICLE-BICYCLE COLLISIONS FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) |
|-----------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|-----------------|------------------------|------------------------------|
| Crash Severity Level | Predicted N _{brmv} | Predicted N _{brsv} | Predicted N _{brdwy} | wy Predicted N _{br} | | Calibration | Predicted N _{biker} |
| | (9) from Worksheet 1C | (9) from Worksheet 1E | (7) from Worksheet 1H | (2)+(3)+(4) | from Table 12-9 | factor, C _r | (5)*(6)*(7) |
| Total | 3.534 | 0.867 | 0.023 | 4.424 | 0.005 | 1.00 | 0.022 |
| Fatal and injury (FI) | | | | | | 1.00 | 0.022 |

WORKSHEET 1K -- CRASH SEVERITY DISTRIBUTION FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) |
|------------------------------------------------------|-------------------------------|-----------------------------------|-------------------------------|
| | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Callisian type | (3) from Worksheet 1D and 1F; | (5) from Worksheet 1D and 1F; and | (6) from Worksheet 1D and 1F; |
| Collision type | (7) from Worksheet 1H; and | (7) from Worksheet 1H | (7) from Worksheet 1H; and |
| | (8) from Worksheet 1I and 1J | (7) HOTH WORKSHEEL TH | (8) from Worksheet 1I and 1J |
| | MULTIPLE-VEHICLE | · | • |
| ear-end collisions (from Worksheet 1D) | 0.834 | 1.676 | 2.510 |
| lead-on collisions (from Worksheet 1D) | 0.020 | 0.018 | 0.038 |
| ngle collisions (from Worksheet 1D) | 0.040 | 0.091 | 0.131 |
| ideswipe, same direction (from Worksheet 1D) | 0.050 | 0.565 | 0.615 |
| ideswipe, opposite direction (from Worksheet 1D) | 0.010 | 0.003 | 0.013 |
| riveway-related collisions (from Worksheet 1H) | 0.006 | 0.016 | 0.023 |
| other multiple-vehicle collision (from Worksheet 1D) | 0.048 | 0.180 | 0.228 |
| ubtotal | 1.009 | 2.549 | 3.557 |
| | SINGLE-VEHICLE | | |
| ollision with animal (from Worksheet 1F) | 0.000 | 0.046 | 0.046 |
| ollision with fixed object (from Worksheet 1F) | 0.072 | 0.588 | 0.660 |
| ollision with other object (from Worksheet 1F) | 0.004 | 0.012 | 0.016 |
| ther single-vehicle collision (from Worksheet 1F) | 0.068 | 0.078 | 0.146 |
| ollision with pedestrian (from Worksheet 1I) | 0.084 | 0.000 | 0.084 |
| ollision with bicycle (from Worksheet 1J) | 0.022 | 0.000 | 0.022 |
| ubtotal | 0.250 | 0.724 | 0.973 |
| otal | 1.258 | 3.272 | 4.530 |

WORKSHEET 1L -- SUMMARY RESULTS FOR URBAN AND SUBURBAN ROADWAY SEGMENTS

| (1) | (2) | (3) | (4) | |
|----------------------------|---------------------------------------------------------------------|--------------------------------|------------------------------|--|
| Crash Severity Level | Predicted average crash frequency, N predicted rs (crashes/year) | Roadway segment length, L (mi) | Crash rate (crashes/mi/year) | |
| | (Total) from Worksheet 1K | | (2) / (3) | |
| Total | 4.5 | 1.50 | 3.0 | |
| Fatal and injury (FI) | 1.3 | 1.50 | 0.8 | |
| Property damage only (PDO) | 3.3 | 1.50 | 2.2 | |

| | PROJECT ELEMENT RESULTS SUMMARY ¹ | | | | | | | | | |
|---------------------------------|----------------------------------------------|----------------------------------------|---------------------------|-----------------------------------------|----------------------------------|------------------------------|------------------------------------------|----------------------------------------|------------------------------|--|
| | Total Crashes/yr (KABCO) | | | Fatal and Injury Crashes/yr (KABC) | | | Property Damage Only Crashes/yr (PDO) | | | |
| Summary for the project element | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement | |
| | N _{predicted (KABCO)} | N _{expected (KABCO)} | | N _{predicted (KABC)} | N _{expected (KABC)} | | N _{predicted (O)} | N _{expected (O)} | | |
| | 4.5 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 | |

Special Note: When the project element is not included in the analysis the results will all be zeros. In addition if only the analysis only includes determining the predicted average crash frequency (i.e. EB analysis is not carried out), the results will show zero values where EB results are usually displayed.

WORKSHEET 2A -- GENERAL INFORMATION AND INPUT DATA FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| General Information | | | Location Inform | nation | | | | |
|------------------------------------------------------------------------------------------|-----------------------------------------------|-----------------------|------------------|---------------------|--------------------------------------|-----------------|--|--|
| Analyst EDF | RM | | Roadway | | Sinclair Rd & Tradition Blvd | | | |
| Agency or Company Kim | nley-Horn | | Location Inform | nation | 0 | | | |
| Date Performed 5/1 | 19/2022 | | Jurisdiction | | Osceola County | | | |
| Intersection Inte | ersection 1 | | Analysis Year | | 2045 | | | |
| Signalized/Unsignalized Sign | nalized | | Ped Volume (af | ter Intx Type) | Not Known | ▼ | | |
| Input Data | | | | | Site Conditions | Base Conditions | | |
| Intersection type (3ST, 3SG, 4ST, 4SG | G) | | | | 3SG | | | |
| AADT major (veh/day) (total entering | on major approaches)* | AADT _{MAX} = | 58,100 | (veh/day) | 20,900 | | | |
| AADT minor (veh/day) (total entering | on minor approaches)* | AADT _{MAX} = | 16,400 | (veh/day) | 5,300 | | | |
| Intersection lighting (present/not pr | resent) | | | | Present | Not Present | | |
| Calibration factor, C _i | | | | | 1.00 | 1.00 | | |
| Data for unsignalized intersections of | only: | | | | | • | | |
| Number of major-road approa | aches with left-turn lanes (0,1,2) | | | | 0 0 | | | |
| Number of major-road approa | aches with right-turn lanes (0,1,2) | | | | 0 0 | | | |
| Data for signalized intersections only | l <u>y:</u> | | | | | · | | |
| Number of approaches with left-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | | | | 2 | 0 | | | |
| Number of approaches with right-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | | | | 1 | 0 | | | |
| Number of approaches with le | eft-turn signal phasing [for 3SG, us | se maximum value | of 3] | | 2 | | | |
| Type of left-turn signal phasin | ng for Leg #1 | | | | Protected/Permissive | Permissive | | |
| Type of left-turn signal phasin | ng for Leg #2 | | | | Protected | | | |
| Type of left-turn signal phasin | ng for Leg #3 | | | | Not Applicable | | | |
| Type of left-turn signal phasin | ng for Leg #4 (if applicable) | | | | Not Applicable | | | |
| Number of approaches with ri | ight-turn-on-red prohibited [for 35 | SG, use maximum | value of 3] | | 0 | 0 | | |
| Intersection red light cameras | s (present/not present) | | | | Not Present | Not Present | | |
| Sum of all pedestrian crossing | g volumes (PedVol) Signalized in | tersections only | | | 50 | | | |
| Maximum number of lanes cre | rossed by a pedestrian (n _{lanesx}) | | | | 4 | | | |
| Number of bus stops within 3 | 300 m (1,000 ft) of the intersection | | | | 0 | 0 | | |
| Schools within 300 m (1,000 f | ft) of the intersection (present/not | present) | | | Not Present | Not Present | | |
| Number of alcohol sales estab | blishments within 300 m (1,000 ft) | of the intersection | n | | 0 | 0 | | |
| Average Annual Crash History (3 or | r 5-yr average) | | | | | | | |
| Multiple vehicle crashes | | KABC | Fatal and Injury | Only | 0.0 | | | |
| iviuitipie veriicie crasfies | | PDO | Property Damag | ge Only | 0.0 | | | |
| Single-vehicle crashes | | KABC | Fatal and Injury | Only | 1.0 | | | |
| Single-verticle crasties | | PDO | Property Damag | ge Only | 3.0 | | | |
| NOTES: * AADT: It is important to re | emember that the AADT(major) = | AADT(major appro | oach1) + AADT(m | ninor approach2) (r | efer to p.12-8 in Part C of the HSM) | | | |

WORKSHEET 2B -- CRASH MODIFICATION FACTORS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|-------------------------|----------------------------------|--------------------------|---------------------------|---------------------|---------------------------|-------------------------|
| CMF for Left-Turn Lanes | CMF for Left-Turn Signal Phasing | CMF for Right-Turn Lanes | CMF for Right Turn on Red | CMF for Lighting | CMF for Red Light Cameras | Combined CMF |
| CMF 1i | CMF 2i | CMF 3i | CMF 4i | CMF 5i | CMF 6i | CMF _{COMB} |
| from Table 12-24 | from Table 12-25 | from Table 12-26 | from Equation 12-35 | from Equation 12-36 | from Equation 12-37 | (1)*(2)*(3)*(4)*(5)*(6) |
| 0.8600 | 0.9306 | 0.9600 | 1.0000 | 0.9661 | 1.0000 | 0.7422 |

WORKSHEET 2C -- MULTIPLE-VEHICLE COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | | (3) | (4) | (5) | (6) | (7) | (8) | (6)*(7)*(8) | |
|----------------------------|------------------|------------------|------------------|-----------------------------|---------------------------|----------------------------------------------------------------------|----------------------------|------------------------|-------------|-----------|
| Crash Severity Level | | SPF Coefficients | | Overdispersion Parameter, k | Initial N _{bimv} | Proportion of Total Crashes | Adjusted N _{bimv} | Combined CMFs | Calibration | Predicted |
| | from Table 12-10 | | from Table 12-10 | from Equation 12-21 | · | (4) _{TOTAL} *(5) | (7) from | Factor, C _i | N_{bimv} | |
| | а | b | С | ITOTTI Table 12-10 | ITOTIT Equation 12 21 | | (')TOTAL (O) | Worksheet 2B | | |
| Total | -12.13 | 1.11 | 0.26 | 0.33 | 3.131 | 1.000 | 3.131 | 0.74 | 1.00 | 2.324 |
| Fatal and Injury (FI) | -11.58 | 1.02 | 0.17 | 0.30 | 1.025 | (4) _{FI} /((4) _{FI} +(4) _{PDO}) 0.343 | 1.075 | 0.74 | 1.00 | 0.798 |
| Property Damage Only (PDO) | -13.24 | 1.14 | 0.30 | 0.36 | 1.960 | (5) _{TOTAL} -(5) _{FI} 0.657 | 2.056 | 0.74 | 1.00 | 1.526 |

WORKSHEET 2D -- MULTIPLE-VEHICLE COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) |
|----------------------------------|----------------------------------|--------------------------------------|------------------------------------|-------------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type(FI) | Predicted N bimv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N bilmv (PDO) (crashes/year) | Predicted N _{bimv (TOTAL)} (crashes/year) |
| | from Table 12-11 | (9)FI from Worksheet 2C | from Table 12-11 | (9)PDO from Worksheet 2C | (9)PDO from Worksheet 2C |
| Total | 1.000 | 0.798 | 1.000 | 1.526 | 2.324 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Rear-end collision | 0.549 | 0.438 | 0.546 | 0.833 | 1.271 |
| Head-on collision | 0.038 | 0.030 | 0.020 | 0.031 | 0.061 |
| Angle collision | 0.280 | 0.223 | 0.204 | 0.311 | 0.535 |
| Sideswipe | 0.076 | 0.061 | 0.032 | 0.049 | 0.109 |
| Other multiple-vehicle collision | 0.057 | 0.045 | 0.198 | 0.302 | 0.348 |

WORKSHEET 2E -- SINGLE-VEHICLE COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | | (2) | | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|----------------------------|------------------|------------------|------|-----------------------------|---------------------------------------------|----------------------------------------------------------------------|----------------------------|--------------------------|------------------------|--------------------------------|
| Crash Severity Level | SPF Coefficients | | | Overdispersion Parameter, k | Initial N _{bisv} | Proportion of Total Crashes | Adjusted N _{bimv} | Combined CMFs | Calibration | Predicted N _{bisv} |
| | _ | from Table 12-12 | | from Table 12-12 | from Eqn. 12-24; (FI) from Eqn. 12-24 or | Proportion of Total Grasiles = | (4) _{TOTAL} *(5) | (7) from Worksheet 2B | Factor, C _i | (6)*(7)*(8) |
| | a | a b c | С | | 12-27 | | | | | |
| Total | -9.02 | 0.42 | 0.40 | 0.36 | 0.244 | 1.000 | 0.244 | 0.74 | 1.00 | 0.181 |
| Fatal and Injury (FI) | -9.75 | 0.27 | 0.51 | 0.24 | 0.068 | (4) _{FI} /((4) _{FI} +(4) _{PDO}) 0.286 | 0.070 | 0.74 | 1.00 | 0.052 |
| Property Damage Only (PDO) | -9.08 | 0.45 | 0.33 | 0.53 | 0.170 | (5) _{TOTAL} -(5) _{FI} 0.714 | 0.174 | 0.74 | 1.00 | 0.129 |

WORKSHEET 2F -- SINGLE-VEHICLE COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) |
|--------------------------------|----------------------------------------------|--------------------------------------|------------------------------------|---------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type _(FI) | Predicted N bisv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N bisv (PDO) (crashes/year) | Predicted N _{bisv (TOTAL)} (crashes/year) |
| | from Table 12-13 | (9) _{FI} from Worksheet 2E | from Table 12-13 | (9)PDO from Worksheet 2E | (9) _{PDO} from Worksheet 2E |
| Total | 1.000 | 0.052 | 1.000 | 0.129 | 0.181 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Collision with parked vehicle | 0.001 | 0.000 | 0.001 | 0.000 | 0.000 |
| Collision with animal | 0.001 | 0.000 | 0.003 | 0.000 | 0.000 |
| Collision with fixed object | 0.653 | 0.034 | 0.895 | 0.116 | 0.149 |
| Collision with other object | 0.091 | 0.005 | 0.069 | 0.009 | 0.014 |
| Other single-vehicle collision | 0.045 | 0.002 | 0.018 | 0.002 | 0.005 |
| Single-vehicle noncollision | 0.209 | 0.011 | 0.014 | 0.002 | 0.013 |

WORKSHEET 2G -- VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL STOP-CONTROLLED INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|-----------------------|-----------------------------|-----------------------------|---------------------------|-------------------|------------------------------------|-----------------------------|
| Crash Severity Level | Predicted N _{bimv} | Predicted N _{bisv} | Predicted N _{bi} | f _{pedi} | Calibration factor, C _i | Predicted N _{pedi} |
| | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-16 | Calibration factor, c _i | (4)*(5)*(6) |
| Total | | | | | 1.00 | |
| Fatal and injury (FI) | | | | | 1.00 | |

WORKSHEET 2H -- CRASH MODIFICATION FACTORS FOR VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL SIGNALIZED INTERSECTIONS

| (1) | (2) | (3) | (4) |
|-------------------|-------------------|--------------------------------------|----------------|
| CMF for Bus Stops | CMF for Schools | CMF for Alcohol Sales Establishments | Combined CMF |
| CMF _{1p} | CMF _{2p} | CMF _{3p} | Combined Civir |
| from Table 12-28 | from Table 12-29 | from Table 12-30 | (1)*(2)*(3) |
| 1.00 | 1.00 | 1.00 | 1.00 |

WORKSHEET 2I -- VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL SIGNALIZED INTERSECTIONS

| (1) | | | (2) | | | (3) | (4) | (5) | (6) | (7) |
|-----------------------|-------|------------------|------------------|------|------|----------------|----------------------------------|--------------------------|------------------------|--------------------------------|
| Crash Severity Level | | : | SPF Coefficients | | | Overdispersion | N _{pedbase} | Combined CMF | Calibration | Predicted N _{pedi} |
| | | from Table 12-14 | | | | | Parameter, k from Equation 12-29 | (4) from Worksheet 2H | factor, C _i | (4)*(5)*(6) |
| | a | b | С | d | е | | Hom Equation 12-27 | (4) ITOTTI WORKSHEET ZIT | | (4) (3) (0) |
| Total | -6.60 | 0.05 | 0.24 | 0.41 | 0.09 | 0.52 | 0.012 | 1.00 | 1.00 | 0.012 |
| Fatal and Injury (FI) | | | | | | | | | 1.00 | 0.012 |

WORKSHEET 2J -- VEHICLE-BICYCLE COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|-----------------------|-----------------------------|-----------------------------|---------------------------|--------------------|------------------------------------|------------------------------|
| Crash Severity Level | Predicted N _{bimv} | Predicted N _{bisv} | Predicted N _{bi} | f _{bikei} | Calibration factor, C _i | Predicted N _{bikei} |
| Crash Severity Level | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-17 | Cambration factor, c | (4)*(5)*(6) |
| Total | 2.324 | 0.181 | 2.505 | 0.011 | 1.00 | 0.028 |
| Fatal and injury (FI) | | | | | 1.00 | 0.028 |

WORKSHEET 2K -- CRASH SEVERITY DISTRIBUTION FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) |
|------------------------------------------------------|-------------------------------|------------------------------|-------------------------------|
| | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 2D and 2F; | (5) from Worksheet 2D and 2F | (6) from Worksheet 2D and 2F; |
| | (7) from 2G or 2I and 2J | | (7) from 2G or 2I and 2J |
| | MULTIPLE-VEHICLE | · | |
| Rear-end collisions (from Worksheet 2D) | 0.438 | 0.833 | 1.271 |
| Head-on collisions (from Worksheet 2D) | 0.030 | 0.031 | 0.061 |
| Angle collisions (from Worksheet 2D) | 0.223 | 0.311 | 0.535 |
| Sideswipe (from Worksheet 2D) | 0.061 | 0.049 | 0.109 |
| Other multiple-vehicle collision (from Worksheet 2D) | 0.045 | 0.302 | 0.348 |
| Subtotal | 0.798 | 1.526 | 2.324 |
| | SINGLE-VEHICLE | | |
| Collision with parked vehicle (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with animal (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with fixed object (from Worksheet 2F) | 0.034 | 0.116 | 0.149 |
| Collision with other object (from Worksheet 2F) | 0.005 | 0.009 | 0.014 |
| Other single-vehicle collision (from Worksheet 2F) | 0.002 | 0.002 | 0.005 |
| Single-vehicle noncollision (from Worksheet 2F) | 0.011 | 0.002 | 0.013 |
| Collision with pedestrian (from Worksheet 2G or 2I) | 0.012 | 0.000 | 0.012 |
| Collision with bicycle (from Worksheet 2J) | 0.028 | 0.000 | 0.028 |
| Subtotal | 0.091 | 0.129 | 0.220 |
| Total | 0.889 | 1.655 | 2.544 |

WORKSHEET 2L -- SUMMARY RESULTS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) |
|----------------------------|------------------------------------------------------------------------------|
| Crash severity level | Predicted average crash frequency, N _{predicted int} (crashes/year) |
| | (Total) from Worksheet 2K |
| Total | 2.5 |
| Fatal and injury (FI) | 0.9 |
| Property damage only (PDO) | 1.7 |

PROJECT ELEMENT RESULTS SUMMARY¹

| | Total Crashes/yr (KABCO) | | | Fata | al and Injury Crashes/ (KABC) | 'yr | Property Damage Only Crashes/yr (PDO) | | |
|---------------------------------|-----------------------------------|-------------------------------|------------------------------|-----------------------------------------|----------------------------------|------------------------------|------------------------------------------|----------------------------------|------------------------------|
| Summary for the project element | Predicted average crash frequency | | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement |
| | N _{predicted (KABCO)} | N _{expected (KABCO)} | | N _{predicted (KABC)} | N _{expected (KABC)} | | N _{predicted (O)} | N _{expected (O)} | |
| | 2.5 | 0 | 0 | 0.9 | 0 | 0 | 1.7 | 0 | 0 |

Special Note: When the project element is not included in the analysis the results will all be zeros. In addition if only the analysis only includes determining the predicted average crash frequency (i.e. EB analysis is not carried out), the results will show zero values where EB results are usually displayed.

WORKSHEET 2A -- GENERAL INFORMATION AND INPUT DATA FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| General Information | | | Location Inf | formation | | | | | |
|-----------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------|----------------------|---------------|---------------------|-------------------------------------------|-----------------|--|--|--|
| Analyst | EDRM | | Roadway | | Goodman Rd & Bella Citta Blvd/Sinclair Rd | | | | |
| Agency or Company | Kimley-Horn | | Location Inf | ormation | 0 | | | | |
| Date Performed | 5/19/2022 | | Jurisdiction | | Osceola County | | | | |
| Intersection | Intersection 2 | | Analysis Yea | ar | 2045 | | | | |
| Signalized/Unsignalized | Signalized | | Ped Volume | e (after Intx Type) | Not Known | | | | |
| Input Data | | | | | Site Conditions | Base Conditions | | | |
| Intersection type (3ST, 3SG, | 4ST, 4SG) | | | | 4SG | | | | |
| AADT major (veh/day) (total e | DT _{major} (veh/day) (total entering on major approaches)* AADT _{MAX} = | | 67,700 | (veh/day) | 17,100 | | | | |
| AADT _{minor} (veh/day) (total e | ntering on minor approaches)* | $AADT_{MAX} =$ | 33,400 | (veh/day) | 9,800 | | | | |
| Intersection lighting (presen | Intersection lighting (present/not present) | | | | Present | Not Present | | | |
| Calibration factor, C _i | | | | | 1.00 | 1.00 | | | |
| Data for unsignalized interse | | | | | | · | | | |
| Number of major road approaches with left turn lanes (0,1,2) | | | | | 9 | 9 | | | |
| Number of major road approaches with right turn lanes (0,1,2) | | | | | 9 | 0 | | | |
| Data for signalized intersecti | ions only: | | | | | | | | |
| Number of approaches with left-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | | | | | 4 | 0 | | | |
| Number of approache | Number of approaches with right-turn lanes (0,1,2,3,4) [for 3SG, use maximum value of 3] | | | | 0 | 0 | | | |
| Number of approache | s with left-turn signal phasing [for 3SG, | use maximum val | ue of 3] | | 4 | | | | |
| Type of left-turn signal | ll phasing for Leg #1 | | | | Protected/Permissive Permissive | | | | |
| Type of left-turn signal | ll phasing for Leg #2 | | | | Protected/Permissive | | | | |
| Type of left-turn signal | ll phasing for Leg #3 | | | | Protected/Permissive | | | | |
| Type of left-turn signa | l phasing for Leg #4 (if applicable) | | | | Protected/Permissive | | | | |
| Number of approache | s with right-turn-on-red prohibited [for | 3SG, use maximu | m value of 3] | | 0 | 0 | | | |
| Intersection red light of | cameras (present/not present) | | | | Not Present | Not Present | | | |
| Sum of all pedestrian | crossing volumes (PedVol) Signalized | intersections only | 1 | | 50 | | | | |
| Maximum number of | lanes crossed by a pedestrian (n _{lanesx}) | | | | 5 | | | | |
| Number of bus stops v | within 300 m (1,000 ft) of the intersection | on | | | 0 | 0 | | | |
| Schools within 300 m | (1,000 ft) of the intersection (present/n | ot present) | | | Present | Not Present | | | |
| Number of alcohol sale | es establishments within 300 m (1,000 | ft) of the intersect | ion | | 0 | 0 | | | |
| Average Annual Crash Histo | ory (3 or 5-yr average) | | | | | | | | |
| Multiple vehicle crashe | 20 | KABC | Fatal and Inj | jury Only | 0.0 | | | | |
| iviuitipie veriicie crasne | es | PDO | Property Da | mage Only | 0.0 | | | | |
| Single vehicle creekes | KABC Fatal and Injury Only | | | jury Only | 0.0 | | | | |
| Single-vehicle crashes PDO Property Damage Only | | | mana Only | 5.0 | | | | | |

WORKSHEET 2B -- CRASH MODIFICATION FACTORS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) | (7) |
|-------------------------|----------------------------------|--------------------------|---------------------------|---------------------|---------------------------|-------------------------|
| CMF for Left-Turn Lanes | CMF for Left-Turn Signal Phasing | CMF for Right-Turn Lanes | CMF for Right Turn on Red | CMF for Lighting | CMF for Red Light Cameras | Combined CMF |
| CMF 1i | CMF 2i | CMF 3i | CMF 4i | CMF 5i | CMF 6i | CMF _{COMB} |
| from Table 12-24 | from Table 12-25 | from Table 12-26 | from Equation 12-35 | from Equation 12-36 | from Equation 12-37 | (1)*(2)*(3)*(4)*(5)*(6) |
| 0.6600 | 0.9606 | 1.0000 | 1.0000 | 0.9661 | 1.0000 | 0.6125 |

WORKSHEET 2C -- MULTIPLE-VEHICLE COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | | (2) | | (3) | (4) | (5) | (6) | (7) | (8) | (6)*(7)*(8) |
|----------------------------|------------------|--------------------------------------|-----------|-----------------------------|---------------------------|-----------------------------------------|----------------------------|---------------|----------------------|-------------|
| Crash Severity Level | SPF Coefficients | | | Overdispersion Parameter, k | Initial N _{bimv} | Proportion of Total Crashes | Adjusted N _{bimv} | Combined CMFs | ned CMFs Calibration | Predicted |
| Crash Severity Level | | from Table 12-10 from Equation 12-21 | | | (4) _{TOTAL} *(5) | (7) from | Factor, C _i | N_{bimv} | | |
| | a | b | С | ITOTTI TADIE 12-10 | ITOTTI Equation 12-21 | | (4)TOTAL (3) | Worksheet 2B | | |
| Total | -10.99 | 1.07 | 0.23 | 0.39 | 4.725 | 1.000 | 4.725 | 0.61 | 1.00 | 2.894 |
| Fatal and Injury (FI) | -13.14 | 1.18 | 1.18 0.22 | 0.33 | 1.467 | $(4)_{FI}/((4)_{FI}+(4)_{PDO})$ | 1.522 | 0.61 | 1.00 | 0.932 |
| ratarana injury (ri) | -13.14 | 1.10 | 0.22 | | | 0.322 | 1.522 | 0.01 | | 0.732 |
| Property Damage Only (PDO) | -11.02 | 1.02 | 0.24 | 0.44 | 3.088 | (5) _{TOTAL} -(5) _{FI} | 3,203 | 0.61 | 1.00 | 1.962 |
| Froperty Damage Only (PDO) | -11.02 | 1.02 | 0.24 | 0.44 | 3.000 | 0.678 | 3.203 | 0.01 | 1.00 | 1.962 |

WORKSHEET 2D -- MULTIPLE-VEHICLE COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) |
|----------------------------------|----------------------------------|--------------------------------------|------------------------------------|---------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type(FI) | Predicted N blmv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N bimv (PDO) (crashes/year) | Predicted N _{bimv (TOTAL)} (crashes/year) |
| | from Table 12-11 | (9)FI from Worksheet 2C | from Table 12-11 | (9)PDO from Worksheet 2C | (9)PDO from Worksheet 2C |
| Total | 1.000 | 0.932 | 1.000 | 1.962 | 2.894 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Rear-end collision | 0.450 | 0.419 | 0.483 | 0.948 | 1.367 |
| Head-on collision | 0.049 | 0.046 | 0.030 | 0.059 | 0.105 |
| Angle collision | 0.347 | 0.323 | 0.244 | 0.479 | 0.802 |
| Sideswipe | 0.099 | 0.092 | 0.032 | 0.063 | 0.155 |
| Other multiple-vehicle collision | 0.055 | 0.051 | 0.211 | 0.414 | 0.465 |

WORKSHEET 2E -- SINGLE-VEHICLE COLLISIONS BY SEVERITY LEVEL FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | | (2) | | (3) | (4) | (5) | (6) | (7) | (8) | (9) |
|----------------------------|----------------------------------|------------------|------------------|-----------------------------|---------------------------|-----------------------------------------|------------------------------------|------------------------|-------------|--------------------------------|
| | | SPF Coefficients | | Overdispersion Parameter, k | Initial N _{bisv} | Proportion of Total Crashes | Adjusted N _{bimv} | Combined CMFs | Calibration | Predicted N _{bisv} |
| Crash Severity Level | | from Table 12-12 | | | from Eqn. 12-24; (FI) | · · | (4) _{TOTAL} *(5) (7) from | Factor, C _i | (6)*(7)*(8) | |
| | a b c from Table 12-12 | | from Table 12-12 | from Eqn. 12-24 or | | (TOTAL (O) | Worksheet 2B | | (0) (1) (0) | |
| | _ | - | - | | 12-27 | | | | | |
| Total | -10.21 | 0.68 | 0.27 | 0.36 | 0.333 | 1.000 | 0.333 | 0.61 | 1.00 | 0.204 |
| Fatal and Injury (FI) | -9.25 | 0.43 | 0.29 | 0.09 | 0.091 | $(4)_{FI}/((4)_{FI}+(4)_{PDO})$ | 0.093 | 0.61 | 1.00 | 0.057 |
| ratarana injury (ri) | 1 and mjury (F1) -9.25 0.43 0.29 | | 0.27 | 0.07 | 0.071 | 0.278 | 0.073 | 0.01 | 1.00 | 0.037 |
| Droporty Domogo Only (DDO) | -11.34 | 0.78 | 0.25 | 0.44 | 0.237 | (5) _{TOTAL} -(5) _{FI} | 0.240 | 0.71 | 1.00 | 0.147 |
| Property Damage Only (PDO) | -11.34 | 0.76 | 0.25 | 0.44 | 0.237 | 0.722 | 0.240 | 0.61 | 1.00 | 0.147 |

WORKSHEET 2F -- SINGLE-VEHICLE COLLISIONS BY COLLISION TYPE FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) | (5) | (6) |
|--------------------------------|----------------------------------|--------------------------------------|------------------------------------|---------------------------------------|----------------------------------------------------|
| Collision Type | Proportion of Collision Type(FI) | Predicted N bisv (FI) (crashes/year) | Proportion of Collision Type (PDO) | Predicted N bisv (PDO) (crashes/year) | Predicted N _{bisv (TOTAL)} (crashes/year) |
| | from Table 12-13 | (9) _{FI} from Worksheet 2E | from Table 12-13 | (9)PDO from Worksheet 2E | (9)PDO from Worksheet 2E |
| Total | 1.000 | 0.057 | 1.000 | 0.147 | 0.204 |
| | | (2)*(3) _{FI} | | (4)*(5) _{PDO} | (3)+(5) |
| Collision with parked vehicle | 0.001 | 0.000 | 0.001 | 0.000 | 0.000 |
| Collision with animal | 0.002 | 0.000 | 0.002 | 0.000 | 0.000 |
| Collision with fixed object | 0.744 | 0.042 | 0.870 | 0.128 | 0.170 |
| Collision with other object | 0.072 | 0.004 | 0.070 | 0.010 | 0.014 |
| Other single-vehicle collision | 0.040 | 0.002 | 0.023 | 0.003 | 0.006 |
| Single-vehicle noncollision | 0.141 | 0.008 | 0.034 | 0.005 | 0.013 |

WORKSHEET 2G -- VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL STOP-CONTROLLED INTERSECTIONS

| (1) | (2) | (3) | (4) (5) | | (6) | (7) |
|-----------------------|-----------------------------|-----------------------------|---------------------------|-------------------|------------------------------------|-----------------------------|
| Crach Soverity Lovel | Predicted N _{bimv} | Predicted N _{bisv} | Predicted N _{bi} | f _{pedi} | Calibration factor, C _i | Predicted N _{pedi} |
| Crash Severity Level | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-16 | Calibration factor, c _i | (4)*(5)*(6) |
| Total | | | | | 1.00 | |
| Fatal and injury (FI) | | | | | 1.00 | |

WORKSHEET 2H -- CRASH MODIFICATION FACTORS FOR VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL SIGNALIZED INTERSECTIONS

| (1) | (2) | (3) | (4) |
|-------------------|-------------------|--------------------------------------|----------------|
| CMF for Bus Stops | CMF for Schools | CMF for Alcohol Sales Establishments | Combined CMF |
| CMF _{1p} | CMF _{2p} | CMF _{3p} | Combined Civir |
| from Table 12-28 | from Table 12-29 | from Table 12-30 | (1)*(2)*(3) |
| 1.00 | 1.35 | 1.00 | 1.35 |

WORKSHEET 2I -- VEHICLE-PEDESTRIAN COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL SIGNALIZED INTERSECTIONS

| (1) | (2) | | | | | (3) | (4) | (5) | (6) | (7) |
|-----------------------|------------------|------|------|------|------|----------------------|-----------------------------------|--------------------------|------------------------|--------------------------------|
| Crash Severity Level | SPF Coefficients | | | | | Overdispersion | N _{pedbase} Combined CMF | | Calibration | Predicted N _{pedi} |
| Crash Severity Level | from Table 12-14 | | | | | Parameter, k | Parameter, k from Equation 12-29 | (4) from Worksheet 2H | factor, C _i | (4)*(5)*(6) |
| | a | b | С | d | е | ITOTT Equation 12-27 | | (4) ITOTTI WORKSHEET ZIT | | (4) (3) (0) |
| Total | -9.53 | 0.40 | 0.26 | 0.45 | 0.04 | 0.24 | 0.026 | 1.35 | 1.00 | 0.036 |
| Fatal and Injury (FI) | | | | | | | | | 1.00 | 0.036 |

WORKSHEET 2J -- VEHICLE-BICYCLE COLLISIONS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (3) (4) | | (6) | (7) |
|-----------------------|-----------------------------|-----------------------------|---------------------------|--------------------|------------------------------------|------------------------------|
| Crash Severity Level | Predicted N _{bimv} | Predicted N _{bisv} | Predicted N _{bi} | f _{bikei} | Calibration factor, C _i | Predicted N _{bikei} |
| Crash Severity Level | (9) from Worksheet 2C | (9) from Worksheet 2E | (2) + (3) | from Table 12-17 | Cambration factor, c _i | (4)*(5)*(6) |
| Total | 2.894 | 0.204 | 3.098 | 0.015 | 1.00 | 0.046 |
| Fatal and injury (FI) | | | | | 1.00 | 0.046 |

WORKSHEET 2K -- CRASH SEVERITY DISTRIBUTION FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) | (3) | (4) |
|------------------------------------------------------|-------------------------------|------------------------------|-------------------------------|
| | Fatal and injury (FI) | Property damage only (PDO) | Total |
| Collision type | (3) from Worksheet 2D and 2F; | (5) from Worksheet 2D and 2F | (6) from Worksheet 2D and 2F; |
| | (7) from 2G or 2I and 2J | | (7) from 2G or 2I and 2J |
| | MULTIPLE-VEHICLE | • | 1 |
| Rear-end collisions (from Worksheet 2D) | 0.419 | 0.948 | 1.367 |
| Head-on collisions (from Worksheet 2D) | 0.046 | 0.059 | 0.105 |
| Angle collisions (from Worksheet 2D) | 0.323 | 0.479 | 0.802 |
| Sideswipe (from Worksheet 2D) | 0.092 | 0.063 | 0.155 |
| Other multiple-vehicle collision (from Worksheet 2D) | 0.051 | 0.414 | 0.465 |
| Subtotal | 0.932 | 1.962 | 2.894 |
| | SINGLE-VEHICLE | | |
| Collision with parked vehicle (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with animal (from Worksheet 2F) | 0.000 | 0.000 | 0.000 |
| Collision with fixed object (from Worksheet 2F) | 0.042 | 0.128 | 0.170 |
| Collision with other object (from Worksheet 2F) | 0.004 | 0.010 | 0.014 |
| Other single-vehicle collision (from Worksheet 2F) | 0.002 | 0.003 | 0.006 |
| Single-vehicle noncollision (from Worksheet 2F) | 0.008 | 0.005 | 0.013 |
| Collision with pedestrian (from Worksheet 2G or 2I) | 0.036 | 0.000 | 0.036 |
| Collision with bicycle (from Worksheet 2J) | 0.046 | 0.000 | 0.046 |
| Subtotal | 0.139 | 0.147 | 0.286 |
| Total | 1.071 | 2.109 | 3.180 |

WORKSHEET 2L -- SUMMARY RESULTS FOR URBAN AND SUBURBAN ARTERIAL INTERSECTIONS

| (1) | (2) |
|----------------------------|------------------------------------------------------------------------------|
| Crash severity level | Predicted average crash frequency, N _{predicted int} (crashes/year) |
| | (Total) from Worksheet 2K |
| Total | 3.2 |
| Fatal and injury (FI) | 1.1 |
| Property damage only (PDO) | 2.1 |

| | F | PROJECT ELEMENT | RESULTS SUMMARY | | | | |
|---------------------------------------|------------------------------|-----------------------------------------|----------------------------------|---------------------------------------|-----------------------------------------|----------------------------------|------------------------------|
| Fatal and Injury Crashes/yr (KABC) | | | | Property Damage Only Crashes/yr (PDO) | | | |
| | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement | Predicted average crash frequency | Expected average crash frequency | Potential for Improvement |

Npredicted (KABCO) Nexpected (KABCO) Nexpected (KABCO) Nexpected (KABCO) Npredicted (KABCO) Npredicted (KABCO) Nexpected (KABCO) Nexpected

Total Crashes/yr (KABCO) Expected

average crash

frequency

Summary for the Predicted average

project element

crash frequency

PROJECT SAFETY PERFORMANCE SUMMARY REPORT

Project Name
Project Description
Reference Number
Analyst
Agency/Company
Contact Email
Contact Phone

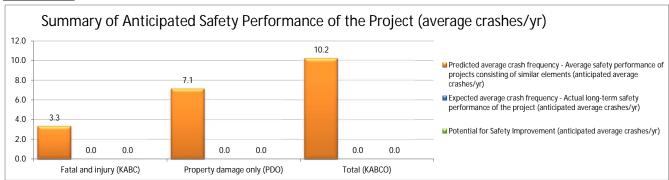
General Information

Sinclair Rd PD&E Sinclair Road PTAR -EDRM

Kimley-Horn

05/19/22

Date Completed
PROJECT SUMMARY



| | Total Crashes/yr (KABCO) | | | Fatal and Injury Crashes/yr (KABC) | | | Property Damage Only Crashes/yr (PDO) | | |
|--------------------------|---------------------------------------------------------------------------|-------------------------------------------------------------------------|------------------------------|--------------------------------------------------------------------------|------------------------------------------------------------------------|------------------------------|-----------------------------------------------------------------------|---------------------------------------------------------------------|------------------------------|
| Project Element | Predicted average crash frequency N _{predicted (KABCO)} | Expected average crash frequency N _{expected (KABCO)} | Potential for Improvement | Predicted average crash frequency N _{predicted (KABC)} | Expected average crash frequency N _{expected (KABC)} | Potential for Improvement | Predicted average crash frequency N _{predicted (O)} | Expected average crash frequency N _{expected (O)} | Potential for Improvement |
| INDIVIDUAL SEGMENTS | | | | | | | | | |
| Segment 1 | 4.5 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 |
| INDIVIDUAL INTERSECTIONS | | | | | | | | | |
| Intersection 1 | 2.5 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | 1.7 | 0.0 | 0.0 |
| Intersection 2 | 3.2 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 | 2.1 | 0.0 | 0.0 |
| COMBINED (sum of column) | 10.2 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 | 7.1 | 0.0 | 0.0 |

PROJECT SUMMARY -- Site-Specific EB Method Summary Results for Urban and Suburban Arterial Project

| | N predicted(PROJECT) | N expected (PROJECT) | N potential for improvement (PROJECT) |
|----------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------|
| Crash severity level | Predicted average crash frequency - Average safety performance of projects consisting of similar elements (anticipated average crashes/yr) | Expected average crash frequency - Actual long-term safety performance of the project (anticipated average crashes/yr) | Potential for Safety Improvement (anticipated average crashes/yr) |
| Fatal and injury (KABC) | 3.3 | 0.0 | N/A |
| Property damage only (PDO) | 7.1 | 0.0 | N/A |
| Total (KABCO) | 10.2 | 0.0 | N/A |

Discussion of Results

Given the potential effects of project characteristics on safety performance, results indicate that:

- 1. It is anticipated that the project will, on average, experience 0 crashes per year (0 fatal and injury crashes per year; and 0 property damage only crashes per year).
- 2. A similar project is anticipated, on average, to experience 10.2 crashes per year (3.3 fatal and injury crashes per year; and 7.1 property damage only crashes per year).